

FOR REVIEW ONLY

First Harley Knox
DPR 20-00014
City of Perris, Riverside County, California

Preliminary Drainage Study

Prepared for:

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SECTION 1 - SUMMARY

PURPOSE

The purpose of this report is to document the hydrologic and hydraulic analyses performed in support of the First Harley Knox logistics project located in the City of Perris, County of Riverside, California. The project site is located at the northwest corner of Harley Knox Boulevard and Redlands Ave. The project is bounded by Oleander Ave to the north, existing light industrial complex to the west, Harley Knox Boulevard to the south, and the Redlands Avenue to the east. The project proposes to build an industrial warehouse on approximately 9.5 acres. This report will summarize the hydrologic and hydraulic analyses that were conducted in order to determine the necessary drainage improvements required to provide flood protection for the proposed building and safely convey the runoff through the site.

The scope of this report will include the following:

- Determine the peak 100-year and 10-year flow rates for the developed condition using the Riverside County Flood Control and Water Conservation District (RCFC&WCD) Rational Method.
- Determine the required storm drain facilities, alignment, and sizes required to flood protect the project site.
- Determine the necessary underground storage area and volume required for water quality treatment and to mitigate for increases in runoff.
- Preparation of a preliminary report summarizing the hydrology and hydraulic results.

DESCRIPTION OF WATERSHED

The project is proposing an industrial warehouse (approximately 158,550 square feet) on approximately 9.5 acres of vacant land. Existing elevations across the site vary from 1459 at the northwest corner to 1458 at the southeast corner (NAVD88 Datum). The site currently slopes down at approximately 0.3% to the southeast corner. The existing drainage pattern for the site and the general area is characterized by sheet flow that currently flows to Harley Knox Boulevard. Flows are captured by an existing catch basin located on the north side of Harley Knox Boulevard and then conveyed within the existing Lat D-3A-4 towards the Perris Valley Storm Drain Channel.

PROPOSED CONDITIONS

The project site is not impacted by off-site flows as there are existing streets around the perimeter of the project that convey any offsite flow away from the site. The balanced earthwork does not allow for conventional gravity storm drains due to lack of drop across the site from the south to the north. In order to convey on-site flows, the project will utilize subsurface storm drain to discharge into underground storage chambers. The chambers are located at the east side of the auto parking stalls along Redlands Avenue and they are sized to hold only the water quality design capture volume for the project. Large flows will be forced out of the chambers at an outlet above the chamber soffit and gravity flow to the existing 48" storm drain line (Lat D-3A) at Harley Knox Boulevard. Water quality runoff will be pumped from the chambers into a Contech Filterra unit.

METHODOLOGY

HYDROLOGY

Hydrologic calculations were performed in accordance with the RCFC&WCD Hydrology Manual, dated April 1978. The Rational Method was utilized in determining peak flow rates.

The hydrological parameters, including rainfall values and soil types were derived from the RCFC&WCD Hydrology Manual. The isohyetal maps and soil map have been included in Section 2.

Rational Method calculations were performed using a computer program developed by CivilDesign Corporation and Joseph E. Bonadiman and Associates Inc. The computer program is commonly referred to as CivilID which incorporates the hydrological parameters outlined in the RCFC&WCD Hydrology Manual.

The Rational Method was used to determine the peak flow rates to size and design the drainage facilities need to convey onsite flows through the site to the proposed basin. The flow rates were computed by generating a hydrologic “link-node” model in which the overall area is divided into separate drainage sub-areas, each tributary to a concentration point (node) determined by the proposed layout and grading.

The Unit Hydrograph Method was used to determine the peak flow rates and volumes associated with the 100-year storm events for the site. Calculations were performed for both the existing condition and developed condition to be used in the analysis of the proposed basin. See Section 2 for additional information and results regarding the hydrologic analyses performed for this project.

HYDRAULICS

Water quality basin calculations were performed using spreadsheets that were created by RCFC&WCD. preliminary calculations and additional details can be found in the preliminary-WQMP.

Basin routing calculations were performed using the CivilID computer program. The CivilID program utilizes the Modified-Puls methodology to routes unit hydrographs through a basin using the stage-storage and stage-discharge curves determined from the proposed basin design. See Section 3 for additional discussion and results.

Hydraulic calculations to determine the required pipe sizes of the proposed onsite storm drain facilities will be provided in the Final Drainage Study.

FIG. 1 VICINITY MAP

FIG. 2 USGS TOPOGRAPHY MAP

FIG. 3 AERIAL PHOTOGRAPH

FIG. 4 RECEIVING WATERBODIES

FIG. 5 SOILS MAP

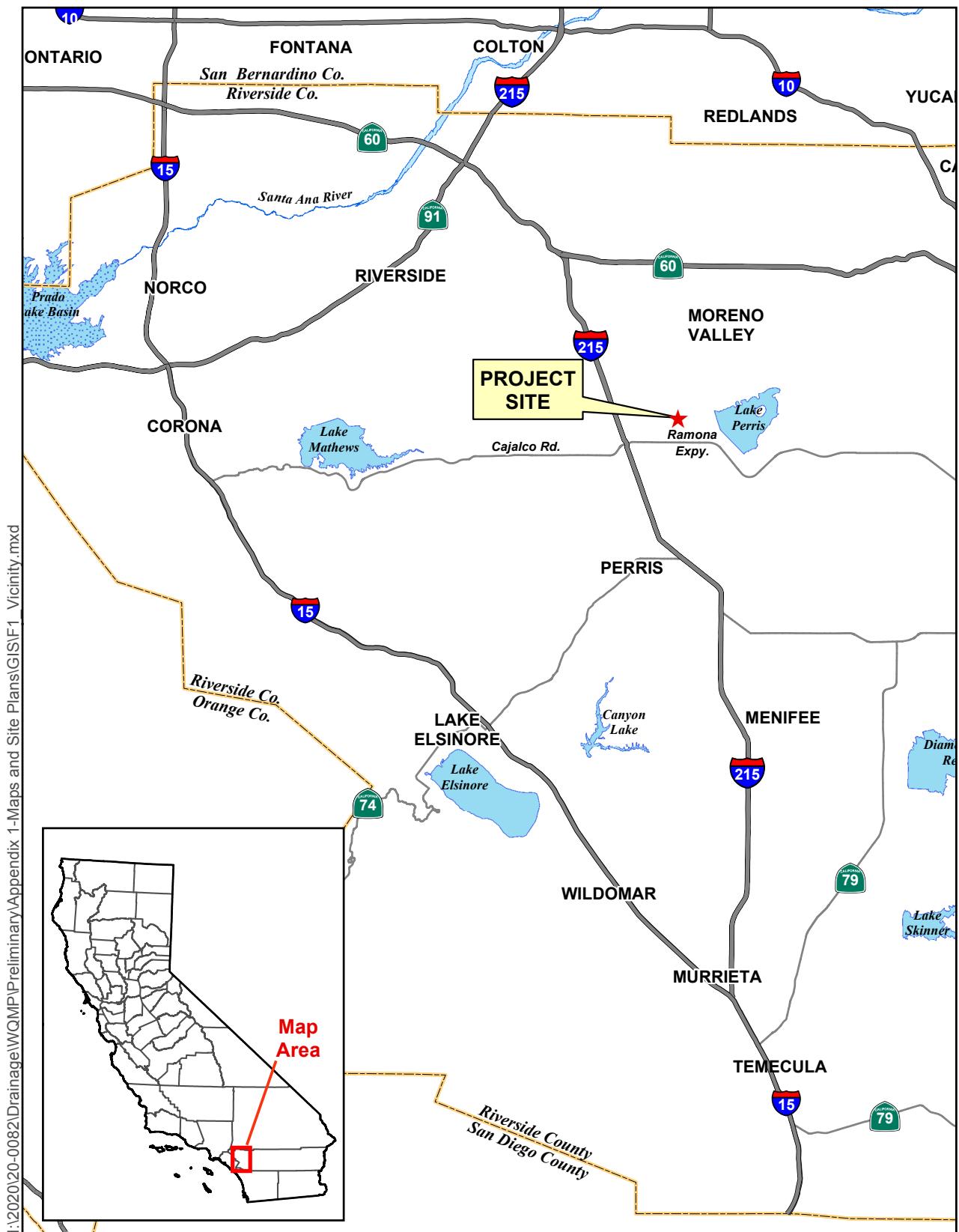
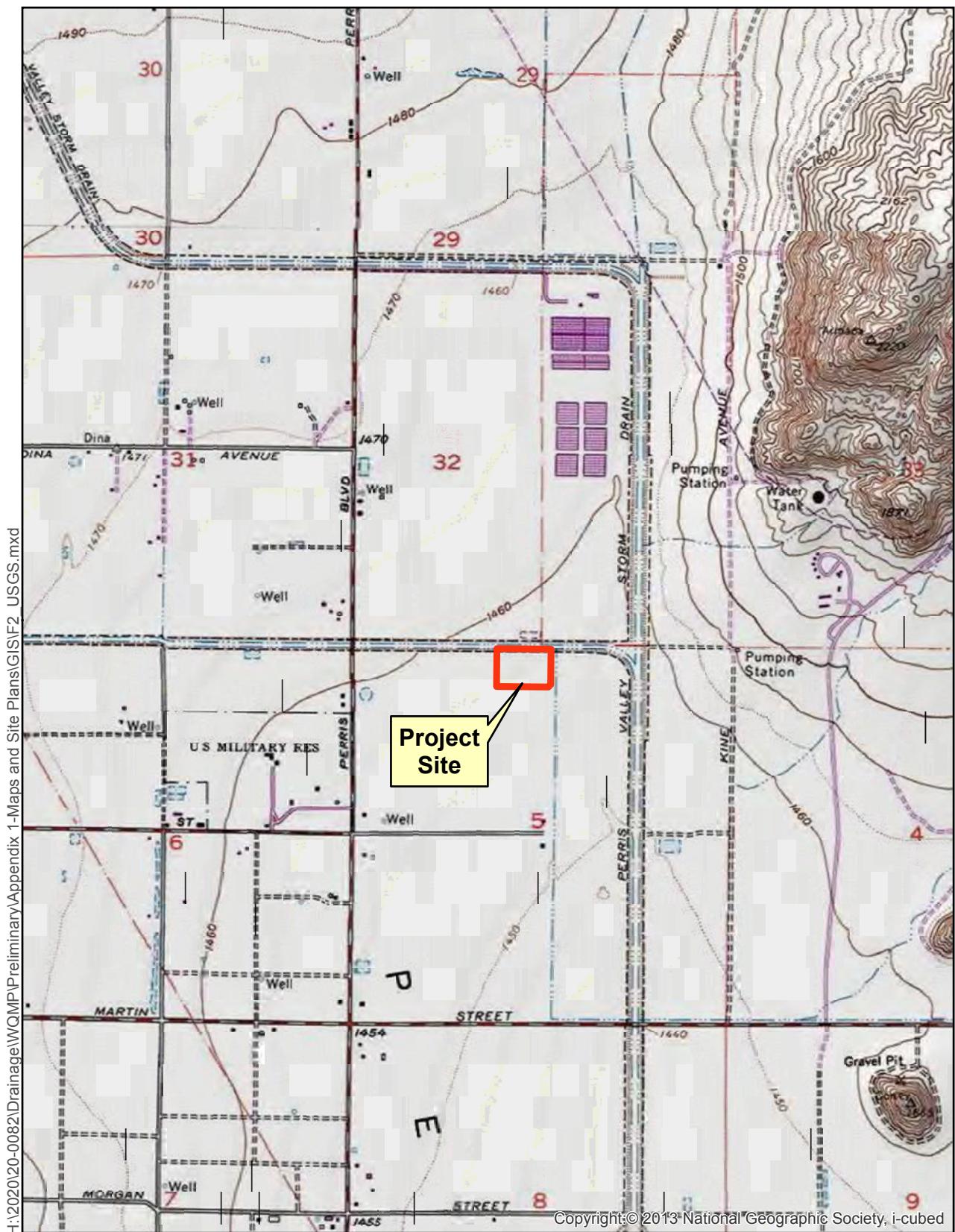


Figure 1. Vicinity Map

0 2.5 5 Miles





Sources: ESRI / USGS 7.5min Quad
DRGs: PERRIS

Figure 2. USGS Topography Map

0 1,000 2,000
Feet



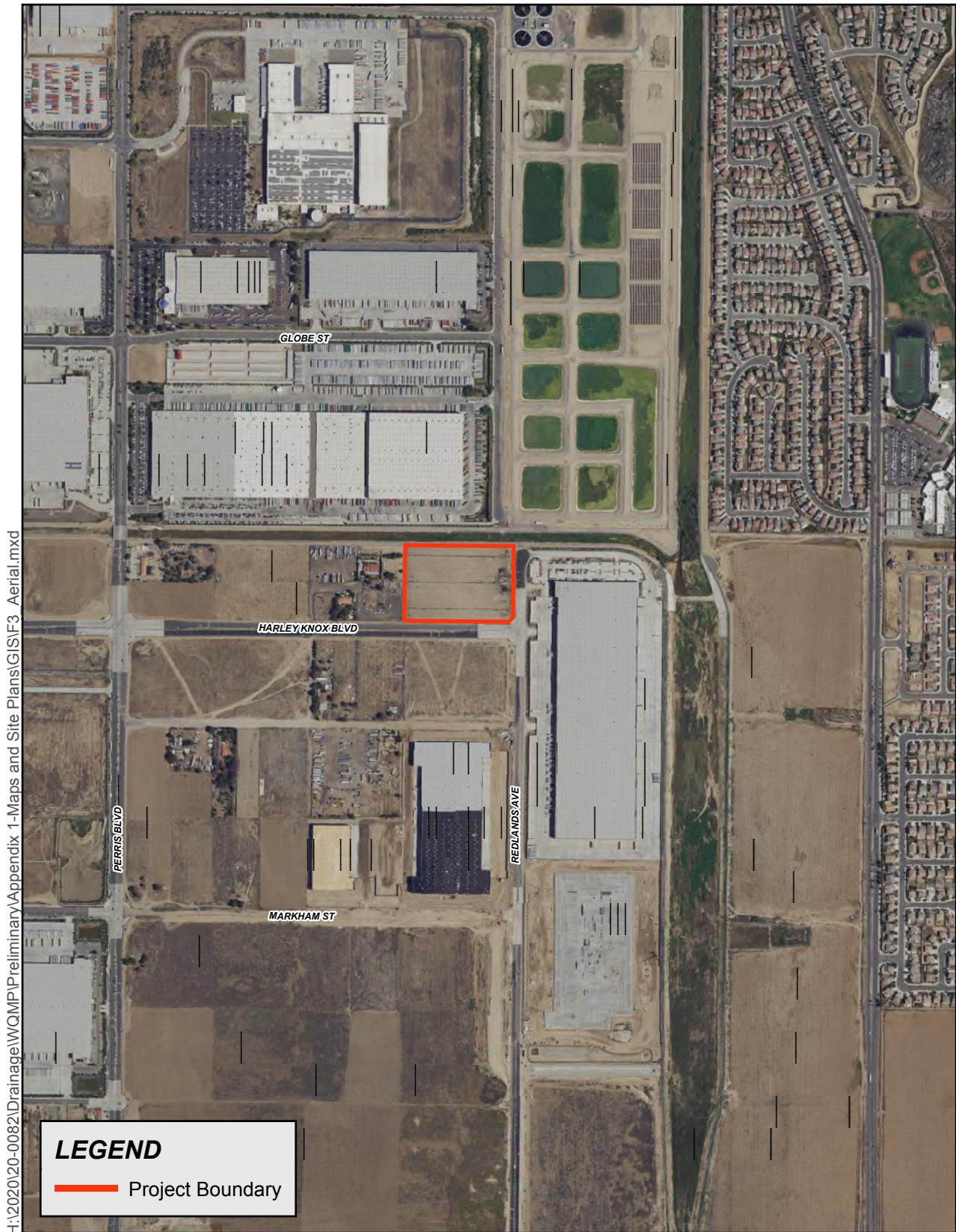
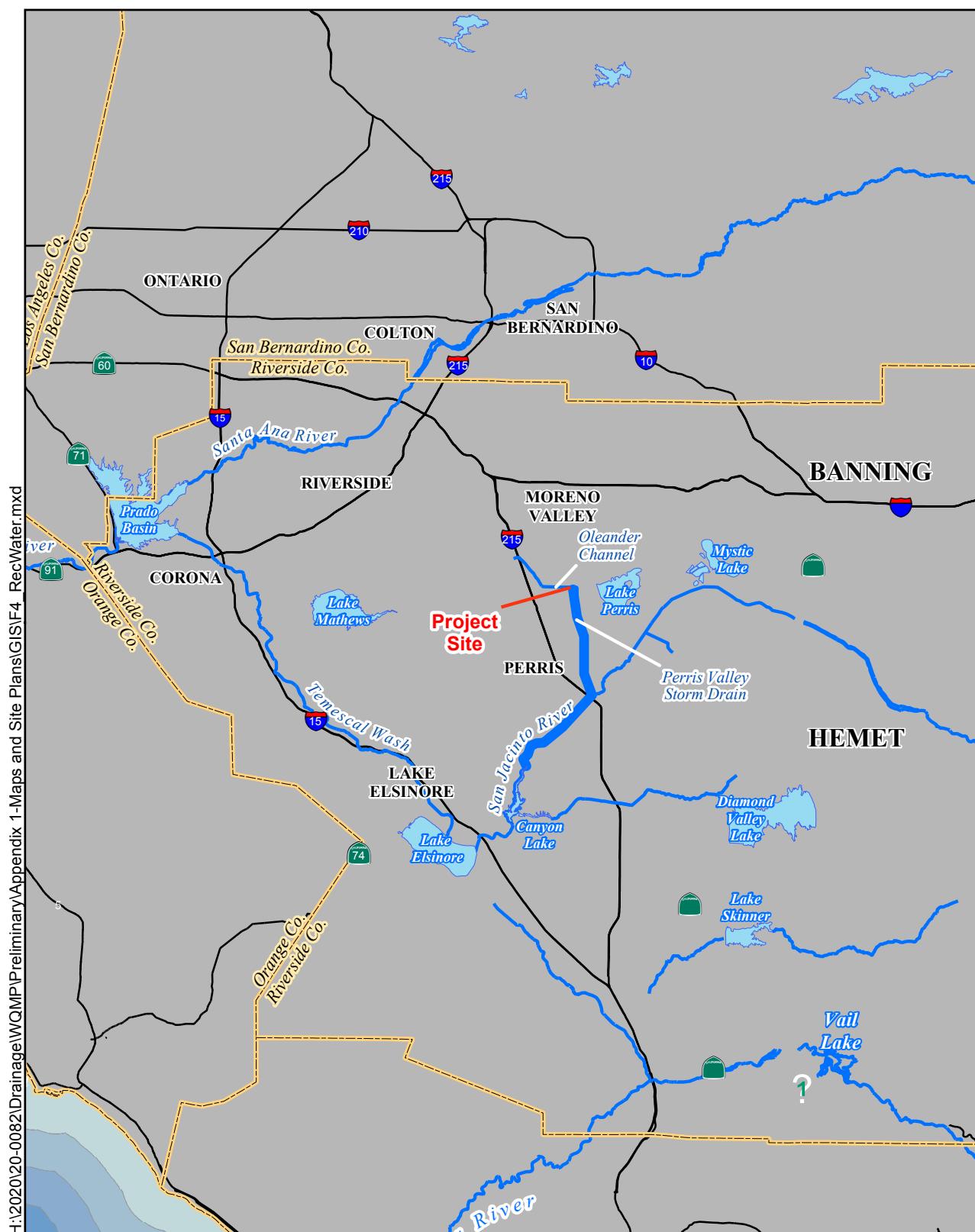


Figure 3. Aerial Photograph

0 400 800
Feet





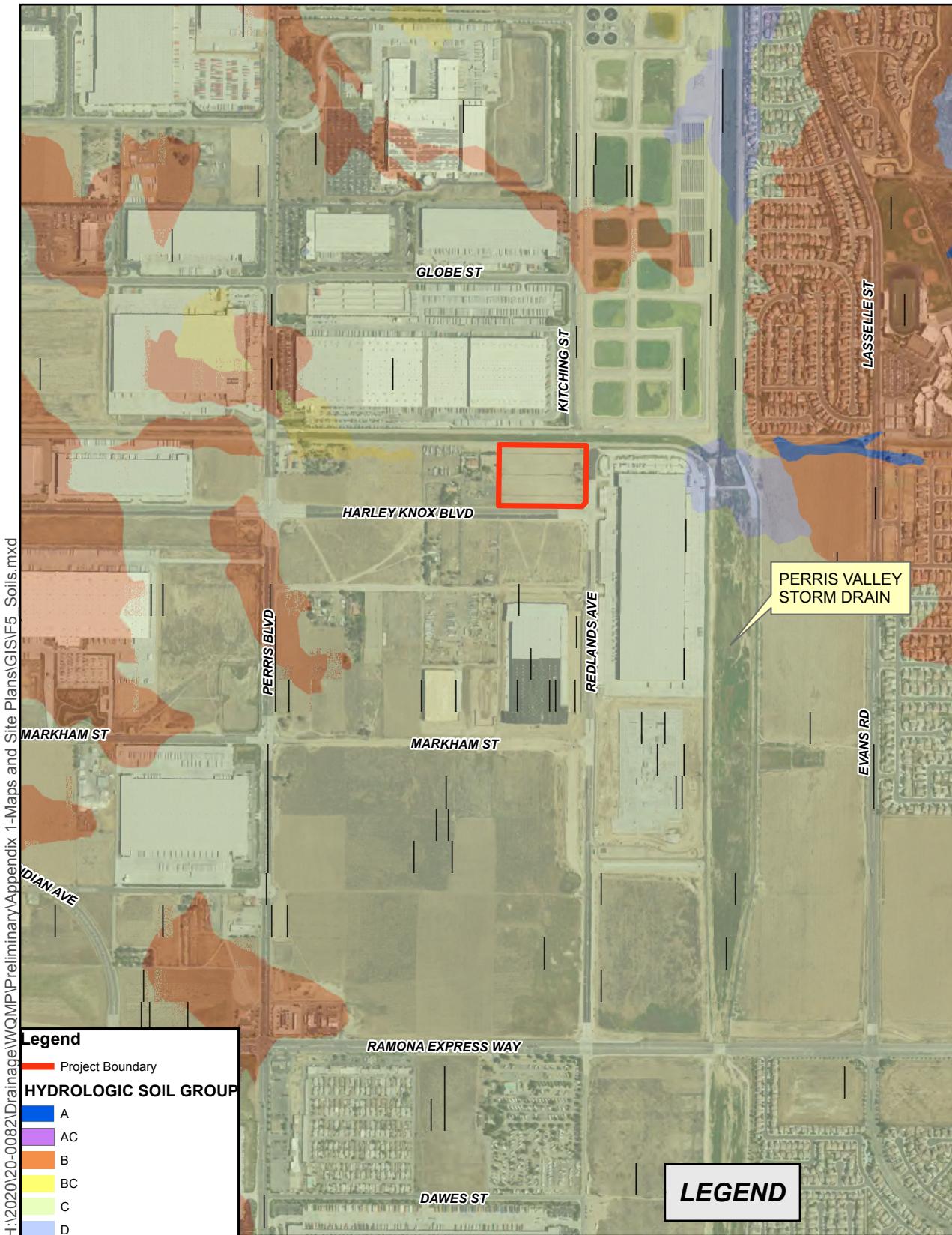
Sources: USGS 30 Meter DEM;
USGS Digital Line Graph

Figure 4. Receiving Waterbodies

0 2 4 6 Miles

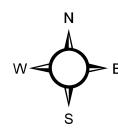


Flowpath



Riverside County GIS, 2016

RCFC&WCD Hydology Manual Plate C-1.30



0 500 1,000
Feet

Figure 5. Soils Map

SECTION 2 - HYDROLOGY ANALYSIS

HYDROLOGY PARAMETERS

The RCFC&WCD Hydrology Manual was used to determine several of the hydrological parameters. The following rainfall depths were utilized in the hydrology analyses, which were obtained from the isohyetal maps provided in the RCFC&WCD Hydrology Manual:

Table 1 – Precipitation Values

Storm Event	Duration
	1-Hour (inches)
10-Year	0.78
100-Year	1.12

The value for slope of intensity was determined to be 0.49. The isohyetal maps have been included in Appendix A.

Based on the Plate C-1.30 (Perris) in the RCFC&WCD Hydrology Manual, the project site is classified as soil type C. The soils map is included in Appendix A.

The residential\commercial landscaping cover type was used to represent the developed condition. Table 2 below summarizes the runoff index values and the recommended values for percentage of impervious cover for each category:

Table 2 – Cover Type

Cover Type	Soil Group A	Soil Group B	Soil Group C	Soil Group D	Percentage of Impervious Cover
Commercial Landscaping	32	56	69	75	90%

ON-SITE RATIONAL METHOD HYDROLOGY

The rational method was used to determine peak flow rates in order to adequately size the proposed subsurface storm drains and associated inlets used to convey on-site flows to the proposed underground storage chambers. The project site was separated into four subareas. Subarea 1 (5.6 acres) is essentially the northerly half of the site and is tributary to inlet 102. Subarea 2 (0.9 acres) is the northerly half of the eastern parking area and is tributary to inlet 202. Subarea 3 (0.3 acres) is the southerly half of the eastern parking area and is tributary to inlet 302. Subarea 4 (2.4 acres) is the southerly half of the site and is tributary to inlet 402. The project is comprised of approximately 15% pervious cover (landscaping). The project was modeled as commercial land use which assumes a 10% pervious cover which is slightly more conservative than what is proposed. As previously described, the underground storage chambers will utilize an outlet structure where high flow will gravity feed to the existing Lat D-3A line located in

Harley Knox Boulevard. Low flows from the underground storage chambers will discharge to a Contech Filterra unit for water quality treatment.

The rational method was used to determine peak flow rates in order to adequately size the proposed subsurface storm drains and associated inlets used to convey on-site flows through the site and into the existing Lat D-3A storm drain. The project site area was divided into 4 subareas.

Area-1 (approximately 5.6 acres) surface flows into a trench drain along the truck docking stalls. A 100-year peak flow of 14.3 cfs is generated by this subarea. The runoff will be conveyed around the building towards Area-2 using Line-A.

Area-2 (approximately 0.9 acres) surface flows into 1 low point on the east side of the project. A 100-year peak flow of 2.3 cfs is generated by this subarea. The runoff will be conveyed towards the underground storage chambers using Lat A-1.

Area-3 (approximately 0.3 acres) surface flows into 1 low point on the east side of the project. A 100-year peak flow of 1.0 cfs is generated by this subarea. The runoff will be conveyed towards the underground storage chambers using Lat A-2.

Area-4 (approximately 2.4 acres) surface flows into several low points on the south side of the project. A 100-year peak flow of 8.0 cfs is generated by this subarea. The runoff will be conveyed towards the underground storage chambers using Line-B.

A peak 100 year flow rate of 23.7 cfs is generated by the site, including the off-site areas and underground storage area. An emergency escape route will be provided capable of bypassing the peak 100 year flow rate.

The following table summarizes the rational method results at key points:

Table 3 – Rational Method Results

Point of Interest	10-Year Peak Flow Rate (cfs)	100-Year Peak Flow Rate (cfs)
Node 102 – Flow tributary to proposed inlet and Line A	9.9	14.3
Node 103 – Total Flow tributary to line A	16.4	23.7
Node 202 – Flow tributary to proposed inlet and Lat A-1	1.6	2.3
Node 203 – Total Flow tributary to Lat A-1	16.4	23.7
Node 302 – Flow tributary to proposed inlet and Lat A-2	0.7	1.0
Node 303 – Total Flow tributary to Lat A-2	16.4	23.7
Node 402 – Flow tributary to proposed inlet and Line B	5.8	8.0
Node 403 – Total Flow tributary to Line B	16.4	23.7

The rational method output files and hydrology map have been included in Appendix A.

SECTION 3 - HYDRAULIC ANALYSIS

ON-SITE STORM DRAIN FACILITIES

The project proposes minimal subsurface storm drain and will utilize curb and gutter and ribbon gutters to convey onsite high flows to the proposed underground storage chamber. The proposed underground storage chambers will receive the runoff generated by 9.5 acres of the site primarily on the easterly side of the site for water quality treatment.

The project proposes one subsurface storm drain system to convey on-site flows. The runoff will discharge into the underground storage chambers. The discharge from the underground storage chambers will be conveyed to a pump facility where it will outflow for water quality purposes. High flows discharged from the underground storage chambers will gravity flow to the existing Line D-3A located in Harley Knox Boulevard.

A brief summary of each system has been provided and the results of the hydraulic analyses are included at the end of the section. The peak flow rates determined during the 100-year rational method on-site hydrology analysis were utilized to evaluate the proposed storm drain systems.

Line-A (Onsite)

The north portion of the project site will surface flow to a trench drain along the truck docking stalls and be collected by Line A-1, a 24" HDPE pipe. Line-A proposes to convey the 100-year peak flow rate to the underground storage chamber. A hydraulic model for Line A-1 will be provided during final engineering to further assess the storm drain design.

Line-B (Onsite)

The south portion of the project site will surface flow to several low points in the south side landscaping area and be collected by Line B-1, a 24" HDPE pipe. Line-B proposes to convey the 100-year peak flow rate to the underground storage chamber. A hydraulic model for Line B-1 will be provided during final engineering to further assess the storm drain design.

OFF-SITE STORM DRAIN FACILITIES

As part of this project, the only offsite improvements proposed for Harley Knox Blvd include the construction of a driveway and sidewalk along the project frontage. There is an existing low point (Lat D-3A-4), within Harley Knox Boulevard. A 30" RCP offsite storm drain connection is proposed to convey all collected, onsite flows towards the existing 48" RCP lateral D-3A located along Harley Knox Boulevard. A peak flow rate of 21.1 cfs is expected per the rational method analysis (See Section 2 and Appendix A for more detail).

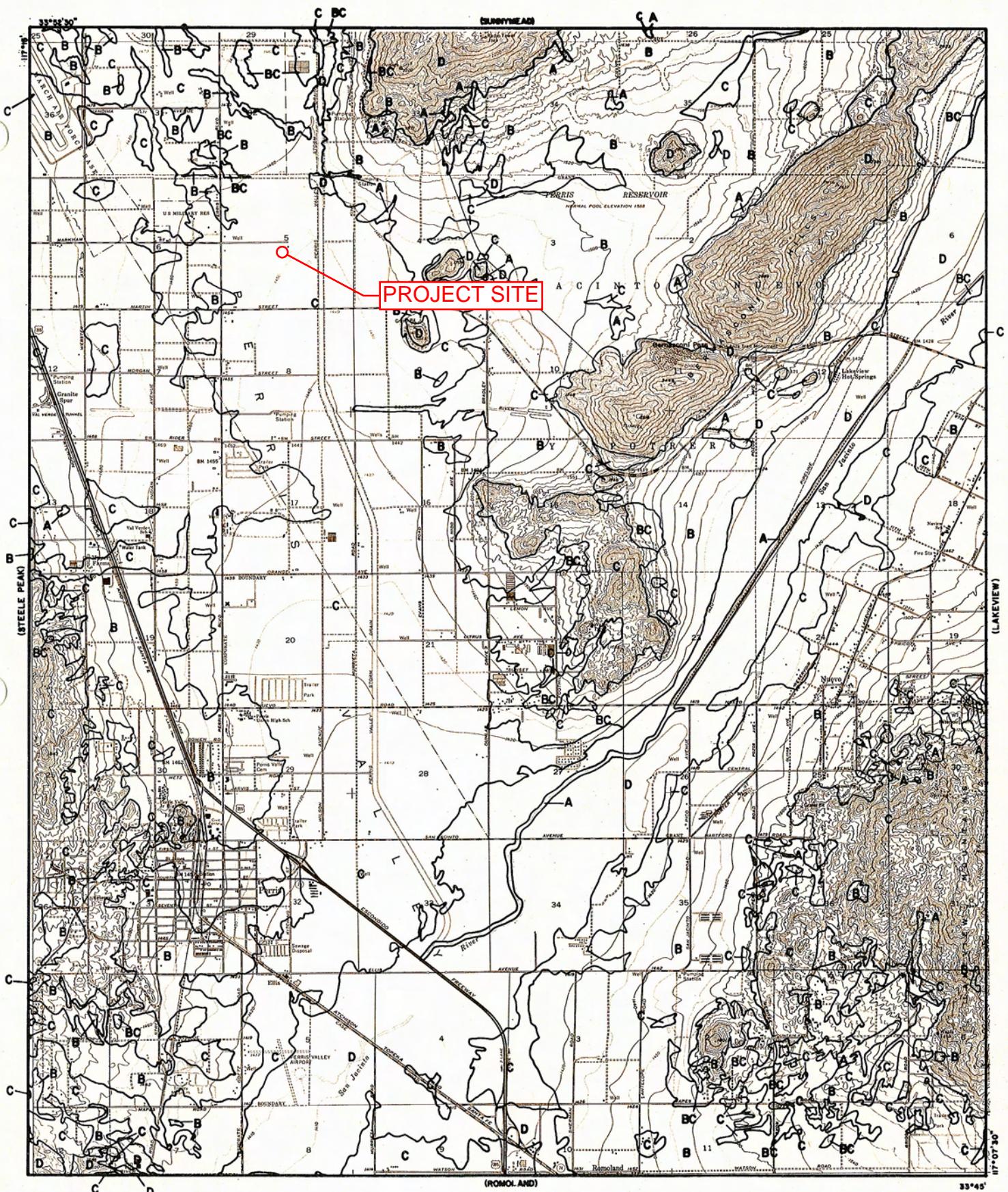
SECTION 4 - CONCLUSION

Based on the analyses and results of this report, the following conclusions were derived from the hydrology and hydraulic results:

- The proposed drainage improvements will adequately convey flows to the underground storage chambers and provide flood protection for the 100-year storm event.
- The proposed Contech Filterra unit will provide adequate water quality treatment.
- The proposed project will not impact flooding condition to upstream or downstream properties.

APPENDIX A – HYDROLOGY

HYDROLOGIC SOILS GROUP MAP (PLATE C-1.30)



LEGEND

- SOILS GROUP BOUNDARY
- A SOILS GROUP DESIGNATION

RCFC & WCD

HYDROLOGY MANUAL



0 FEET 5000

HYDROLOGIC SOILS GROUP MAP FOR

PERRIS

ISOHYETAL MAPS

RAINFALL INTENSITY-INCHES PER HOUR

R C F C & W C D
HYDROLOGY MANUAL

**STANDARD
INTENSITY-DURATION
CURVES DATA**

PLATE D-4.1 (4 of 6)

MIRA LOMA				MURRIETA - TEMECULA & RANCHO CALIFORNIA				NORCO				PALM SPRINGS				PERRIS VALLEY			
DURATION MINUTES	FREQUENCY		DURATION MINUTES	FREQUENCY		DURATION MINUTES	FREQUENCY		DURATION MINUTES	FREQUENCY		DURATION MINUTES	FREQUENCY		DURATION MINUTES	FREQUENCY			
	10 YEAR	100 YEAR		10 YEAR	100 YEAR		10 YEAR	100 YEAR		10 YEAR	100 YEAR		10 YEAR	100 YEAR		10 YEAR	100 YEAR		
5	2.84	4.48	5	3.45	5.10	5	2.77	4.16	5	4.23	6.76	5	2.64	3.78					
6	2.58	4.07	6	3.12	4.61	6	2.53	3.79	6	3.80	6.08	6	2.41	3.46					
7	2.37	3.75	7	2.87	4.24	7	2.34	3.51	7	3.48	5.56	7	2.24	3.21					
8	2.21	3.49	8	2.67	3.94	8	2.19	3.29	8	3.22	5.15	8	2.09	3.01					
9	2.08	3.28	9	2.50	3.69	9	2.07	3.10	9	3.01	4.81	9	1.98	2.84					
10	1.96	3.10	10	2.36	3.48	10	1.96	2.94	10	2.83	4.52	10	1.88	2.69					
11	1.87	2.95	11	2.24	3.30	11	1.87	2.80	11	2.67	4.28	11	1.79	2.57					
12	1.78	2.82	12	2.13	3.15	12	1.79	2.68	12	2.54	4.07	12	1.72	2.46					
13	1.71	2.70	13	2.04	3.01	13	1.72	2.58	13	2.43	3.88	13	1.65	2.37					
14	1.64	2.60	14	1.96	2.89	14	1.66	2.48	14	2.33	3.72	14	1.59	2.29					
15	1.58	2.50	15	1.89	2.79	15	1.60	2.40	15	2.23	3.58	15	1.54	2.21					
16	1.53	2.42	16	1.82	2.69	16	1.55	2.32	16	2.15	3.44	16	1.49	2.14					
17	1.48	2.34	17	1.76	2.60	17	1.50	2.25	17	2.08	3.32	17	1.45	2.08					
18	1.44	2.27	18	1.71	2.52	18	1.46	2.19	18	2.01	3.22	18	1.41	2.02					
19	1.40	2.21	19	1.66	2.45	19	1.42	2.13	19	1.95	3.12	19	1.37	1.97					
20	1.36	2.15	20	1.61	2.38	20	1.39	2.08	20	1.89	3.03	20	1.34	1.92					
22	1.29	2.04	22	1.53	2.26	22	1.32	1.98	22	1.79	2.86	22	1.28	1.83					
24	1.24	1.95	24	1.46	2.15	24	1.26	1.90	24	1.70	2.72	24	1.22	1.75					
26	1.18	1.87	26	1.39	2.06	26	1.22	1.82	26	1.62	2.60	26	1.18	1.69					
28	1.14	1.80	28	1.34	1.98	28	1.17	1.76	28	1.56	2.49	28	1.13	1.63					
30	1.10	1.73	30	1.29	1.90	30	1.13	1.70	30	1.49	2.39	30	1.10	1.57					
32	1.06	1.67	32	1.24	1.84	32	1.10	1.64	32	1.44	2.30	32	1.06	1.52					
34	1.03	1.62	34	1.20	1.78	34	1.06	1.59	34	1.39	2.22	34	1.03	1.48					
36	1.00	1.57	36	1.17	1.72	36	1.03	1.55	36	1.34	2.15	36	1.00	1.44					
38	.97	1.53	38	1.13	1.67	38	1.01	1.51	38	1.30	2.09	38	.98	1.40					
40	.94	1.49	40	1.10	1.62	40	.98	1.47	40	1.27	2.02	40	.95	1.37					
45	.89	1.40	45	1.03	1.52	45	.92	1.39	45	1.18	1.89	45	.90	1.29					
50	.84	1.32	50	.97	1.44	50	.88	1.31	50	1.11	1.78	50	.85	1.22					
55	.80	1.26	55	.92	1.36	55	.84	1.25	55	1.05	1.68	55	.81	1.17					
60	.76	1.20	60	.88	1.30	60	.80	1.20	60	1.00	1.60	60	.78	1.12					
65	.73	1.15	65	.84	1.24	65	.77	1.15	65	.95	1.53	65	.75	1.08					
70	.70	1.11	70	.81	1.19	70	.74	1.11	70	.91	1.46	70	.72	1.04					
75	.68	1.07	75	.78	1.15	75	.72	1.07	75	.88	1.41	75	.70	1.00					
80	.65	1.03	80	.75	1.11	80	.69	1.04	80	.85	1.35	80	.68	.97					
85	.63	1.00	85	.73	1.07	85	.67	1.01	85	.82	1.31	85	.66	.94					

SLOPE = .530

SLOPE = .550

SLOPE = .500

SLOPE = .580

SLOPE = .490

10-YEAR ONSITE HYDROLOGY (RATIONAL METHOD)

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
Rational Hydrology Study Date: 08/12/21 File:prop10.out

20-0082 - FIR HK
ONSITE RATIONAL METHOD HYDROLOGY
10 YEAR STORM EVENT
FN: PROP10.OUT RC

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 4010

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)

For the [Perris Valley] area used.

10 year storm 10 minute intensity = 1.880(In/Hr)

10 year storm 60 minute intensity = 0.780(In/Hr)

100 year storm 10 minute intensity = 2.690(In/Hr)

100 year storm 60 minute intensity = 1.120(In/Hr)

Storm event year = 10.0

Calculated rainfall intensity data:

1 hour intensity = 0.780(In/Hr)

Slope of intensity duration curve = 0.4900

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 363.000(Ft.)
Top (of initial area) elevation = 1459.100(Ft.)
Bottom (of initial area) elevation = 1456.800(Ft.)

Difference in elevation = 2.300(Ft.)
Slope = 0.00634 s(percent)= 0.63
TC = $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Initial area time of concentration = 8.724 min.
Rainfall intensity = 2.006(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.879
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 9.880(CFS)
Total initial stream area = 5.600(Ac.)
Pervious area fraction = 0.100

++++++
Process from Point/Station 102.000 to Point/Station 103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.900(Ft.)
Downstream point/station elevation = 1450.300(Ft.)
Pipe length = 512.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 9.880(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 9.880(CFS)
Normal flow depth in pipe = 17.81(In.)
Flow top width inside pipe = 15.07(In.)
Critical Depth = 14.04(In.)
Pipe flow velocity = 4.54(Ft/s)
Travel time through pipe = 1.88 min.
Time of concentration (TC) = 10.60 min.

++++++
Process from Point/Station 102.000 to Point/Station 103.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 5.600(Ac.)
Runoff from this stream = 9.880(CFS)
Time of concentration = 10.60 min.
Rainfall intensity = 1.823(In/Hr)

++++++
Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

```
Initial area flow distance = 395.000(Ft.)
Top (of initial area) elevation = 1460.100(Ft.)
Bottom (of initial area) elevation = 1457.400(Ft.)
Difference in elevation = 2.700(Ft.)
Slope = 0.00684 s(percent)= 0.68
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.888 min.
Rainfall intensity = 1.988(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.879
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 1.573(CFS)
Total initial stream area = 0.900(Ac.)
Pervious area fraction = 0.100
```

```
+++++
Process from Point/Station 202.000 to Point/Station 203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation = 1451.800(Ft.)
Downstream point/station elevation = 1451.500(Ft.)
Pipe length = 29.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 1.573(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.573(CFS)
Normal flow depth in pipe = 6.45(In.)
Flow top width inside pipe = 8.11(In.)
Critical Depth = 6.93(In.)
Pipe flow velocity = 4.64(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) = 8.99 min.
```

```
+++++
Process from Point/Station 202.000 to Point/Station 203.000
**** CONFLUENCE OF MINOR STREAMS ****
```

```
Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.900(Ac.)
Runoff from this stream = 1.573(CFS)
Time of concentration = 8.99 min.
Rainfall intensity = 1.977(In/Hr)
```

+++++
Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 120.000(Ft.)
Top (of initial area) elevation = 1461.000(Ft.)
Bottom (of initial area) elevation = 1458.600(Ft.)
Difference in elevation = 2.400(Ft.)
Slope = 0.02000 s(percent)= 2.00
TC = $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Warning: TC computed to be less than 5 min.; program is assuming the time of concentration is 5 minutes.
Initial area time of concentration = 5.000 min.
Rainfall intensity = 2.636(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.883
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 0.698(CFS)
Total initial stream area = 0.300(Ac.)
Pervious area fraction = 0.100

+++++
Process from Point/Station 302.000 to Point/Station 303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.800(Ft.)
Downstream point/station elevation = 1451.500(Ft.)
Pipe length = 41.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 0.698(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.698(CFS)
Normal flow depth in pipe = 4.27(In.)
Flow top width inside pipe = 8.99(In.)
Critical Depth = 4.56(In.)
Pipe flow velocity = 3.39(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 5.20 min.

+++++
Process from Point/Station 302.000 to Point/Station 303.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.300(Ac.)
Runoff from this stream = 0.698(CFS)
Time of concentration = 5.20 min.
Rainfall intensity = 2.585(In/Hr)

+++++
Process from Point/Station 401.000 to Point/Station 402.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 171.000(Ft.)
Top (of initial area) elevation = 1462.100(Ft.)
Bottom (of initial area) elevation = 1458.300(Ft.)
Difference in elevation = 3.800(Ft.)
Slope = 0.02222 s(percent)= 2.22
TC = $k(0.300)*[(length^3)/(elevation change)]^{0.2}$
Initial area time of concentration = 5.023 min.
Rainfall intensity = 2.630(In/Hr) for a 10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.883
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 5.575(CFS)
Total initial stream area = 2.400(Ac.)
Pervious area fraction = 0.100

+++++
Process from Point/Station 402.000 to Point/Station 403.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1454.200(Ft.)
Downstream point/station elevation = 1451.300(Ft.)
Pipe length = 597.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 5.575(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 5.575(CFS)
Normal flow depth in pipe = 11.13(In.)
Flow top width inside pipe = 17.49(In.)
Critical Depth = 10.93(In.)
Pipe flow velocity = 4.86(Ft/s)
Travel time through pipe = 2.05 min.
Time of concentration (TC) = 7.07 min.

+++++
 Process from Point/Station 402.000 to Point/Station 403.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4

Stream flow area = 2.400(Ac.)

Runoff from this stream = 5.575(CFS)

Time of concentration = 7.07 min.

Rainfall intensity = 2.224(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	9.880	10.60	1.823
2	1.573	8.99	1.977
3	0.698	5.20	2.585
4	5.575	7.07	2.224

Largest stream flow has longer time of concentration

$Q_p = 9.880 + \text{sum of}$

$$Q_b \quad I_a/I_b \\ 1.573 * 0.922 = 1.451$$

$$Q_b \quad I_a/I_b \\ 0.698 * 0.705 = 0.493$$

$$Q_b \quad I_a/I_b \\ 5.575 * 0.820 = 4.571$$

$Q_p = 16.394$

Total of 4 streams to confluence:

Flow rates before confluence point:

9.880 1.573 0.698 5.575

Area of streams before confluence:

5.600 0.900 0.300 2.400

Results of confluence:

Total flow rate = 16.394(CFS)

Time of concentration = 10.604 min.

Effective stream area after confluence = 9.200(Ac.)

End of computations, total study area = 9.20 (Ac.)

The following figures may
 be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(A_p) = 0.100

Area averaged RI index number = 69.0

100-YEAR ONSITE HYDROLOGY (RATIONAL METHOD)

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
Rational Hydrology Study Date: 08/12/21 File:prop100.out

20-0082 - FIR HK
ONSITE RATIONAL METHOD HYDROLOGY
100 YEAR STORM EVENT
FN: PROP100.OUT RC

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 4010

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)
For the [Perris Valley] area used.

10 year storm 10 minute intensity = 1.880(In/Hr)
10 year storm 60 minute intensity = 0.780(In/Hr)
100 year storm 10 minute intensity = 2.690(In/Hr)
100 year storm 60 minute intensity = 1.120(In/Hr)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.120(In/Hr)
Slope of intensity duration curve = 0.4900

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 363.000(Ft.)
Top (of initial area) elevation = 1459.100(Ft.)
Bottom (of initial area) elevation = 1456.800(Ft.)

Difference in elevation = 2.300(Ft.)
Slope = 0.00634 s(percent)= 0.63
TC = $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Initial area time of concentration = 8.724 min.
Rainfall intensity = 2.881(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.885
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 14.271(CFS)
Total initial stream area = 5.600(Ac.)
Pervious area fraction = 0.100

++++++
Process from Point/Station 102.000 to Point/Station 103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.900(Ft.)
Downstream point/station elevation = 1450.300(Ft.)
Pipe length = 512.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 14.271(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 14.271(CFS)
Normal flow depth in pipe = 20.72(In.)
Flow top width inside pipe = 16.49(In.)
Critical Depth = 16.33(In.)
Pipe flow velocity = 4.95(Ft/s)
Travel time through pipe = 1.72 min.
Time of concentration (TC) = 10.45 min.

++++++
Process from Point/Station 102.000 to Point/Station 103.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 5.600(Ac.)
Runoff from this stream = 14.271(CFS)
Time of concentration = 10.45 min.
Rainfall intensity = 2.637(In/Hr)

++++++
Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

```
Initial area flow distance = 395.000(Ft.)
Top (of initial area) elevation = 1460.100(Ft.)
Bottom (of initial area) elevation = 1457.400(Ft.)
Difference in elevation = 2.700(Ft.)
Slope = 0.00684 s(percent)= 0.68
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.888 min.
Rainfall intensity = 2.855(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.884
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 2.272(CFS)
Total initial stream area = 0.900(Ac.)
Pervious area fraction = 0.100
```

```
#####
Process from Point/Station 202.000 to Point/Station 203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation = 1451.800(Ft.)
Downstream point/station elevation = 1451.500(Ft.)
Pipe length = 29.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 2.272(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.272(CFS)
Normal flow depth in pipe = 6.55(In.)
Flow top width inside pipe = 11.95(In.)
Critical Depth = 7.73(In.)
Pipe flow velocity = 5.18(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 8.98 min.
```

```
#####
Process from Point/Station 202.000 to Point/Station 203.000
**** CONFLUENCE OF MINOR STREAMS ****
```

```
Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.900(Ac.)
Runoff from this stream = 2.272(CFS)
Time of concentration = 8.98 min.
Rainfall intensity = 2.840(In/Hr)
```

+++++
Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 120.000(Ft.)
Top (of initial area) elevation = 1461.000(Ft.)
Bottom (of initial area) elevation = 1458.600(Ft.)
Difference in elevation = 2.400(Ft.)
Slope = 0.02000 s(percent)= 2.00
TC = $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Warning: TC computed to be less than 5 min.; program is assuming the time of concentration is 5 minutes.
Initial area time of concentration = 5.000 min.
Rainfall intensity = 3.785(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.888
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 1.008(CFS)
Total initial stream area = 0.300(Ac.)
Pervious area fraction = 0.100

+++++
Process from Point/Station 302.000 to Point/Station 303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.800(Ft.)
Downstream point/station elevation = 1451.500(Ft.)
Pipe length = 41.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 1.008(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.008(CFS)
Normal flow depth in pipe = 5.33(In.)
Flow top width inside pipe = 8.85(In.)
Critical Depth = 5.53(In.)
Pipe flow velocity = 3.70(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 5.18 min.

+++++
Process from Point/Station 302.000 to Point/Station 303.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.300(Ac.)
Runoff from this stream = 1.008(CFS)
Time of concentration = 5.18 min.
Rainfall intensity = 3.718(In/Hr)

+++++
Process from Point/Station 401.000 to Point/Station 402.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 171.000(Ft.)
Top (of initial area) elevation = 1462.100(Ft.)
Bottom (of initial area) elevation = 1458.300(Ft.)
Difference in elevation = 3.800(Ft.)
Slope = 0.02222 s(percent)= 2.22
TC = $k(0.300)*[(length^3)/(elevation change)]^{0.2}$
Initial area time of concentration = 5.023 min.
Rainfall intensity = 3.776(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.888
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff = 8.045(CFS)
Total initial stream area = 2.400(Ac.)
Pervious area fraction = 0.100

+++++
Process from Point/Station 402.000 to Point/Station 403.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1454.200(Ft.)
Downstream point/station elevation = 1451.300(Ft.)
Pipe length = 597.00(Ft.) Manning's N = 0.012
No. of pipes = 1 Required pipe flow = 8.045(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 8.045(CFS)
Normal flow depth in pipe = 15.00(In.)
Flow top width inside pipe = 13.42(In.)
Critical Depth = 13.18(In.)
Pipe flow velocity = 5.11(Ft/s)
Travel time through pipe = 1.95 min.
Time of concentration (TC) = 6.97 min.

+++++
Process from Point/Station 402.000 to Point/Station 403.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4

Stream flow area = 2.400(Ac.)

Runoff from this stream = 8.045(CFS)

Time of concentration = 6.97 min.

Rainfall intensity = 3.216(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	14.271	10.45	2.637
2	2.272	8.98	2.840
3	1.008	5.18	3.718
4	8.045	6.97	3.216

Largest stream flow has longer time of concentration

$Q_p = 14.271 + \text{sum of}$

$$Q_b \quad I_a/I_b \\ 2.272 * 0.929 = 2.110$$

$$Q_b \quad I_a/I_b \\ 1.008 * 0.709 = 0.715$$

$$Q_b \quad I_a/I_b \\ 8.045 * 0.820 = 6.597$$

$Q_p = 23.693$

Total of 4 streams to confluence:

Flow rates before confluence point:

14.271 2.272 1.008 8.045

Area of streams before confluence:

5.600 0.900 0.300 2.400

Results of confluence:

Total flow rate = 23.693(CFS)

Time of concentration = 10.448 min.

Effective stream area after confluence = 9.200(Ac.)

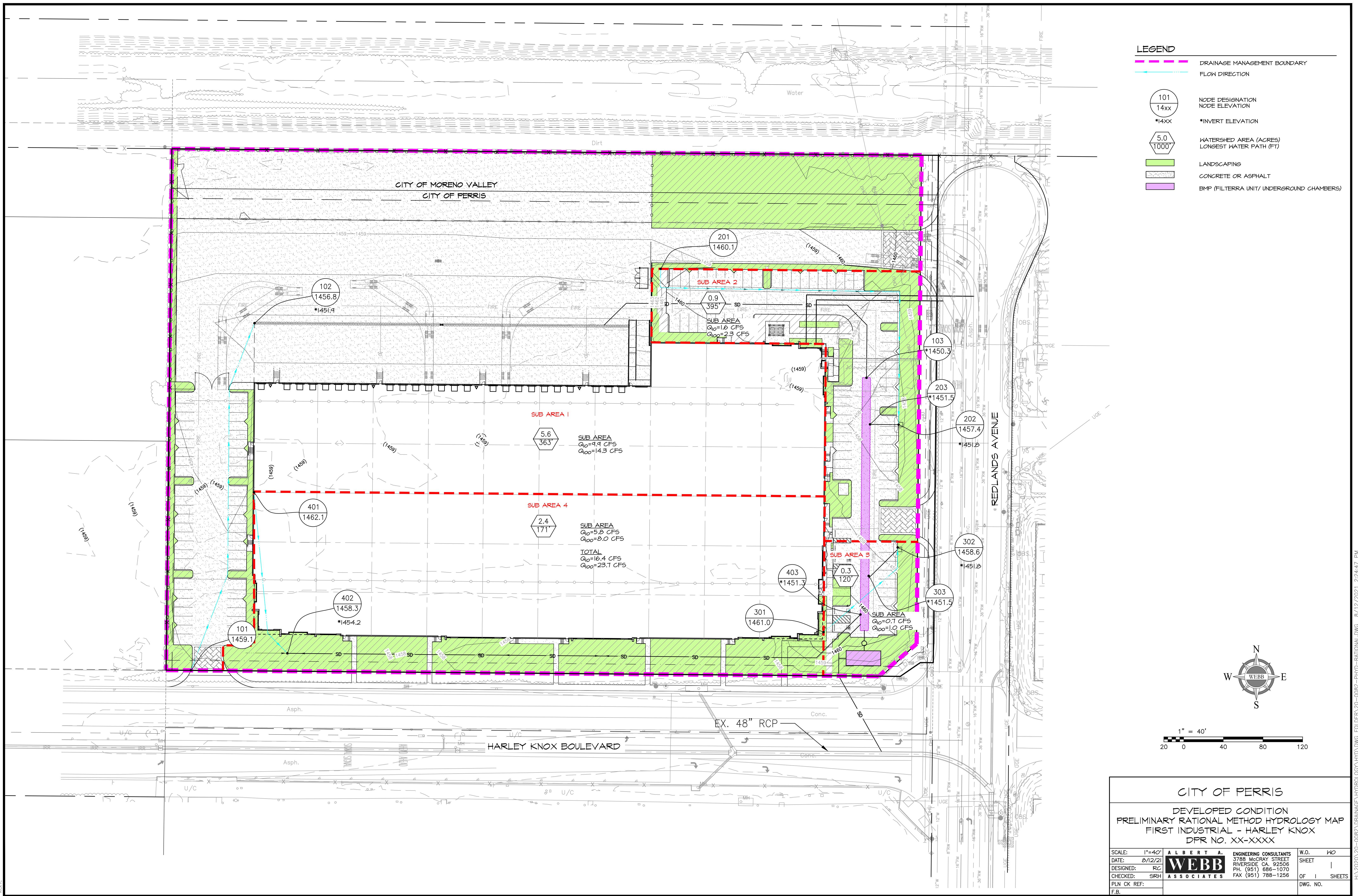
End of computations, total study area = 9.20 (Ac.)

The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(A_p) = 0.100

Area averaged RI index number = 69.0

HYDROLOGY MAPS



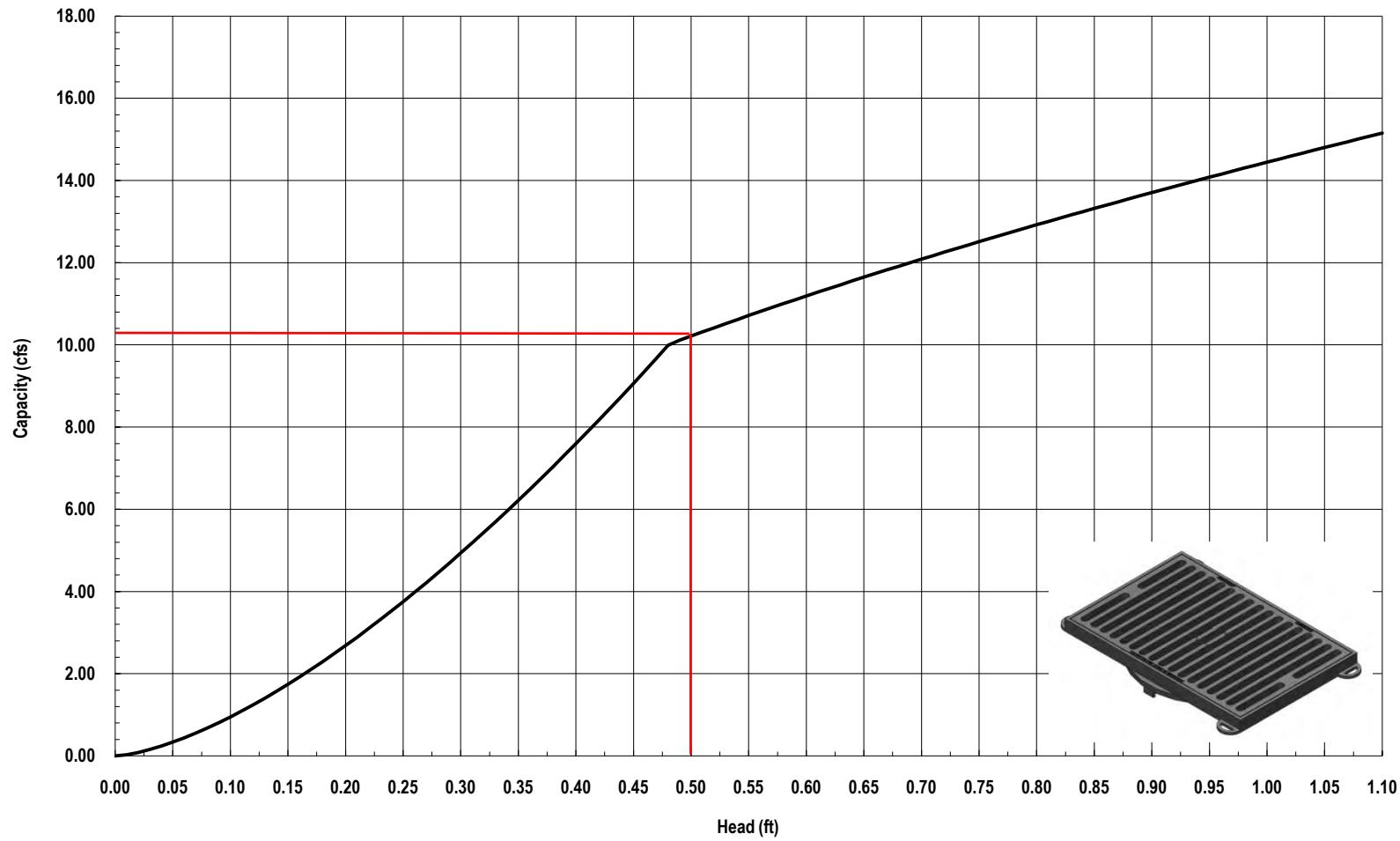
APPENDIX B – HYDRAULICS

HYDRAULIC CALCULATIONS

Hydraulic calculations to be provided in Final Engineering.

INLET AND CATCH BASIN CALCULATIONS

Nyloplast 2' x 3' Road & Highway Grate Inlet Capacity Chart



Nyloplast®

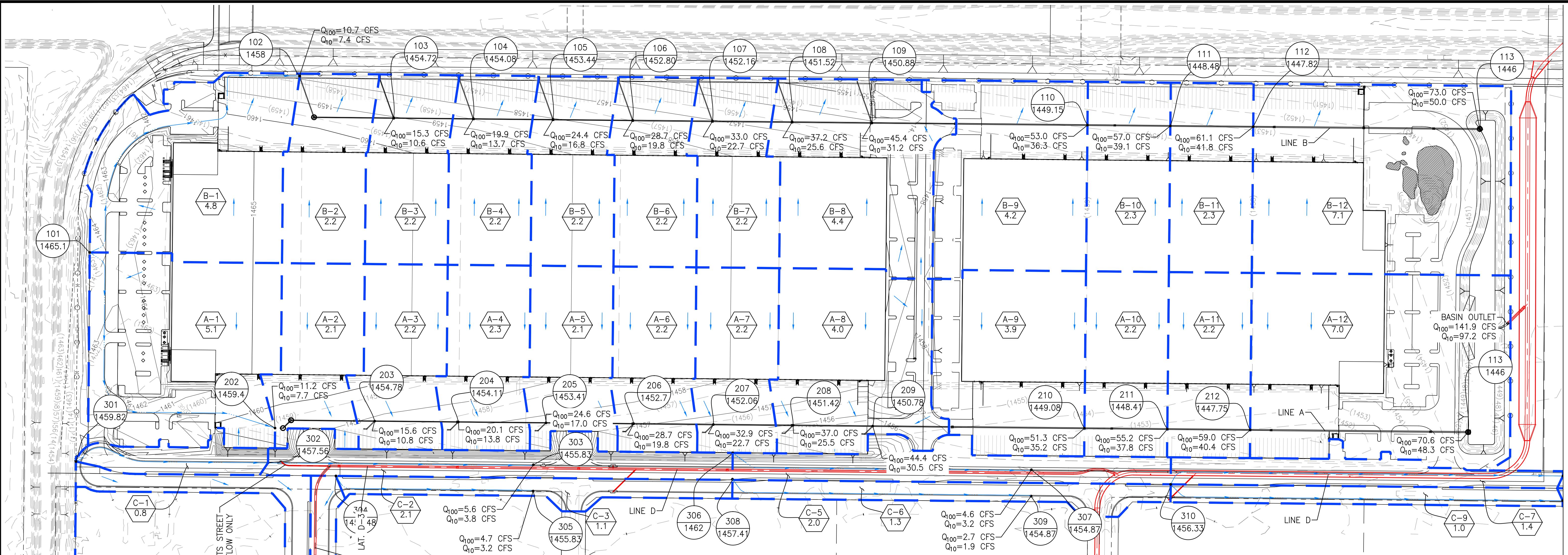
3130 Verona Avenue • Buford, GA 30518
(866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490
© Nyloplast Inlet Capacity Charts June 2012

APPENDIX C – REFERENCES

PERRIS VALLEY MDP LAT D-3A PLANS

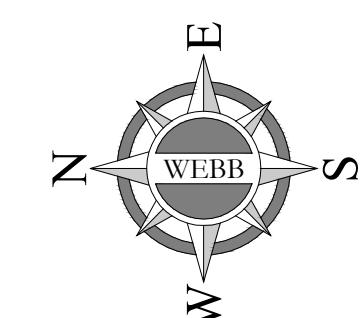
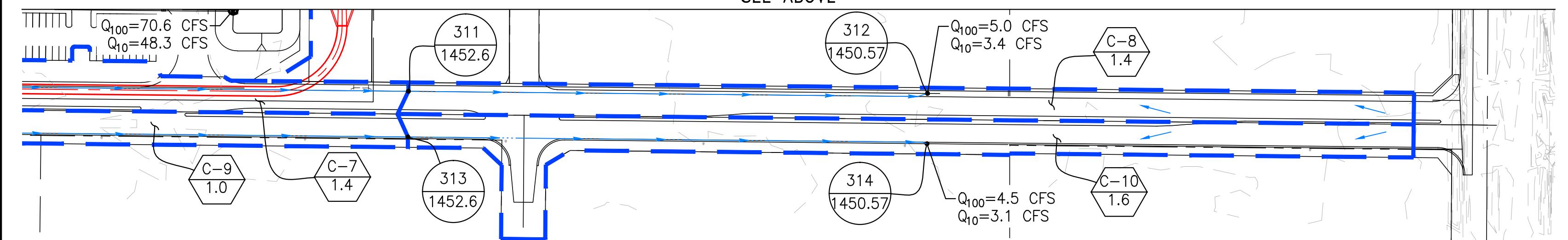
REDLANDS AVE. HYDROLOGY (CONT.)

SEE BELOW

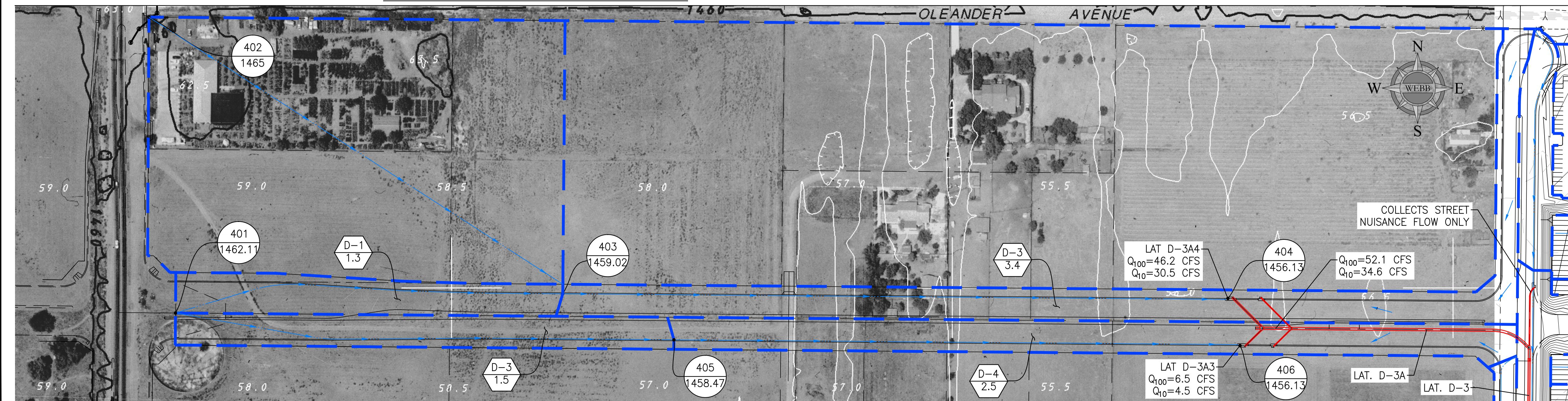


REDLANDS AVE. HYDROLOGY (CONT.)

SEE ABOVE



HARLEY KNOX BLVD. HYDROLOGY



LEGEND

- WATERSHED BOUNDARY
- WATER COURSE
- FLOW DIRECTION
- NODE ELEVATION
- SUBAREA DESIGNATION
ACREAGE - ACRES

PROPOSED CONDITION HYDROLOGY MAP

STRATFORD RANCH INDUSTRIAL SITE ON-SITE & STREET HYDROLOGY

SCALE: 1"=120'	ALBERT A. WEBB ASSOCIATES	ENGINEERING CONSULTANTS	W.O. 13-0239
DATE: 12/6/2013	RIVERSIDE, CA 92506	3788 McCRAY STREET	
DESIGNED: CRC	PH. (951) 686-1070	FAX (951) 788-1256	
CHECKED: EA			
PLN CR REF:			
F.B.			
			SHEET 1 OF 1 SHEETS
			DWG. NO.

GENERAL NOTES

- IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER/OWNER CONTRACTOR TO APPLY TO THE CITY OF PERRIS ENGINEERING DEPARTMENT, PERMIT SECTION, FOR AN ENCROACHMENT PERMIT FOR ALL WORK PERFORMED WITHIN PUBLIC RIGHT-OF-WAY, DEDICATED AND ACCEPTED FOR PUBLIC USE; AND TO BE RESPONSIBLE FOR SATISFACTORY COMPLIANCE FOR ALL CURRENT ENVIRONMENTAL REGULATIONS DURING THE LIFE OF CONSTRUCTION ACTIVITIES FOR THIS PROJECT, ADDITIONAL STUDIES AND/OR PERMITS MAY BE REQUIRED.
- THE CONTRACTOR/DEVELOPER SHALL BE RESPONSIBLE FOR THE CLEARING OF THE WORK AREA, AND RELOCATION COSTS OF ALL EXISTING UTILITIES, THIS INCLUDES UNDERGROUNDING OF EXISTING OVERHEAD LINES ALONG THE PROJECT FRONTAGE AS REQUIRED BY THE CONDITIONS OF APPROVAL, PERMITTEE MUST INFORM CITY OF CONSTRUCTION SCHEDULE AT LEAST 48 HOURS PRIOR TO BEGINNING OF CONSTRUCTION, PHONE: (951) 943-6304.
- THE DEVELOPER WILL INSTALL STREET NAME SIGNS CONFORMING TO COUNTY STANDARD NO. 816 OR AS APPROVED BY THE CITY ENGINEER.
- ALL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE RIVERSIDE COUNTY TRANSPORTATION DEPARTMENT IMPROVEMENT STANDARDS AND SPECIFICATIONS, LATEST EDITION, COUNTY ORDINANCE NO. 461 AND SUBSEQUENT AMENDMENTS.
- IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER TO NOTIFY THE ENGINEER TO INSTALL STREET CENTERLINE MONUMENTS AS REQUIRED BY RIVERSIDE COUNTY ORDINANCE NO. 461 (TRACTS AND PARCEL MAPS ONLY). ALL EXISTING SURVEY MONUMENTS SHALL BE PROTECTED IN PLACE OR RELOCATED BY A LICENSED PROFESSIONAL PRIOR TO CONSTRUCTION.
- ALL UNDERGROUND FACILITIES, WITH LATERALS, SHALL BE IN PLACE PRIOR TO PAVING THE STREET, INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING: SEWER, WATER, ELECTRIC, GAS, STORM DRAINS.
- CURB DEPRESSIONS AND DRIVEWAY APPROACHES WILL BE INSTALLED AND CONSTRUCTED ACCORDING TO COUNTY STANDARD NO. 207A, AS DIRECTED IN THE FIELD AND AS APPROVED BY THE CITY ENGINEER.
- IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER OR CONTRACTOR TO INSTALL AND MAINTAIN ALL CONSTRUCTION, REGULATORY, GUIDE AND WARNING SIGNS WITHIN THE PROJECT LIMITS AND ITS SURROUNDINGS TO PROVIDE SAFE PASSAGE FOR THE TRAVELING PUBLIC AND WORKERS UNTIL THE FINAL COMPLETION AND ACCEPTANCE OF THE PROJECT BY THE CITY. A TRAFFIC CONTROL PLAN MUST BE SUBMITTED FOR REVIEW TO THE PERMITS SECTION OR INSPECTION SECTION PRIOR TO OBTAINING AN ENCROACHMENT PERMIT.
- ALL STREET SECTIONS ARE MINIMUM REQUIREMENTS. ADDITIONAL SOIL TESTS SHALL BE TAKEN AFTER ROUGH GRAVING TO DETERMINE THE RECOMMENDED STREET SECTION REQUIREMENTS. USE COUNTY STD. NO. 401 IF EXPANSIVE SOILS ARE ENCOUNTERED.
- ASPHALTIC EMULSION (FOG SEAL) SHALL BE APPLIED NOT LESS THAN FOURTEEN DAYS FOLLOWING PLACEMENT OF THE ASPHALT SURFACING. FOG SEAL AND PAINT BINDER SHALL BE APPLIED AT A RATE OF 0.05 AND 0.03 GALLON PER SQUARE YARD RESPECTIVELY. ASPHALTIC EMULSION SHALL CONFORM TO SECTION 37, 39 AND 94 OF THE STATE STANDARD SPECIFICATIONS.
- INSTALL STREET TREES IN ACCORDANCE WITH ORDINANCE NO. 461 AND THE COMPREHENSIVE LANDSCAPING GUIDELINES.
- STREET LIGHTS SHALL BE INSTALLED PER RIVERSIDE COUNTY STANDARDS AND IN ACCORDANCE WITH THE APPROVED STREET LIGHTING PLAN.
- AS DETERMINED BY THE CITY ENGINEER, THE DEVELOPER IS RESPONSIBLE AT A MINIMUM FOR ROAD IMPROVEMENTS TO CENTERLINE, AND MAY BE REQUIRED TO RECONSTRUCT EXISTING PAVEMENT, INCLUDING BASE, AND MATCHING OVERLAY REQUIRED TO MEET THE STRUCTURAL STANDARDS FOR THE CURRENT ASSIGNED TRAFFIC INDEX PER ENGINEERING CONDITION OF APPROVAL.
- ANY PRIVATE DRAINAGE FACILITIES SHOWN ON THESE PLANS ARE FOR INFORMATION ONLY. BY SIGNING THESE IMPROVEMENT PLANS, NO REVIEW OR APPROVAL OF THOSE PRIVATE FACILITIES IS IMPLIED OR INTENDED BY THE CITY OF PERRIS ENGINEERING DEPARTMENT.
- CONSTRUCTION PROJECTS MUST OBTAIN A NATIONAL POLLUTANT DISCHARGE ELIMINATION SYSTEM (NPDES) PERMIT. OWNERS/DEVELOPERS ARE REQUIRED TO FILE A NOTICE OF INTENT (NOI) WITH THE STATE WATER RESOURCES CONTROL BOARD (SWRCB), PREPARE A STORM WATER POLLUTION PREVENTION PLAN (SWPPP) AND MONITORING PLAN FOR THE SITE.
- PRIOR TO ANY CONSTRUCTION, THE DEVELOPER SHALL PROVIDE THE CITY A COPY OF THE NOI WITH A VALID WWD NUMBER.
- THE DEVELOPER SHALL BE RESPONSIBLE FOR THE INSTALLATION OF ADDITIONAL SIGNS AND MARKINGS NOT INCLUDED IN THE SIGNING AND STRIPING PLAN WITHIN THE PROJECT AREAS, OR ON ROADWAYS ADJACENT TO THE PROJECT BOUNDARIES, UPON THE REQUEST OF THE CITY ENGINEER OR HIS DESIGNEE TO IMPROVE TRAFFIC SAFETY ON THE ROADS UNDER THE JURISDICTION OF THE DEVELOPER.
- EXISTING STORM DRAIN PIPES / CULVERTS (WHETHER TO BE CONNECTED TO, EXTENDED, ADJUSTED, DRAINED TO, OR JUST IN THE PROJECT VICINITY) MUST BE REPAIRED, AND/OR CLEANED TO MAKE THEM FUNCTIONAL AND ACCEPTABLE APPROVED BY THE CITY ENGINEER.
- FOR ALL DRIVEWAY RECONSTRUCTION BEYOND RIGHT-OF-WAY, PROOF OF DRIVEWAY OWNER NOTIFICATION IS REQUIRED PRIOR TO CONSTRUCTION.
- IN THE EVENT OF ANY DAMAGE TO ADJACENT STREETS CAUSED BY THE CONSTRUCTION, CONTRACTOR SHALL REMOVE AND REPLACE DAMAGES AS DIRECTED BY CITY ENGINEER.

NOTICE TO CONTRACTORS

CONTRACTOR AGREES THAT HE SHALL ASSUME COMPLETE AND SOLE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY; THAT THIS REQUIREMENT SHALL CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS; AND THAT THE CONTRACTOR SHALL DEFEND, INDEMNIFY AND HOLD THE OWNER AND ENGINEER HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT, EXCEPTING FROM LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF THE OWNER OR ENGINEER.

UNDERGROUND STRUCTURES

ALL UNDERGROUND STRUCTURES OR UTILITIES REPORTED BY THE OWNER OR OTHERS AND THOSE SHOWN ON THE RECORDS EXAMINED ARE INDICATED WITH THEIR APPROXIMATE LOCATION AND EXTENT.

THE OWNER, BY ACCEPTING THESE PLANS OR PROCEEDING WITH THE IMPROVEMENTS PURSUANT THERETO AGREES TO ASSUME LIABILITY AND TO HOLD THE UNDERSIGNED HARMLESS FOR ANY DAMAGES RESULTING FROM THE EXISTENCE OF UNDERGROUND UTILITIES OR STRUCTURES NOT REPORTED TO THE UNDERSIGNED, NOT INDICATED ON THE PUBLIC RECORDS EXAMINED, OR LOCATED AT VARIANCE WITH THAT REPORTED OR SHOWN ON THE RECORDS EXAMINED.

THE CONTRACTOR IS REQUIRED TO TAKE DUE PRECAUTIONARY MEASURES TO PROTECT THE UTILITIES OR STRUCTURES SHOWN AND ANY OTHER UTILITIES OR STRUCTURES FOUND AT THE SITE. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY THE OWNERS OF THE UTILITIES OR STRUCTURES CONCERNED BEFORE STARTING WORK.

BASIS OF BEARINGS

THE BASIS OF BEARINGS FOR THIS SURVEY IS THE CALIFORNIA COORDINATE SYSTEM ZONE 6, NAD 83, 1991.35 EPOCH AS DETERMINED LOCALLY BY A LINE BETWEEN 40 Y (PID DX2103) AND SANTA FE (PID DX3719) BEING NORTH 80°43'18" WEST AS DERIVED FROM GEODETIC VALUES PUBLISHED BY NATIONAL GEODETIC SURVEY(NGS)

DISTANCES SHOWN HEREON ARE GROUND DISTANCES UNLESS OTHERWISE NOTED. TO OBTAIN GRID DISTANCES MULTIPLY GROUND DISTANCES BY 0.99999207.

CALCULATIONS FROM GRID TO GROUND VALUES AND CONVERGENCE ANGLE FOR THIS SURVEY WERE MADE AT POINT #653 WITH COORDINATES OF N-2,252,331.06, E-6,265,288.22, USING AN ELEVATION OF 1454.22(NAV088)

BENCHMARK

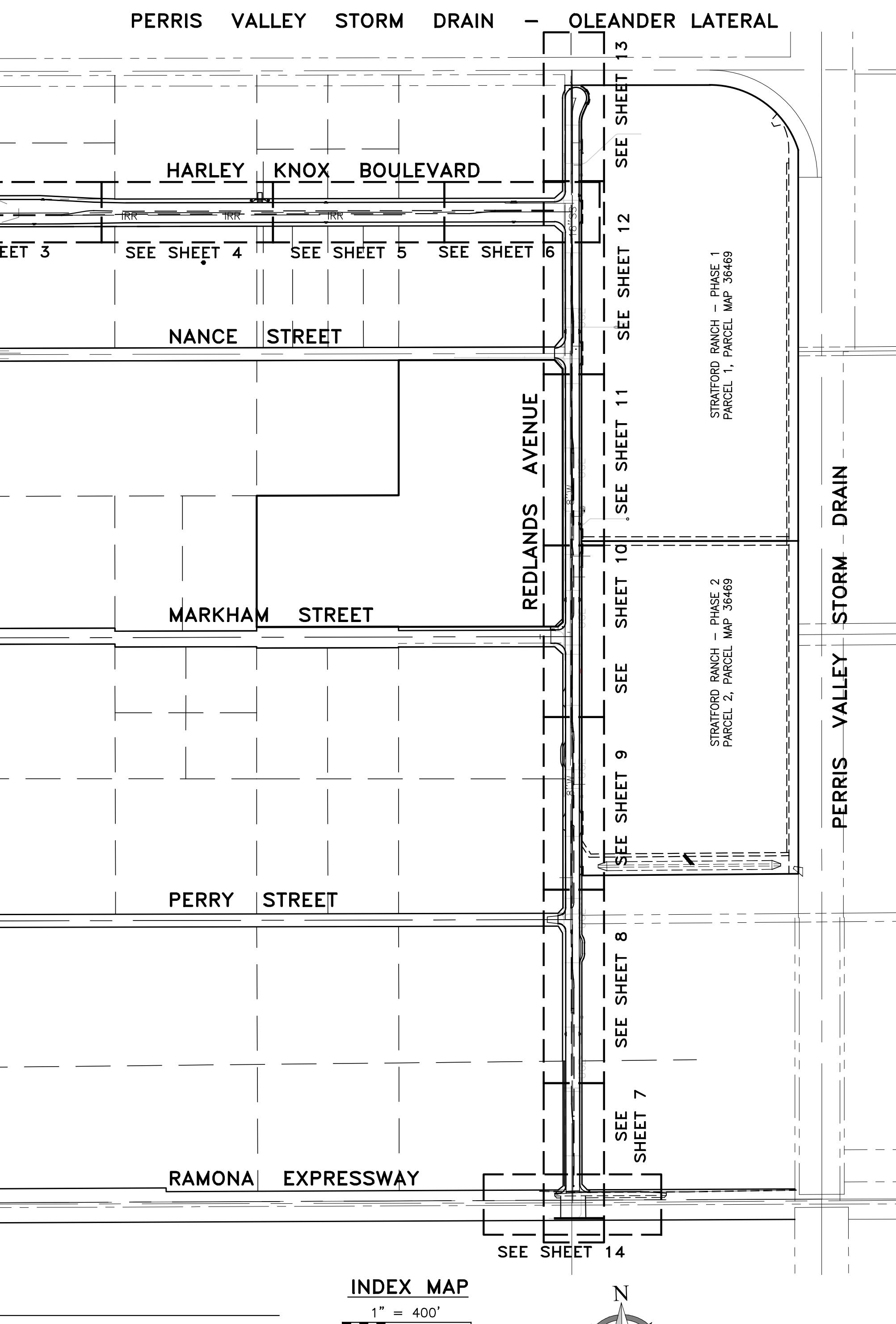
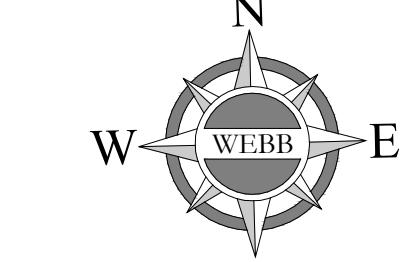
USC & GS BENCHMARKS:

40Y (PID #DX2103) - 3" BRASS DISK, SET IN BOULDER.

STATION IS ABOUT 4-1/2 MILES W. OF LAKEVIEW, ABOUT ONE MILE W. OF THE PASS THROUGH THE BERNASCONI MOUNTAINS, ABOUT 200 FEET SW OF THE INTERSECTION OF BRADLEY ROAD AND WALNUT AVENUE, 70 FEET S OF CENTER LINE OF WALNUT AVENUE, IN A LARGE BULLDOG, AND MARKED WITH A TEE. MARK IS A METROPOLITAN WATER DISTRICT OF SOUTHERN CALIFORNIA STANDARD DISK STAMPED 40 Y 1931.

ELEV. = 1496.35, (NAVD 88) NAVD88 - 2.58 = NAVD29

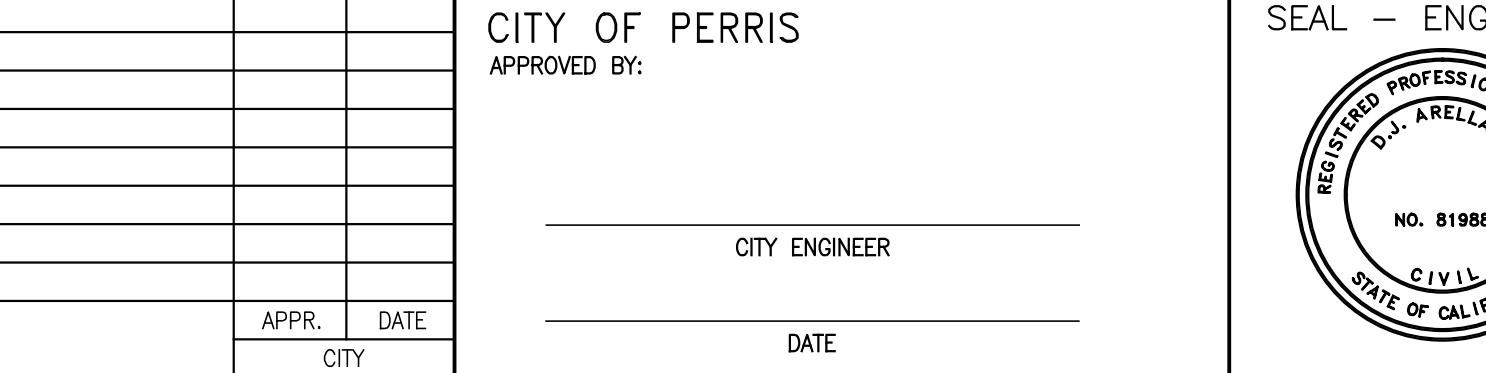
1" = 400'



NOTE:
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DJ 5/29/15 CATCH BASIN REVISED PER FIELD CONDITIONS
DJ 3/5/15 ADDED CONSTRUCTION NOTE
MARK BY DATE
APP. DATE
CITY
CITY OF PERRIS APPROVED BY: CITY ENGINEER
D.J. ARELLANO NO. 81988
CIVIL STATE OF CALIFORNIA
REGISTERED PROFESSIONAL ENGINEER
WEBB ASSOCIATES
UNDER THE SUPERVISION OF: R.C.E. #C81988
D.J. ARELLANO 1/12/2015
DATE



ALBERT A. ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 686-1070
FAX (951) 788-1256
SEE HEREON
1/12/2015
D.J. ARELLANO R.C.E. #C81988
DATE

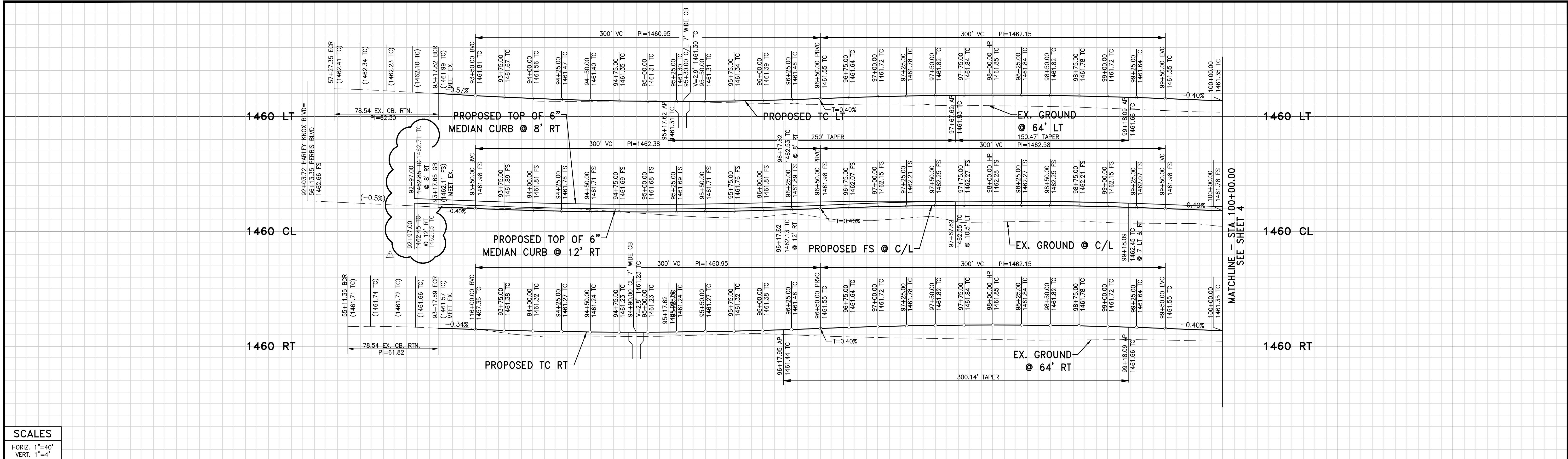
BENCHMARK:	CITY OF PERRIS			SHEET NO.
	AMENDED DPR NO. 11-12-0004 STRATFORD RANCH-PARCEL MAP 36469 STREET IMPROVEMENT PLAN TITLE SHEET			
SEE HEREON	FOR: IDI	W.O.: 2013-0239	CITY FILE NO. P8-1189	1 OF 23 SHEETS
SCALE: H: AS SHOWN V: AS SHOWN				

CONSTRUCTION NOTES AND QUANTITY ESTIMATE

- ** 1 CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II (401,625 SF) 19,370 TONS AC 22,310 CY BASE
- ** 2 CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.) 122,134 SF 3,020 CY CONC. 6,020 CY BASE
- ** 3 CONSTRUCT TYPE "A-B" CURB & GUTTER PER RIV. CO. STD. NO. 201 15,120 LF
- ** 4 CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204 13,325 SF
- ** 5 CONSTRUCT COMMERCIAL DRIVE PER RIV. CO. STD. NO. 207A 4,550 LF
- ** 6 CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401 30,700 LF
- ** 7 CONSTRUCT CURB RAMPS PER RIV. CO. STD. NO. 403, CASE A 18 EA
- ** 8 COORD UNDERGROUNDING/RELOCATION OF PP & GUY WIRE - BY UTILITY COMPANY 5 EA
- ** 9 RELOCATE EX. UTILITY RISER - BY UTILITY COMPANY 16 EA
- ** 10 REMOVE AC PAVEMENT AND DISPOSE OF LEGALLY 1,150 SF
- ** 11 SAWCUT & JOIN EX. A.C. PAVEMENT PER DETAIL ON SHEET 2 700 LF
- ** 12 RELOCATE 4 EA
- ** 13 ADJUST TO GRADE 19 EA
- ** 14 PROTECT IN PLACE -
- ** 15 INSTALL 3" AC OVER 95% COMPACTED NATIVE 1,455 SF
- ** 16 REMOVE EX. FENCE 1,900 LF
- ** 17 CONSTRUCT CROSS GUTTER PER RIV. CO. STD. NO. 209 1,425 SF
- ** 18 CONSTRUCT 6" TYPE "D-1" CURB PER RIV. CO. STD. NO. 203 - LF
- ** 19 0.15' GRIND AND OVERLAY 3,550 SF
- ** 20 INSTALL 48" RCP (D-LOAD PER PLAN) 280 LF
- ** 21 INSTALL 36" RCP (D-LOAD PER PLAN) 860 LF
- ** 22 INSTALL 24" RCP (D-LOAD PER PLAN) 2,110 LF
- ** 23 INSTALL 18" RCP (D-LOAD PER PLAN) 560 LF
- ** 24 CONSTRUCT JUNCTION STRUCTURE NO 2 PER RCFC&WCD STD. JS227 6 EA
- ** 25 CONSTRUCT JUNCTION STRUCTURE NO 3 PER RCFC&WCD STD. JS228 1 EA
- ** 26 CONSTRUCT JUNCTION STRUCTURE NO 4 PER RCFC&WCD STD. JS229 1 EA
- ** 27 CONSTRUCT CURB INLET CATCH BASIN PER RIV. CO. STD. NO. 300 17 EA
- ** 28 CONSTRUCT LOCAL DEPRESSION PER RIV. CO. STD. NO. 311 17 EA
- ** 29 CONSTRUCT MANHOLE NO.1 PER RFC&WCD STD. MH251 5 EA
- ** 30 CONSTRUCT MANHOLE NO.2 PER RFC&WCD STD. MH252 2 EA
- ** 31 CONSTRUCT MANHOLE NO.4 PER RFC&WCD STD. MH254 4 EA
- ** 32 CONSTRUCT DRAINAGE INLET TYPE G3 PER CALTRANS PLAN D73, AND DETAIL ON SHEET 2, 1 EA
- ** 33 REMOVE CONCRETE BULKHEAD 1 EA
- ** 34 INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL) 190 LF
- ** 35 INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE 6 EA
- ** 36 REMOVE BACKFLOW AND SERVICE. COORDINATE WITH EMWD 1 EA
- ** 37 CONSTRUCT 8" THICK CONCRETE CLASS 560-C-3250; "B" AGGREGATE GRADATION 4 EA
- ** 38 CONSTRUCT BUS TURNOUT PER RIV. CO. STD. NO. 814 2 EA
- ** 39 INSTALL 48" CIPCD PER MANUFACTURES SPECS 280 LF
- ** 40 INSTALL 36" CIPCD PER MANUFACTURES SPECS 860 LF
- ** 41 INSTALL 24" CIPCD PER MANUFACTURES SPECS 1,300 LF
- ** 42 INSTALL 6" SLURRY BACKFILL (2 SACK) 395 LF
- ** 43 INSTALL CONCRETE COLLAR PER RFC&WCD STD. M803 1 EA
- ** 44 INSTALL 24" CMP HEL-COR PIPE ("CONTECH" OR APPROVED EQUAL) 100 LF
- ** 45 INSTALL 24" FLARED END SECTION ("CONTECH" OR APPROVED EQUAL) 2 EA
- ** 46 CONSTRUCT CONCRETE BULKHEAD 1 EA
- ** 47 CONSTRUCT MODIFIED GRATING CATCH BASIN PER SSPWC STD 303-3 AND DETAIL ON SHEET 16 1 EA
- ** 48 CONSTRUCT LOCAL DEPRESSION PER SSPWC STD 313-3 CASE C 1 EA

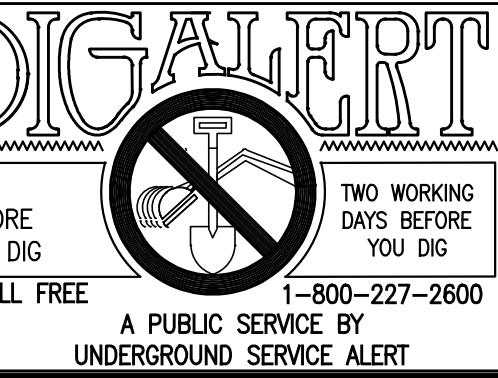
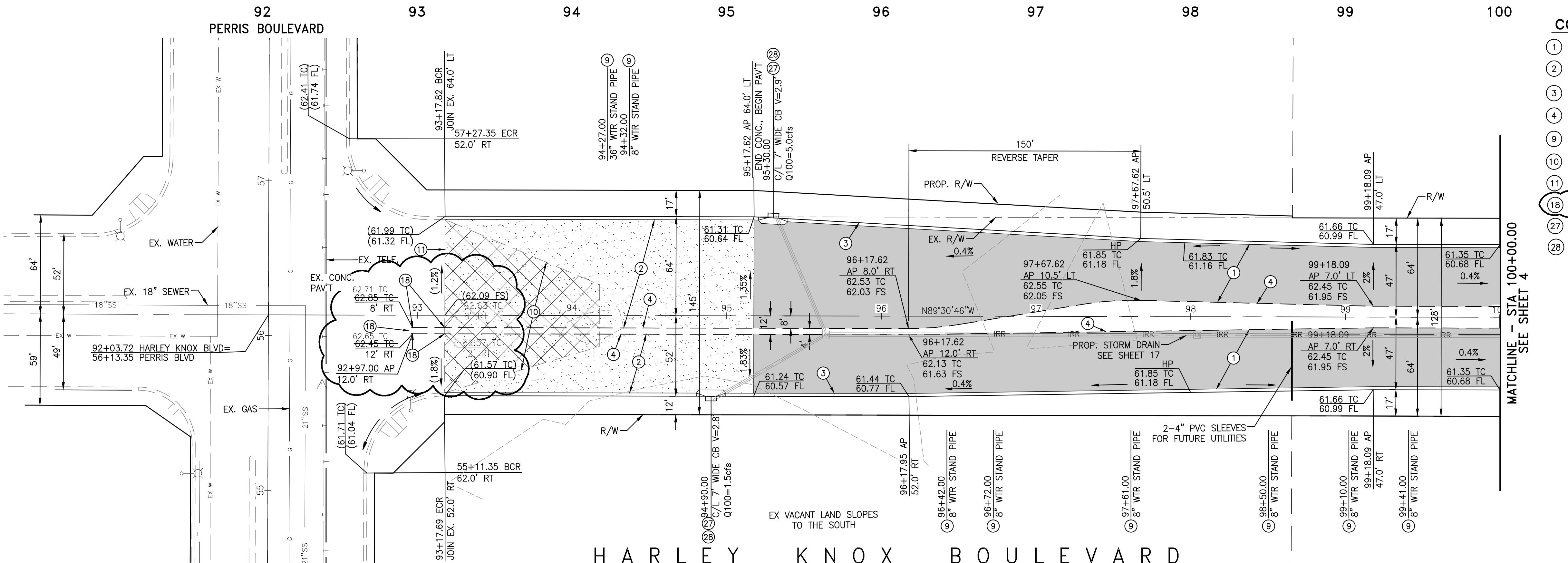
THE QUANTITY ESTIMATE SHOWN HEREON IS FOR THE USE OF GOVERNING AGENCIES IN DETERMINING BOND AMOUNT AND/OR FEES AND IS NOT TO BE USED FOR BID PURPOSES.

* * SEE GENERAL NOTE NO. 9



SCALES

HORIZ. 1"=40'
VERT. 1"=4'



NOTE:
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APPROVED BY:		CITY OF PERRIS		SEAL - ENGINEER	
D.J. ARELLANO	REVISER	CITY ENGINEER	REVISER	ALBERT A. WEBB	ENGINEERING CONSULTANTS
D.J. ARELLANO	REVISER	REVISIONS	REVISIONS	ASSOCIATES	3788 McCRAY STREET RIVERSIDE CA. 92506 PH. (951) 666-1070 FAX (951) 788-1256
MARK BY DATE	APPR. DATE	APPR. DATE	APPR. DATE	UNDER THE SUPERVISION OF: D.J. ARELLANO R.C.E. #C81988	BENCHMARK: SEE SHEET 1

CITY OF PERRIS

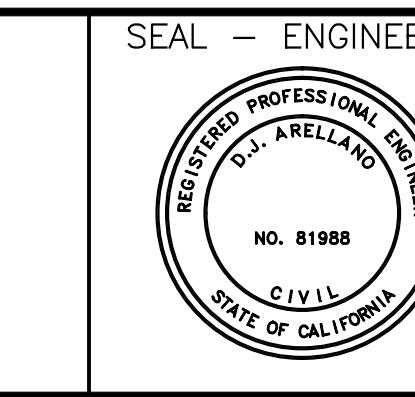
APPROVED BY:

APPR. DATE

APPR. DATE

APPR. DATE

APPR. DATE



ALBERT A. WEBB
ASSOCIATES
REGISTERED PROFESSIONAL ENGINEER
NO. 81988
CIVIL
STATE OF CALIFORNIA
1/12/2015
D.J. ARELLANO
R.C.E. #C81988
DATE

BENCHMARK:

CITY OF PERRIS

AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
HARLEY KNOX BOULEVARD
STA 92+03.72 TO STA 100+00.00

SEE SHEET 1

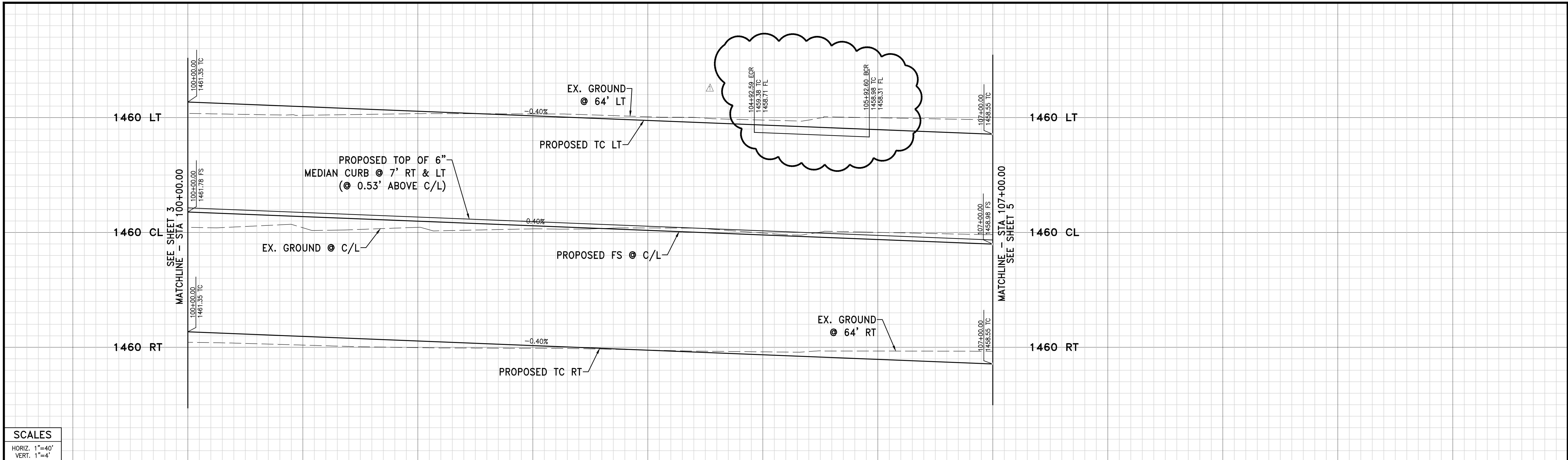
SCALE:
H: AS SHOWN V: AS SHOWN

FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189

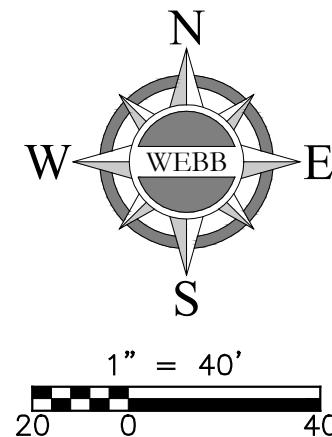
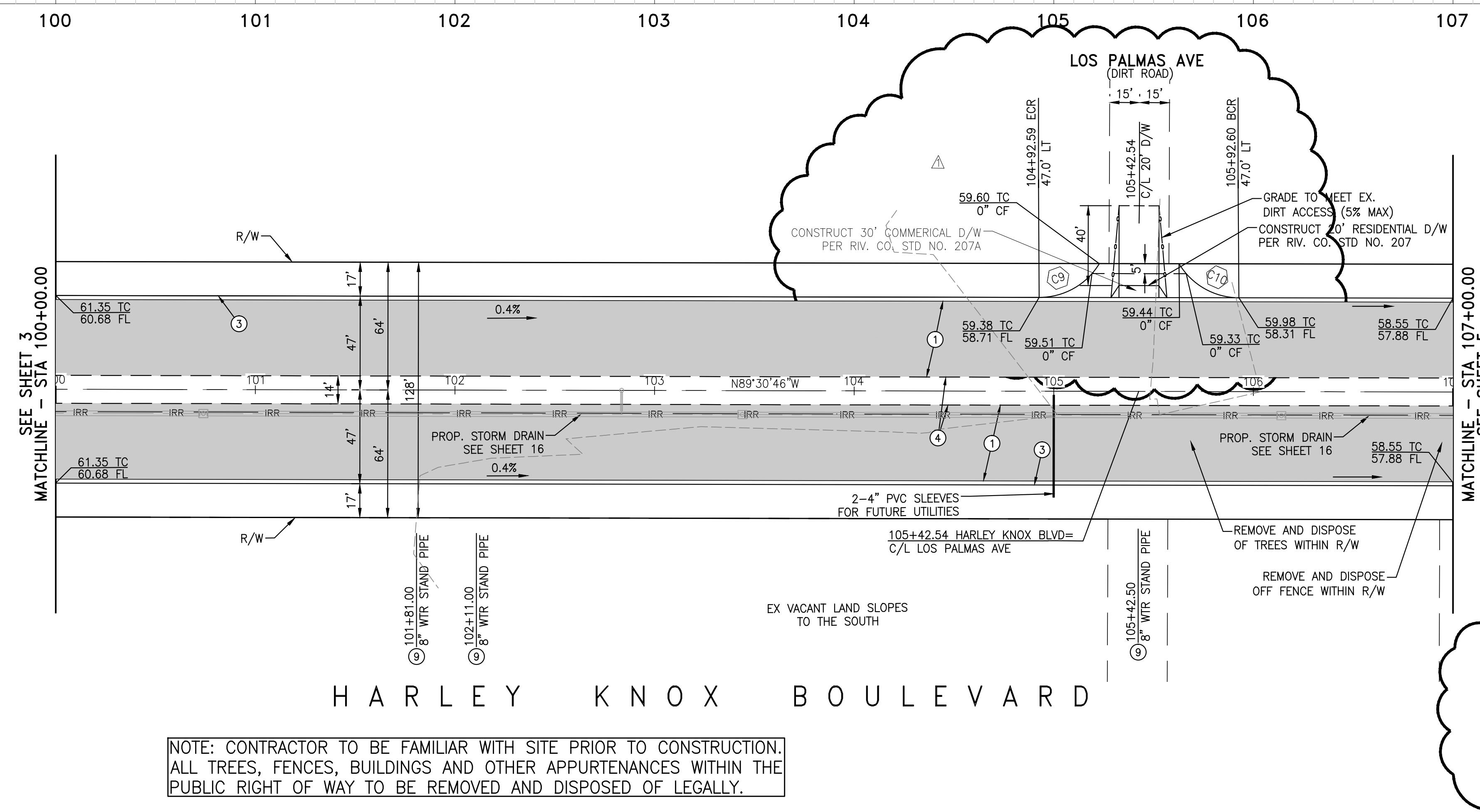


LEGEND:

- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
- REMOVE EXISTING AC PAVING
- INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE



SCALES
HORIZ. 1''=40'
VERT. 1''=4'



NOTE: CONTRACTOR TO BE FAMILIAR WITH SITE PRIOR TO CONSTRUCTION.
ALL TREES, FENCES, BUILDINGS AND OTHER APPURTENANCES WITHIN
THE PUBLIC RIGHT OF WAY TO BE REMOVED AND DISPOSED OF LEGALLY.

CONSTRUCTION NOTES

- ① CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II
- ③ CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201
- ④ CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204
- ⑨ RELOCATE EX. UTILITY RISER - BY UTILITY COMPANY

AS BUILT

THESE PLANS REFLECT ANY SUBSTANTIAL
DESIGN MODIFICATIONS AS PROVIDED TO
WEBB ASSOCIATES BY THE CONTRACTOR

SIGNATURE _____
DATE 05/19/2016

REGISTRED PROFESSIONAL ENGINEER
D.J. ARELLANO
NO. 81988
CIVIL
STATE OF CALIFORNIA

05/19/2016

AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
HARLEY KNOX BOULEVARD
STA 100+00.00 TO STA 107+00.00

5/18/2016 8:29 AM

LEGEND:

- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
- REMOVE EXISTING AC PAVING
- INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE

CURVE TABLE				
#	LENGTH	RADIUS	DELTA	TANGENT
C9	36.07	35.00	059°03'01"	19.82
C10	36.07	35.00	059°03'01"	19.82



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DJM	5/19/13	REVISE DRIVEWAY FROM STD 207 TO STD 207A
MARK	BY DATE	REVISIONS
ENGINEER	APPR. DATE	CITY

CITY OF PERRIS
APPROVED BY:
CITY ENGINEER
DATE

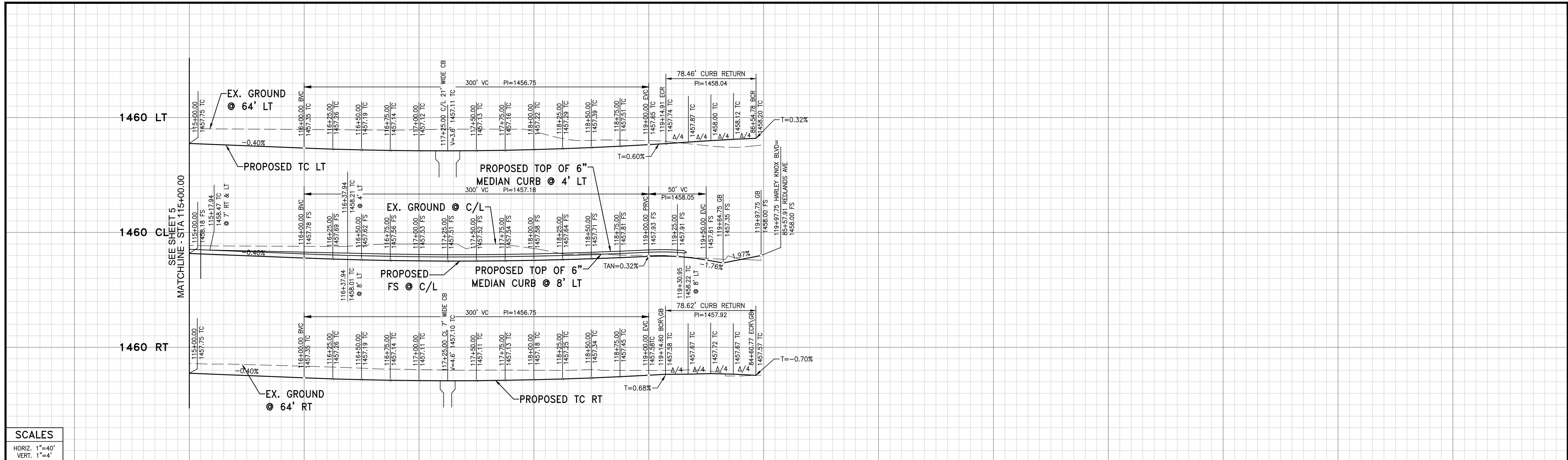
SEAL - ENGINEER
WEBB
ASSOCIATES
REGISTERED PROFESSIONAL ENGINEER
D.J. ARELLANO
NO. 81988
CIVIL
STATE OF CALIFORNIA

ALBERT A. ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 686-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #C81988
1/12/2015
DATE

BENCHMARK:
SEE SHEET 1
SCALE: H: AS SHOWN V: AS SHOWN
FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189

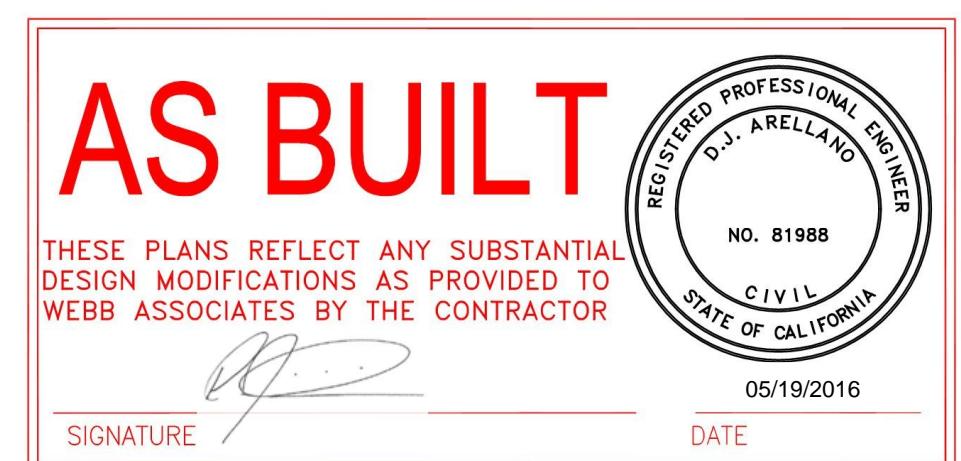
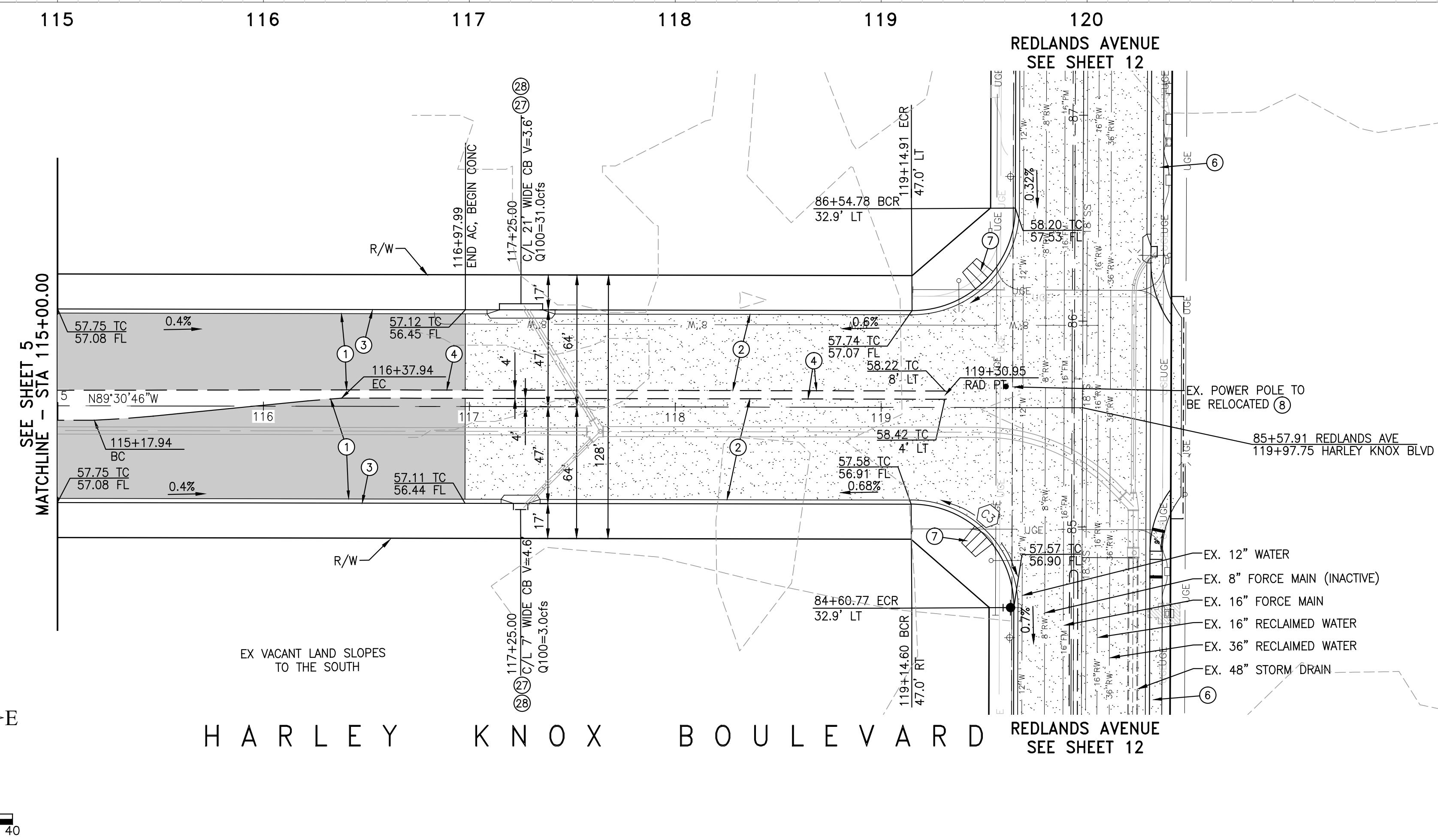
CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
HARLEY KNOX BOULEVARD
STA 100+00.00 TO STA 107+00.00

SHEET NO. 4
OF 23 SHEETS
G:\2013\1-3-0239\DRAWINGS\AS-BUILT\13-0239-C-ST-AB.DWG 5/18/2016 8:29 AM



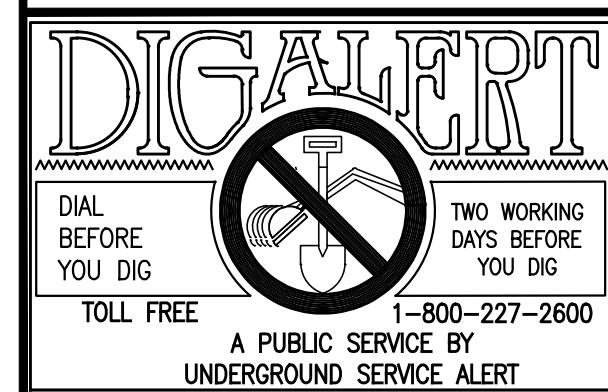
SCALES

HORIZ. 1"=40'
VERT. 1"=4'



LEGEND:

- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
- REMOVE EXISTING AC PAVING
- INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE

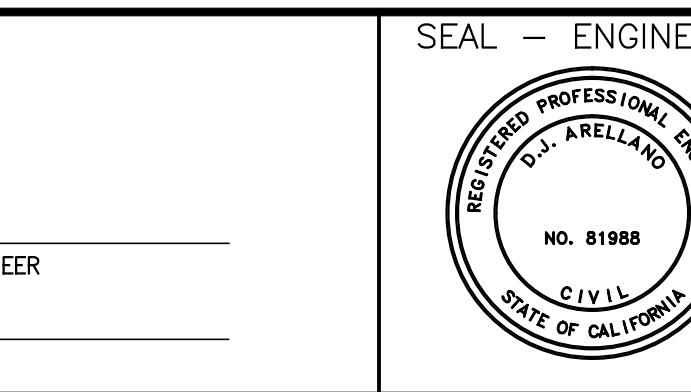


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MARK	BY	DATE	REVISIONS	APPR.	DATE
ENGINEER				CITY	

CITY OF PERRIS
APPROVED BY:



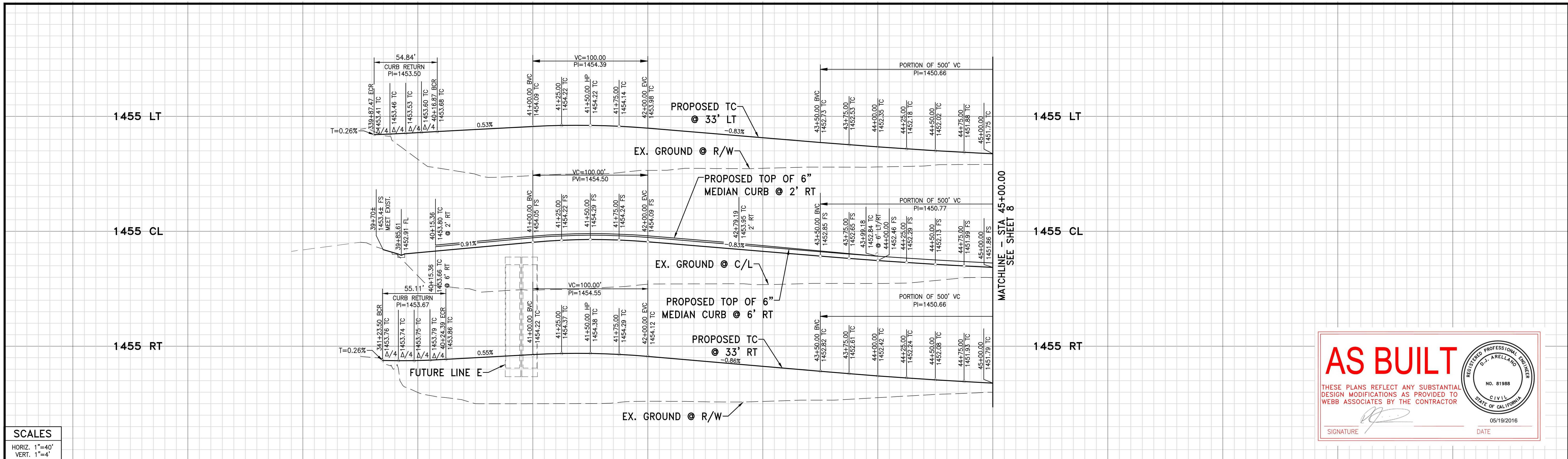
SEAL - ENGINEER

ALBERT A. WEBB
ASSOCIATES
REGISTERED PROFESSIONAL ENGINEER
D.J. ARELLANO
NO. 81988
CIVIL STATE OF CALIFORNIA

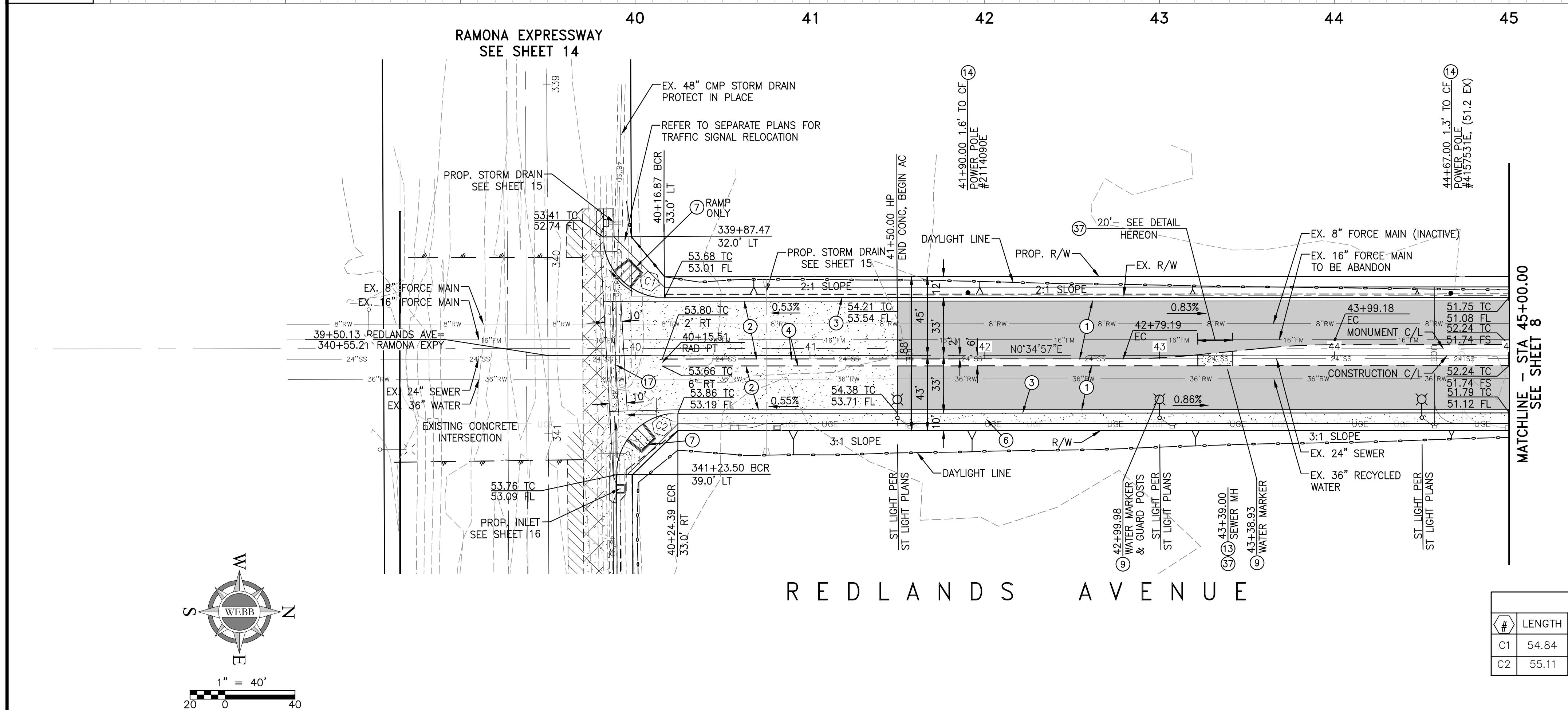
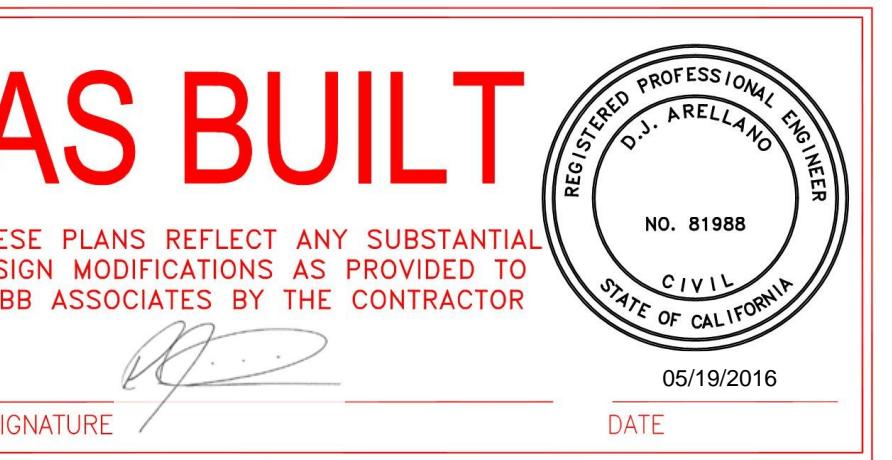
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R.C.E. #C81988
1/12/2015

BENCHMARK:
SEE SHEET 1

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
HARLEY KNOX BOULEVARD
STA 115+00.00 TO STA 119+93.75
SHEET NO. 6
OF 23 SHEETS
SCALE: H: AS SHOWN V: AS SHOWN
FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189
DATE: 5/18/2016 8:30 AM

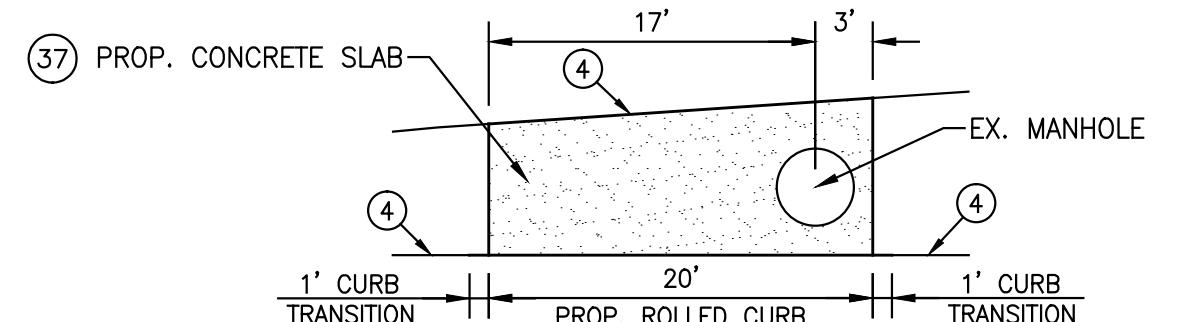


SCALES
HORIZ. 1"=40'
VERT. 1"=4'



CONSTRUCTION NOTES

- ① CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II
- ② CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)
- ③ CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201
- ④ CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204
- ⑥ CONSTRUCT 6" WIDE SIDEWALK PER RIV. CO. STD. 401
- ⑦ CONSTRUCT CURB RAMP PER RIV. CO. STD. NO. 403, CASE A
- ⑨ RELOCATE EX. UTILITY RISER - BY UTILITY COMPANY
- ⑪ SAWCUT & JOIN EX. A.C. PAVEMENT PER DETAIL ON SHEET 2
- ⑬ ADJUST TO GRADE
- ⑭ PROTECT IN PLACE
- ⑯ CONSTRUCT CROSS GUTTER PER RIV. CO. STD. NO. 209
- ⑰ CONSTRUCT 8" THICK CONCRETE CLASS 560-C-3250; "B" AGGREGATE GRADATION



SEWER MANHOLE MEDIAN DETAIL

STATION 43+39.00
NOT TO SCALE

LEGEND:

- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
- REMOVE EXISTING AC PAVING
- INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE

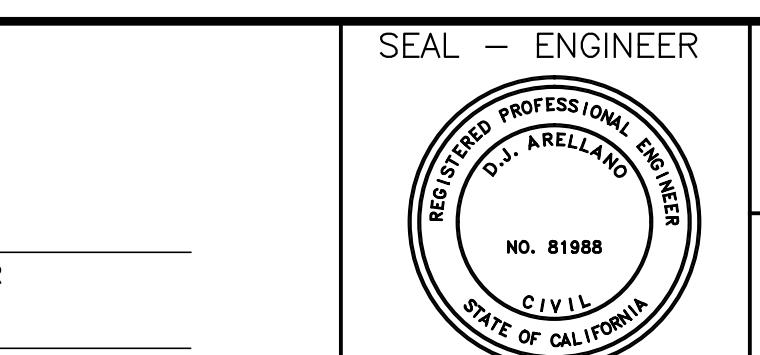


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MARK	BY	DATE	REVISIONS	APPR.	DATE	CITY
ENGINEER						

CITY OF PERRIS
APPROVED BY:



ALBERT A. WEBB
ASSOCIATES
REGISTERED PROFESSIONAL ENGINEER
CIVIL
NO. 81988
STATE OF CALIFORNIA

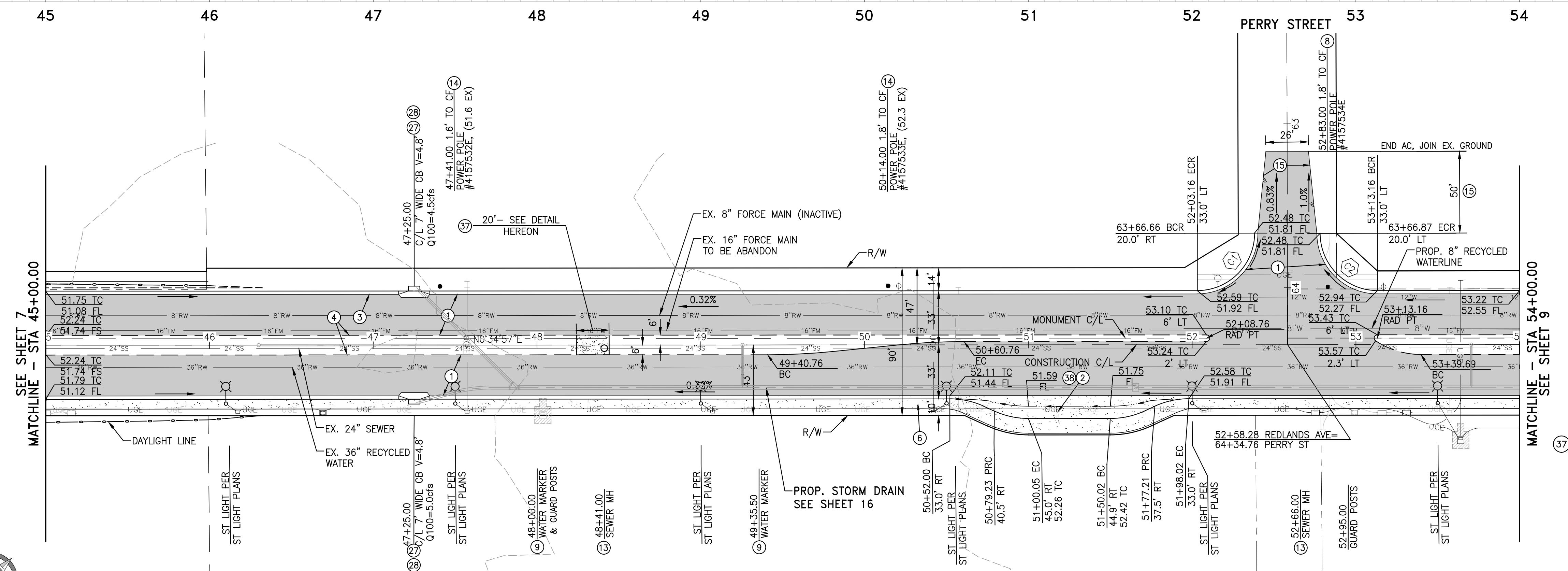
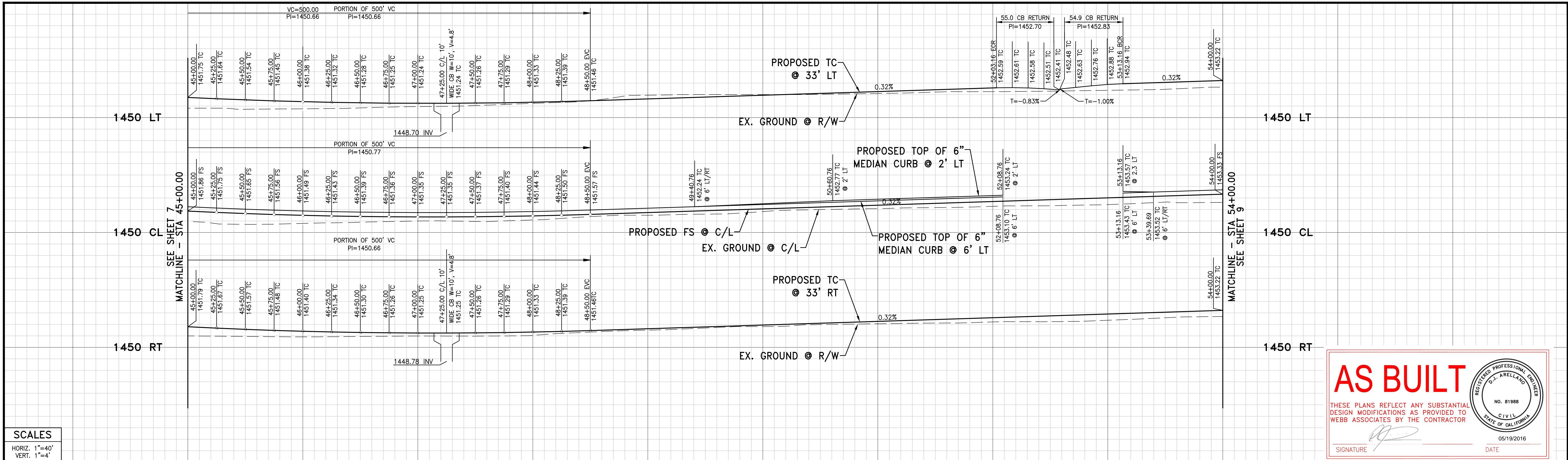
ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 686-1070
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1/12/2015

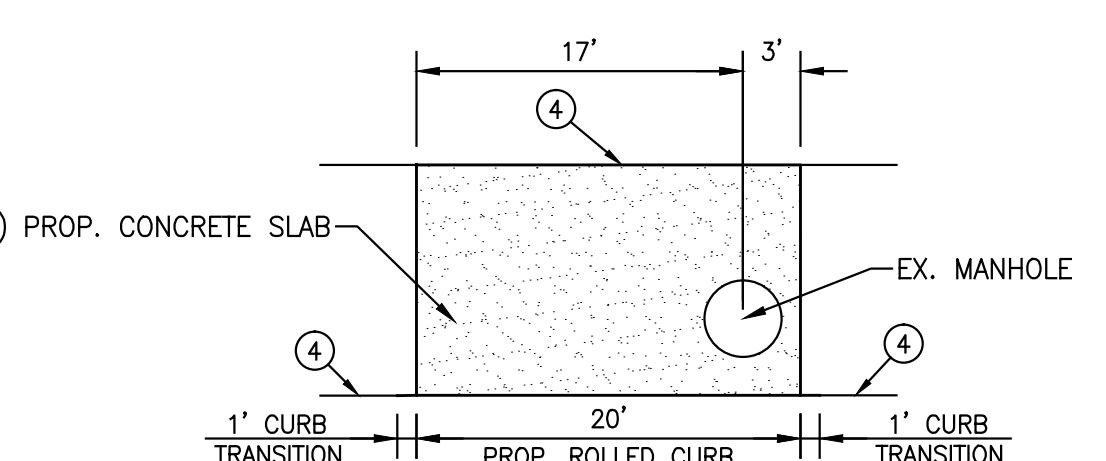
BENCHMARK:
SEE SHEET 1

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
REDLANDS AVENUE
STA 39+50.13 TO STA 45+00.00

SHEET NO.
7
OF 23 SHEETS
FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189



- CONSTRUCTION NOTES**
- CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II
 - CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)
 - CONSTRUCT TYPE "A-B" CURB & GUTTER PER RIV. CO. STD. NO. 201
 - CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204
 - CONSTRUCT 6" WIDE SIDEWALK PER RIV. CO. STD. 401
 - COORD UNDERGROUNDING/RELOCATION OF PP & GUY WIRE - BY UTILITY COMPANY
 - RELOCATE EX. UTILITY RISER - BY UTILITY COMPANY
 - ADJUST TO GRADE
 - PROTECT IN PLACE
 - INSTALL 3" AC OVER 95% COMPACTED NATIVE
 - CONSTRUCT CURB INLET CATCH BASIN PER RIV. CO. STD. NO. 300
 - CONSTRUCT LOCAL DEPRESSION PER RIV. CO. STD. NO. 311
 - CONSTRUCT 8" THICK CONCRETE CLASS 560-C-3250; "B" AGGREGATE GRADATION
 - CONSTRUCT BUS TURNOUT PER RIV. CO. STD. NO. 814



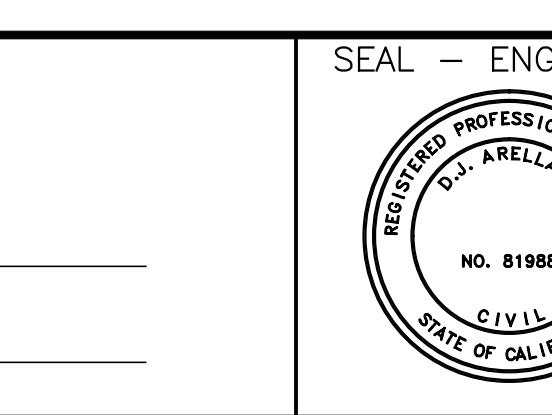
- LEGEND:**
- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
 - REMOVE EXISTING AC PAVING
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ENGINEER			CITY

CITY OF PERRIS
APPROVED BY:
CITY ENGINEER
DATE

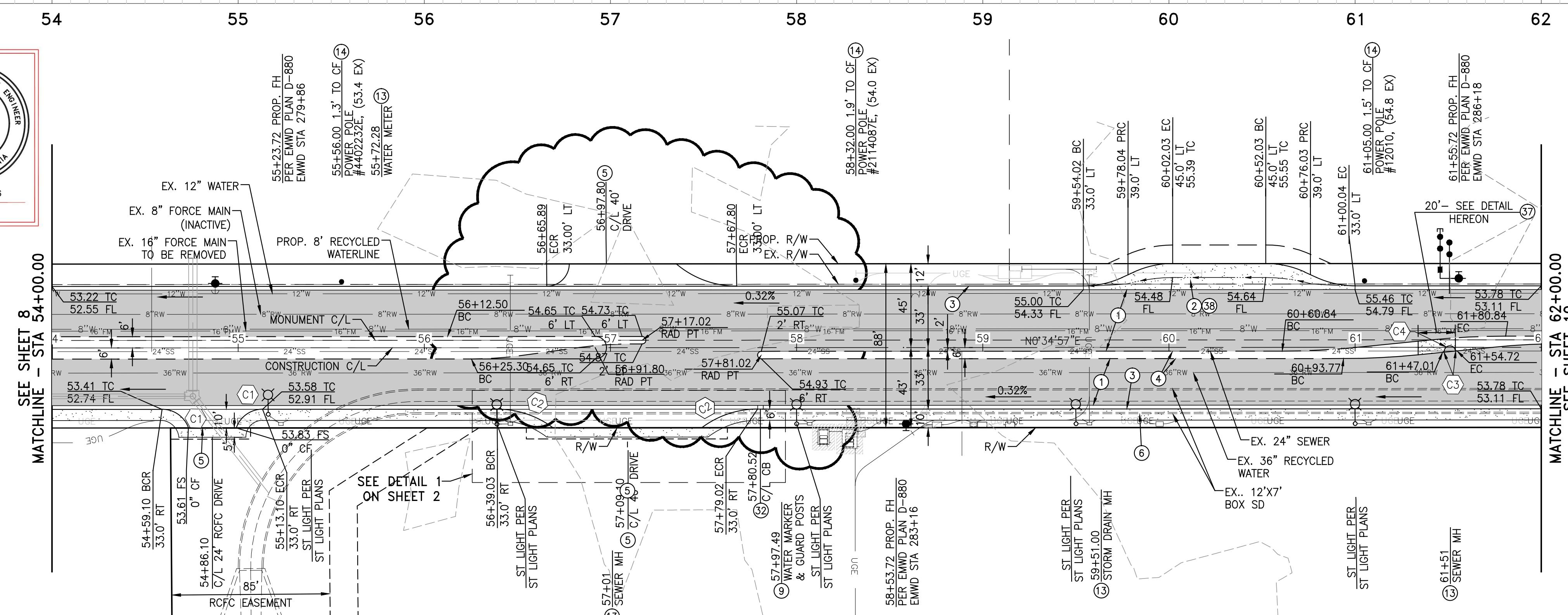
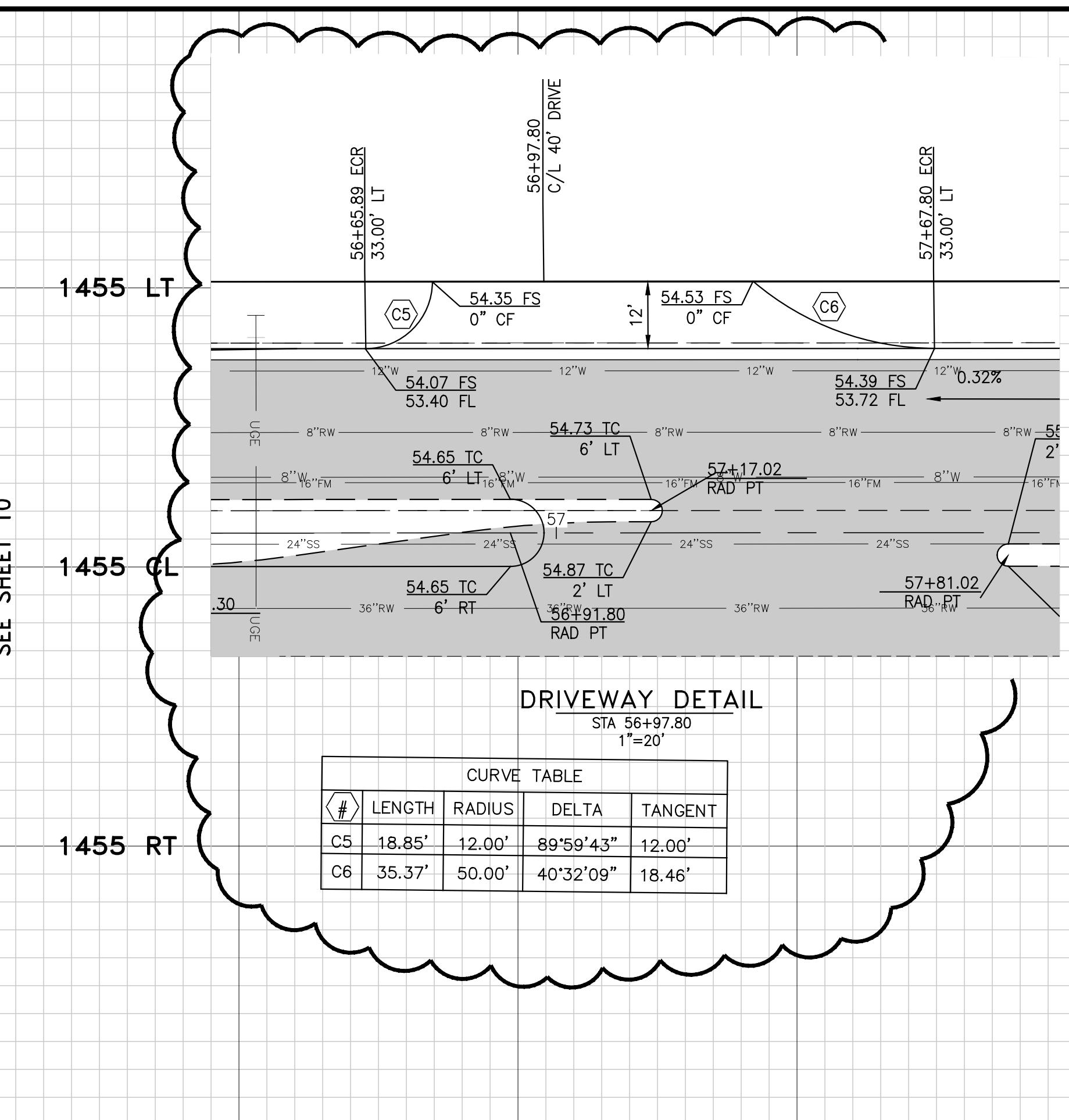
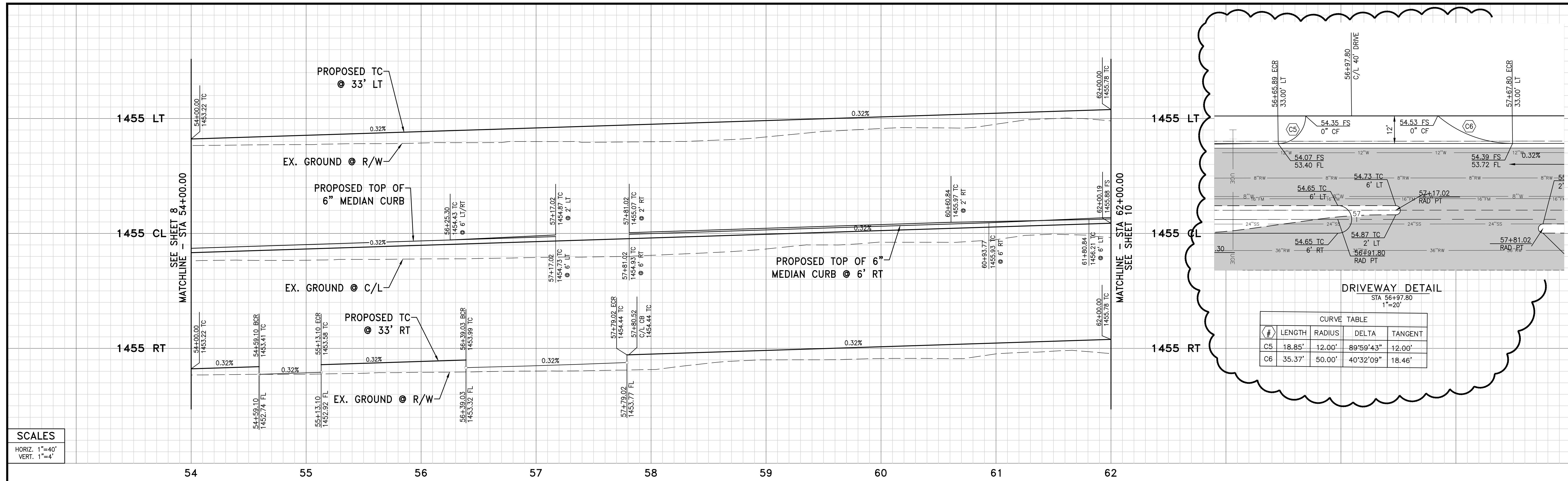


ALBERT A. ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 666-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #C81988
1/12/2015

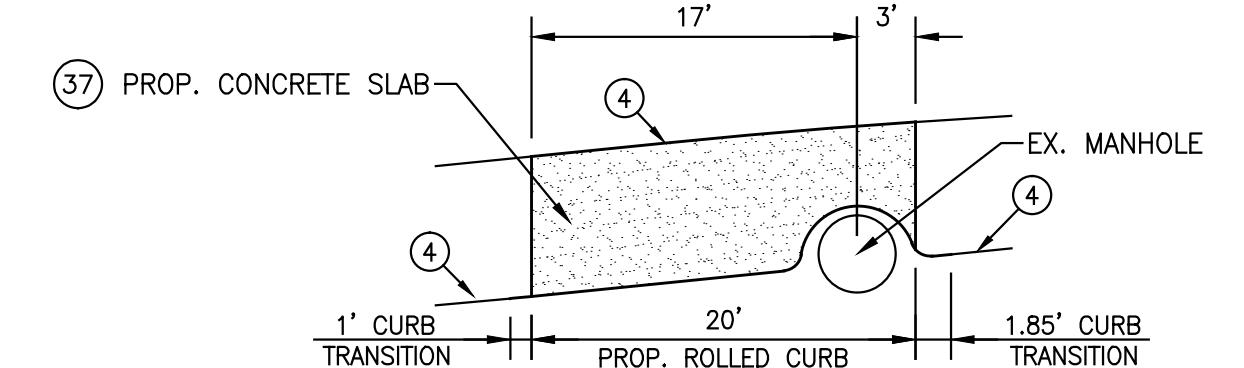
BENCHMARK:
SEE SHEET 1
SCALE:
H: AS SHOWN V: AS SHOWN

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
REDLANDS AVENUE
STA 45+00.00 TO STA 54+00.00
FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189

SHEET NO.
OF 23 SHEETS
8



- CONSTRUCTION NOTES**
- CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II
 - CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)
 - CONSTRUCT TYPE "A-B" CURB & GUTTER PER RIV. CO. STD. NO. 201
 - CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204
 - CONSTRUCT COMMERCIAL DRIVE PER RIV. CO. STD. NO. 207A
 - CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401
 - RELOCATE EX. UTILITY RISER - BY UTILITY COMPANY
 - ADJUST TO GRADE
 - PROTECT IN PLACE
 - CONSTRUCT DRAINAGE INLET TYPE G3 PER CALTRANS PLAN D73, AND DETAIL ON SHEET 2
 - CONSTRUCT 8" THICK CONCRETE CLASS 560-C-3250; "B" AGGREGATE GRADATION
 - CONSTRUCT BUS TURNOUT PER RIV. CO. STD. NO. 814



SEWER MANHOLE MEDIAN DETAIL
STATION 61+51.00
NOT TO SCALE

- LEGEND:**
- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
 - REMOVE EXISTING AC PAVING
 - INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE

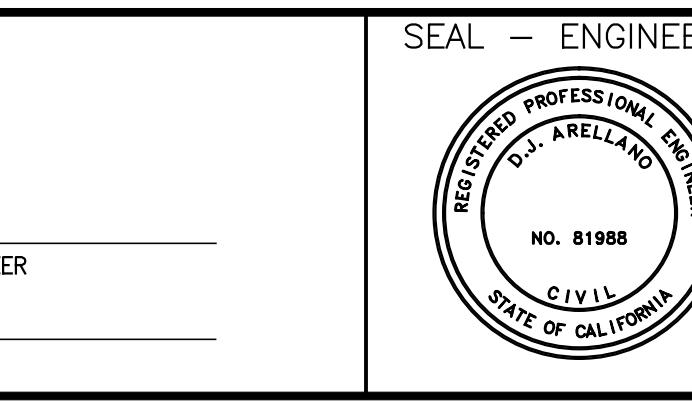
CURVE TABLE				
#	LENGTH	RADIUS	DELTA	TANGENT
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C2	32.18	50.00	036°52'12"	16.67
C3	1.32	1.00	075°31'21"	0.77
C4	7.91	3.00	151°02'42"	11.62



NOTE:
WORK CONTAINED WITHIN THESE PLANS SHALL NOT COMMENCE UNTIL AN ENCROACHMENT PERMIT AND/OR A GRADING PERMIT HAS BEEN ISSUED.
THE PRIVATE ENGINEER SIGNING THESE PLANS IS RESPONSIBLE FOR ASSURING THE ACCURACY AND ACCEPTABILITY OF THE DESIGN HEREON. IN THE EVENT OF DISCREPANCIES ARISING AFTER CITY APPROVAL OR DURING CONSTRUCTION, THE PRIVATE ENGINEER SHALL BE RESPONSIBLE FOR DETERMINING AN ACCEPTABLE SOLUTION AND REVISING THE PLANS FOR APPROVAL BY THE CITY.

APPR. DATE	DATE
ENGINEER	CITY
REVISIONS	

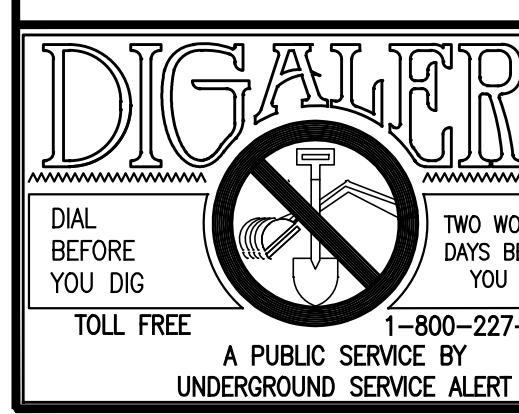
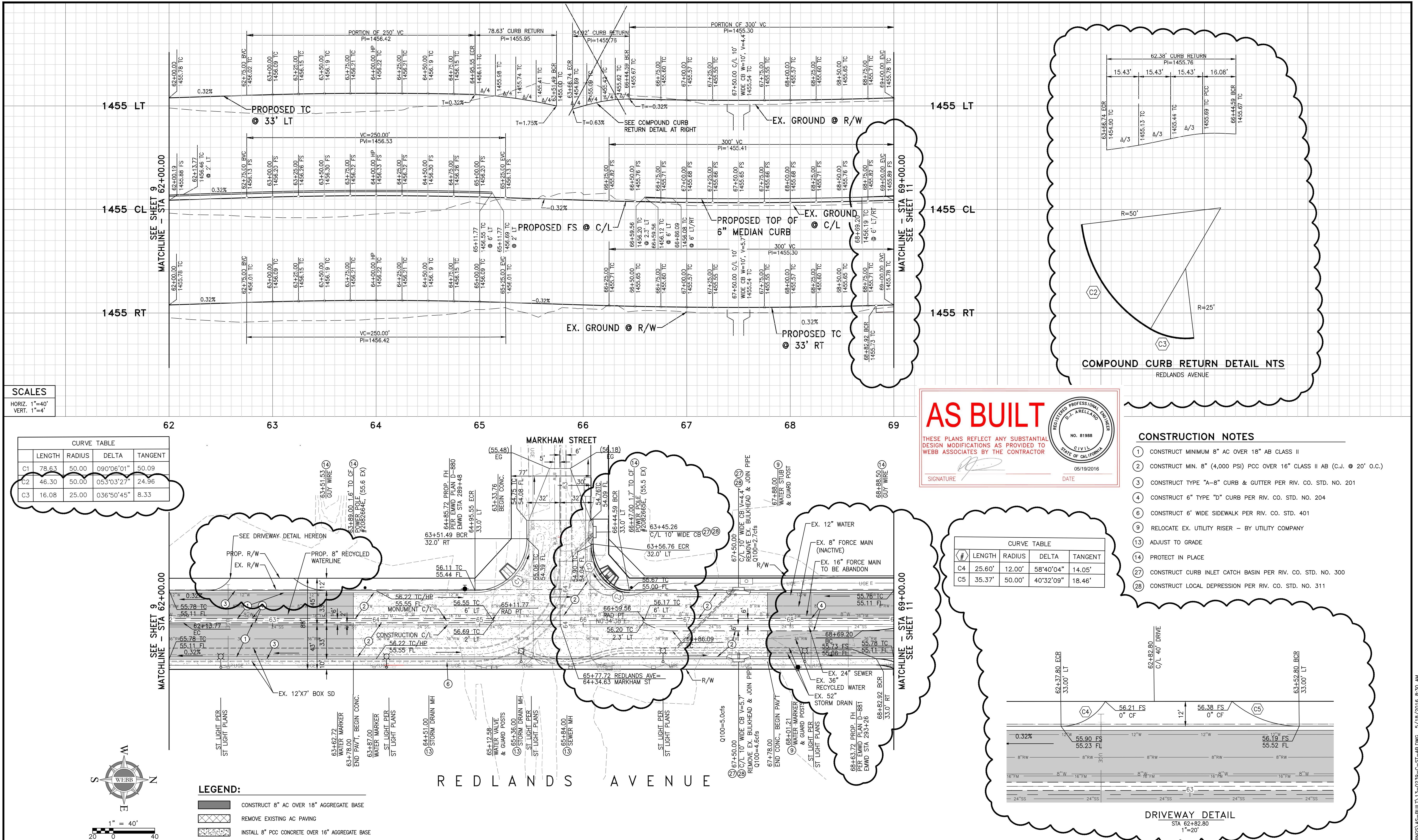
CITY OF PERRIS
APPROVED BY:
CITY ENGINEER



ALBERT A. ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 666-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #C81988
1/12/2015

BENCHMARK:
SEE SHEET 1

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
REDLANDS AVENUE
STA 54+00.00 TO STA 62+00.00
FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189
SHEET NO. 9A
OF 23 SHEETS



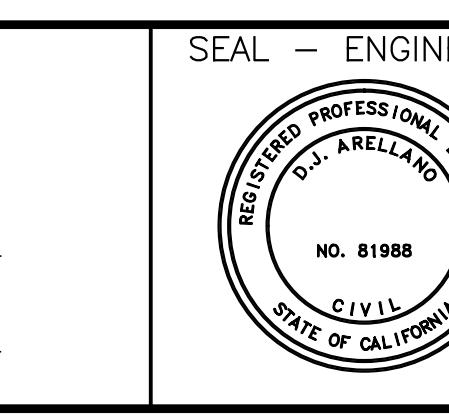
NOTE:

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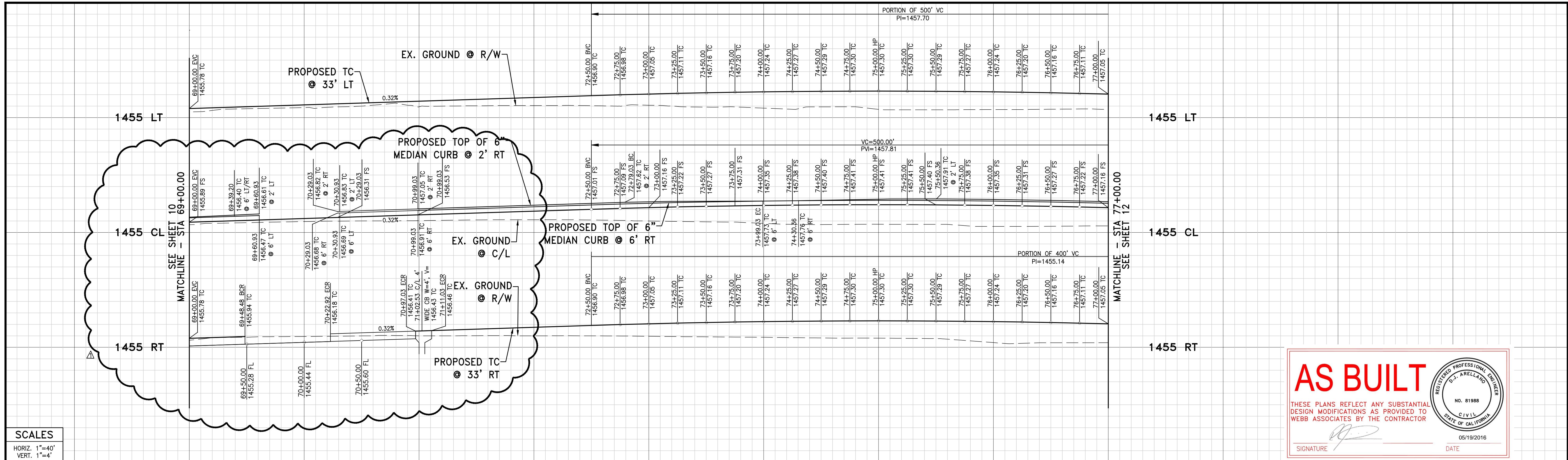
For more information about the study, please contact Dr. John Smith at (555) 123-4567 or via email at john.smith@researchinstitute.org.

10 of 10



BENCH
S
SCALE:
H: AS S

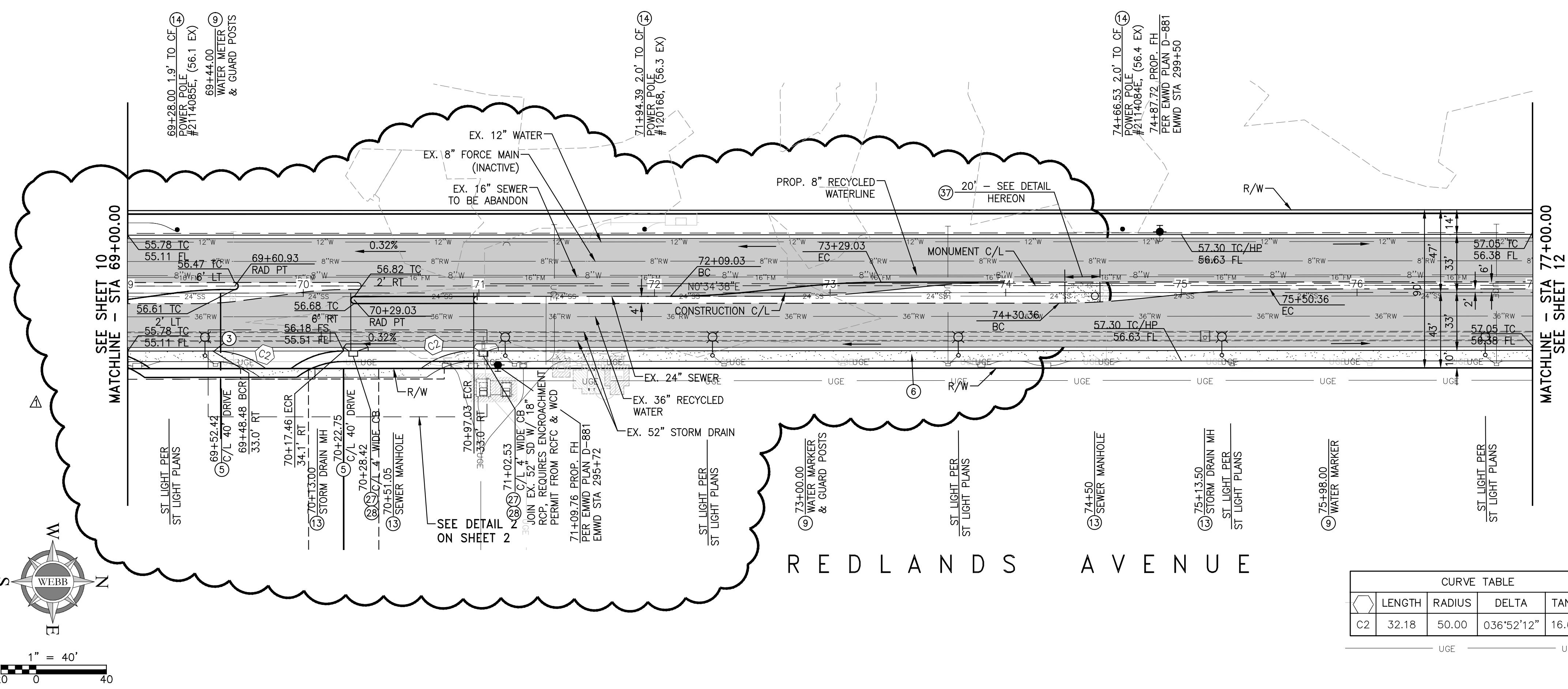
MARK: EE SHEET 1	CITY OF PERRIS	SHEET NO.	
	AMENDED DPR NO. 11-12-0004 STRATFORD RANCH-PARCEL MAP 36469 REDLANDS AVENUE STA 62+00.00 TO STA 70+00.00	10A OF 23 SHEETS	
<u>SHOWN V: AS SHOWN</u>	FOR: IDI	W.O. 2013-0239	CITY FILE NO. P8-1189



SCALES

HORIZ. 1"=40'
VERT. 1"=4'

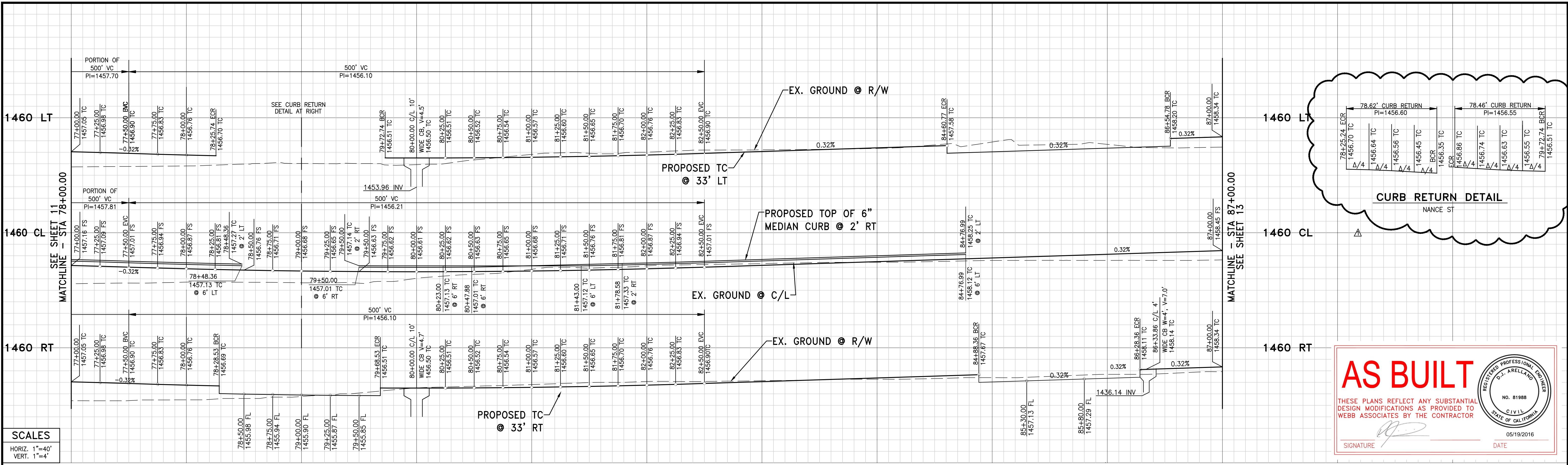
69 70 71 72 73 74 75 76 77 78



NOTE:
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APPROVED BY:		CITY OF PERRIS		SEAL - ENGINEER		ALBERT A. WEBB		ENGINEERING CONSULTANTS		BENCHMARK:	
△ DJM	7/1/15	REVISER DRIVEWAY AND CATCH BASIN LOCATIONS		NO. 81988	REGISTERED PROFESSIONAL ENGINEER D.J. ARELLANO CIVIL STATE OF CALIFORNIA	UNDER THE SUPERVISION OF: D.J. ARELLANO	R.C.E. #C81988	3788 McCRAY STREET RIVERSIDE CA. 92506 PH. (951) 666-1070 FAX (951) 788-1256	1/12/2015	SEE SHEET 1	CITY OF PERRIS
MARK BY DATE		REVISIONS	APPR. DATE							AMENDED DPR NO. 11-12-0004 STRATFORD RANCH-PARCEL MAP 36469 REDLANDS AVENUE STA 70+00.00 TO STA 78+00.00	
ENGINEER			CITY	DATE						SCALE: H: AS SHOWN V: AS SHOWN	FOR: IDI



AS BUILT

THESE PLANS REFLECT ANY SUBSTANTIAL
DESIGN MODIFICATIONS AS PROVIDED TO
THE CONTRACTOR BY THE ASSOCIATES.

BB ASSOCIATES BY THE CONTRACTOR

SIGNATURE

CONSTRUCTION NOTES

- CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II

CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)

CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201

CONSTRUCT 6" TYPE "D" CURB PER RIV. CO. STD. NO. 204

CONSTRUCT COMMERCIAL DRIVE PER RIV. CO. STD. NO. 207A

CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401

CONSTRUCT CURB RAMP PER RIV. CO. STD. NO. 403, CASE A

COORD UNDERGROUNDING/RELOCATION OF PP
& GUY WIRE - BY UTILITY COMPANY

RELOCATE EX. UTILITY RISER - BY UTILITY COMPANY

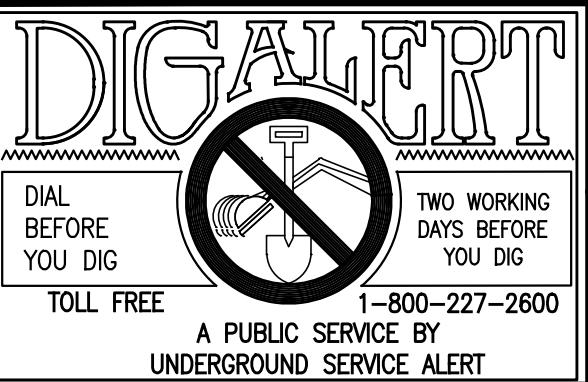
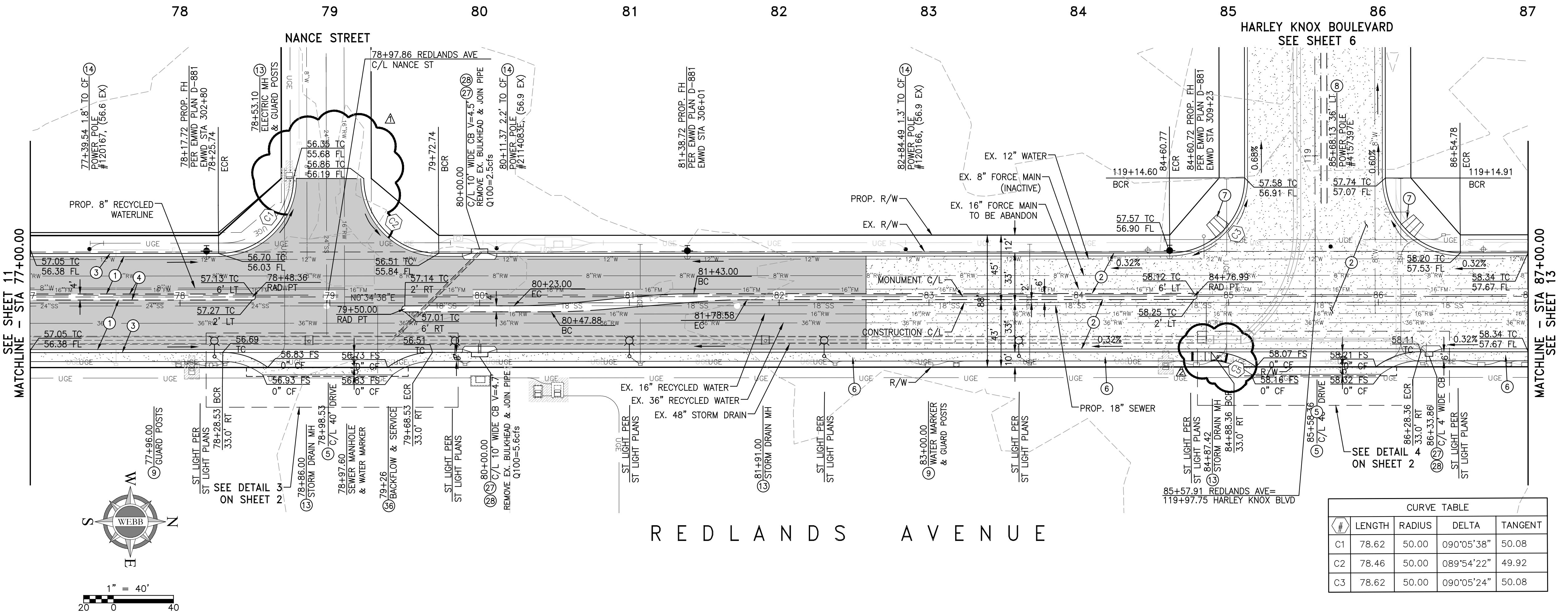
ADJUST TO GRADE

PROTECT IN PLACE

CONSTRUCT CURB INLET CATCH BASIN PER RIV. CO. STD. NO. 300

CONSTRUCT LOCAL DEPRESSION PER RIV. CO. STD. NO. 311

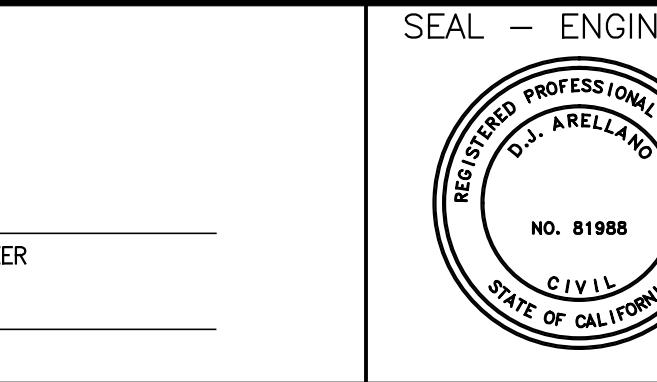
REMOVE BACKFLOW AND SERVICE. COORDINATE WITH EMWD



OTE:
WORK CONTAINED WITHIN THESE PLANS SHALL NOT
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AND/OR A GRADING PERMIT HAS BEEN ISSUED.

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DURING CONSTRUCTION, THE PRIVATE ENGINEER SHALL BE
RESPONSIBLE FOR DETERMINING AN ACCEPTABLE SOLUTION AND
REVISING THE PLANS FOR APPROVAL BY THE CITY.

CITY OF PERRIS
APPROVED BY



EER

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U
D

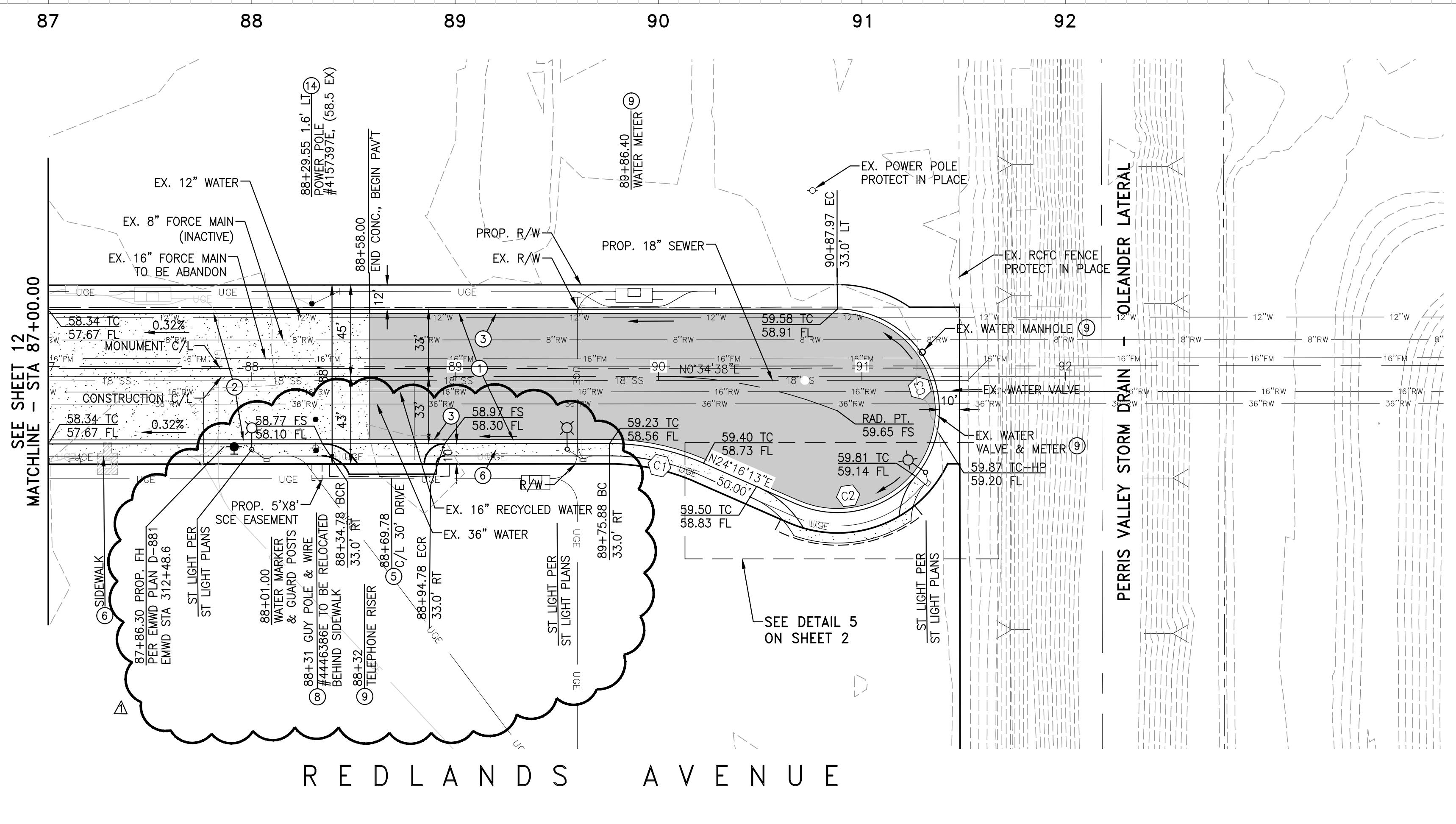
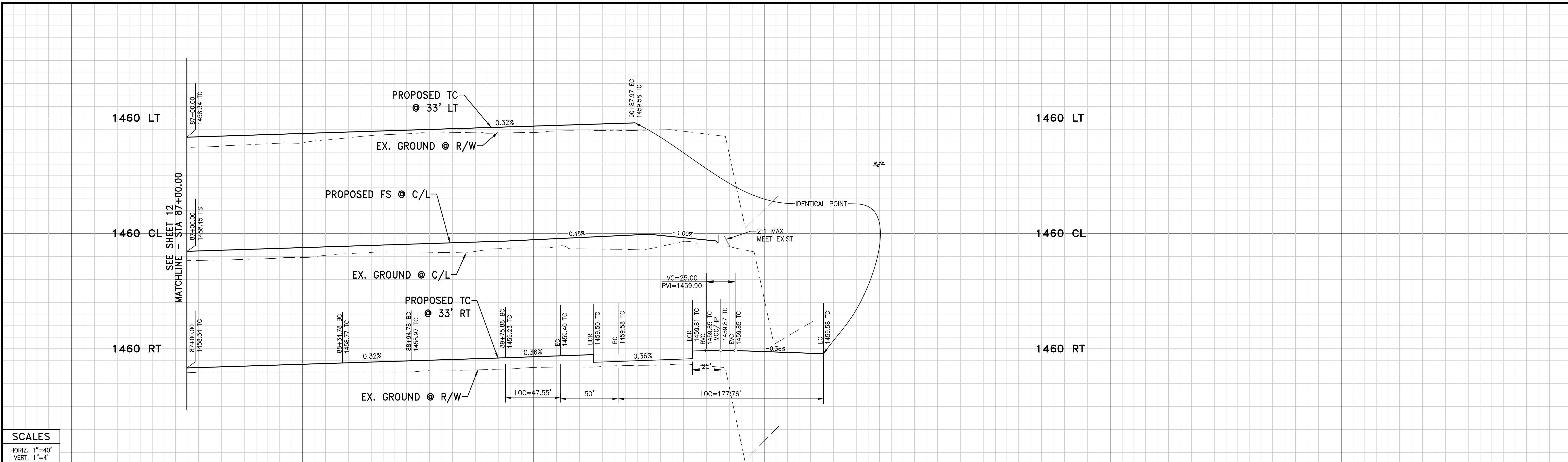
NSULTANTS
STREET
92506
6-1070
8-1256

2015
ATE

HMARK:
SEE SHEET 1

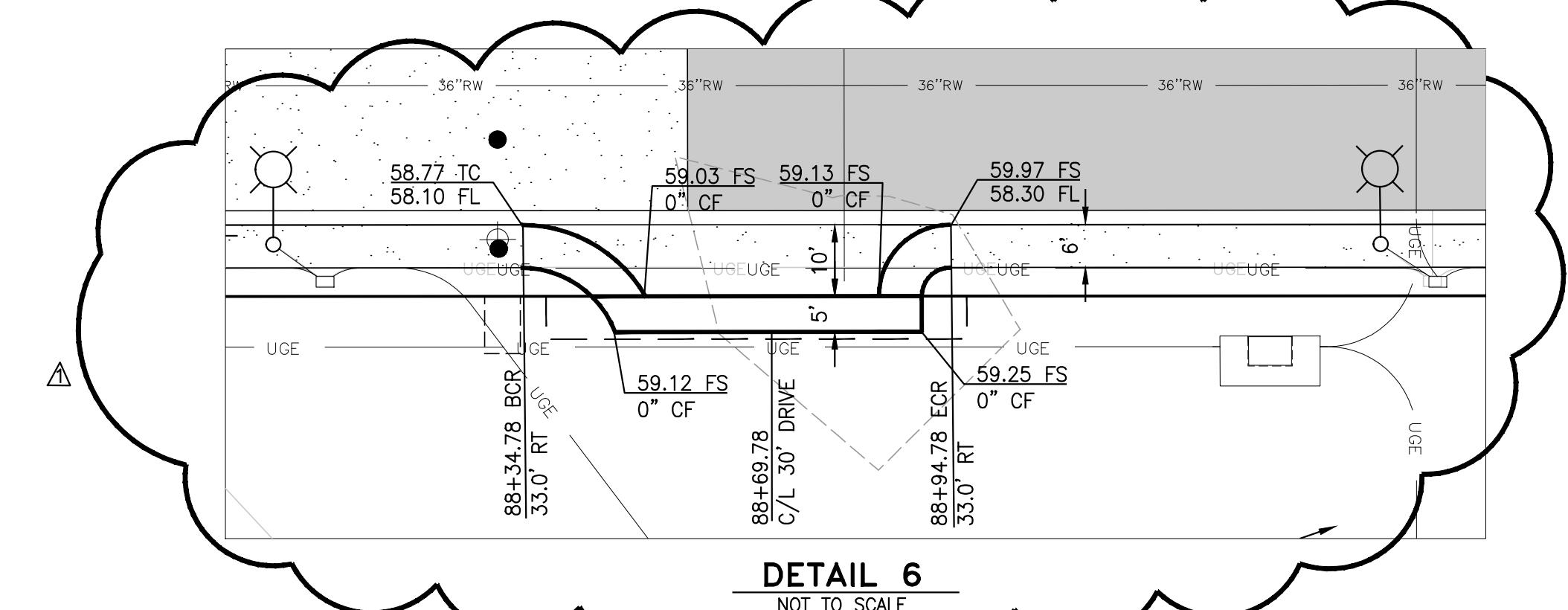
SHOWN V: AS SH

CITY OF PERRIS		SHEET NO.
AMENDED DPR NO. 11-12-0004 STRATFORD RANCH-PARCEL MAP 36469 REDLANDS AVENUE STA 78+00.00 TO STA 87+00.00		12 OF 23 SHEETS
FOR: <u>OWN</u>	W.O. IDI	CITY FILE NO. P8-1189
2013-0239		



- ## **CONSTRUCTION NOTES**

 -) CONSTRUCT MINIMUM 8" AC OVER 18" AB CLASS II
 -) CONSTRUCT MIN. 8" (4,000 PSI) PCC OVER 16" CLASS II AB (C.J. @ 20' O.C.)
 -) CONSTRUCT TYPE "A-8" CURB & GUTTER PER RIV. CO. STD. NO. 201
 -) CONSTRUCT 6' WIDE SIDEWALK PER RIV. CO. STD. 401
 -) COORD UNDERGROUNDING/RELOCATION OF PP
& GUY WIRE – BY UTILITY COMPANY
 -) RELOCATE EX. UTILITY RISER – BY UTILITY COMPANY
 -) PROTECT IN PLACE



CURVE TABLE				
	LENGTH	RADIUS	DELTA	TANGENT
C1	47.55	115.00	023°41'34"	24.12
C2	64.31	50.00	073°41'37"	37.47
C3	113.45	50.00	129°59'58"	107.22

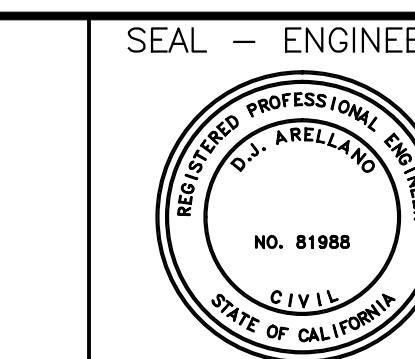
LEGEND:

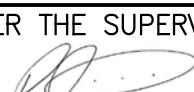
-  CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
-  REMOVE EXISTING AC PAVING
-  INSTALL 8" RCC CONCRETE OVER 16" AGGREGATE BASE

The DIG ALERT logo features the word "DIG" in a large, bold, outlined font at the top left, and "ALERT" in a similar style at the top right. A thick black circle containing a shovel and a pipe with a diagonal slash over it is positioned in the center. Below the logo, there are two rectangular boxes: one on the left with the text "DIAL BEFORE YOU DIG" and one on the right with "TWO WORKING DAYS BEFORE YOU DIG". At the bottom, there is a toll-free number "1-800-227-2600" and the text "A PUBLIC SERVICE BY UNDERGROUND SERVICE ALERT".

NOTE:
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CITY OF PERRIS
APPROVED BY

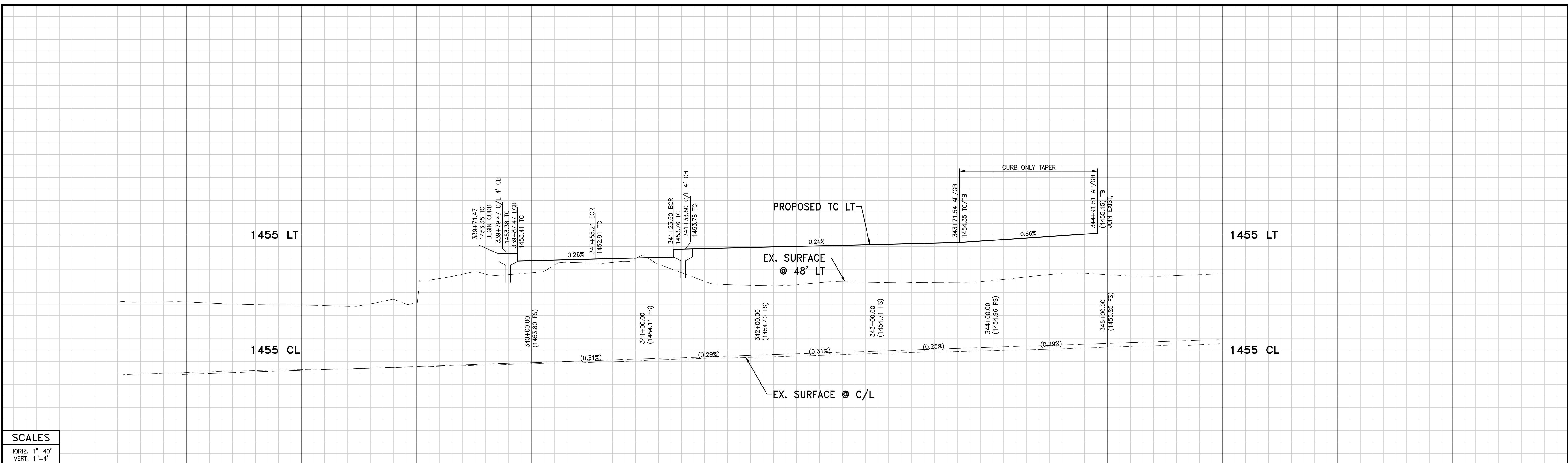


<u>A L B E R T</u> A. <hr/> WEBB <u>A S S O C I A T E S</u>	ENGINEERING CONSULTANTS 3788 McCRAY ST. RIVERSIDE CA. 92520 PH. (951) 686-1111 FAX (951) 788-1111	
UNDER THE SUPERVISION OF: 		
<hr/> D.J. ARELLANO	<hr/> R.C.E. #C81988	<hr/> DATE 1/12/2011

TS T 6 0 6	BENCHM SEE
------------------------	---------------

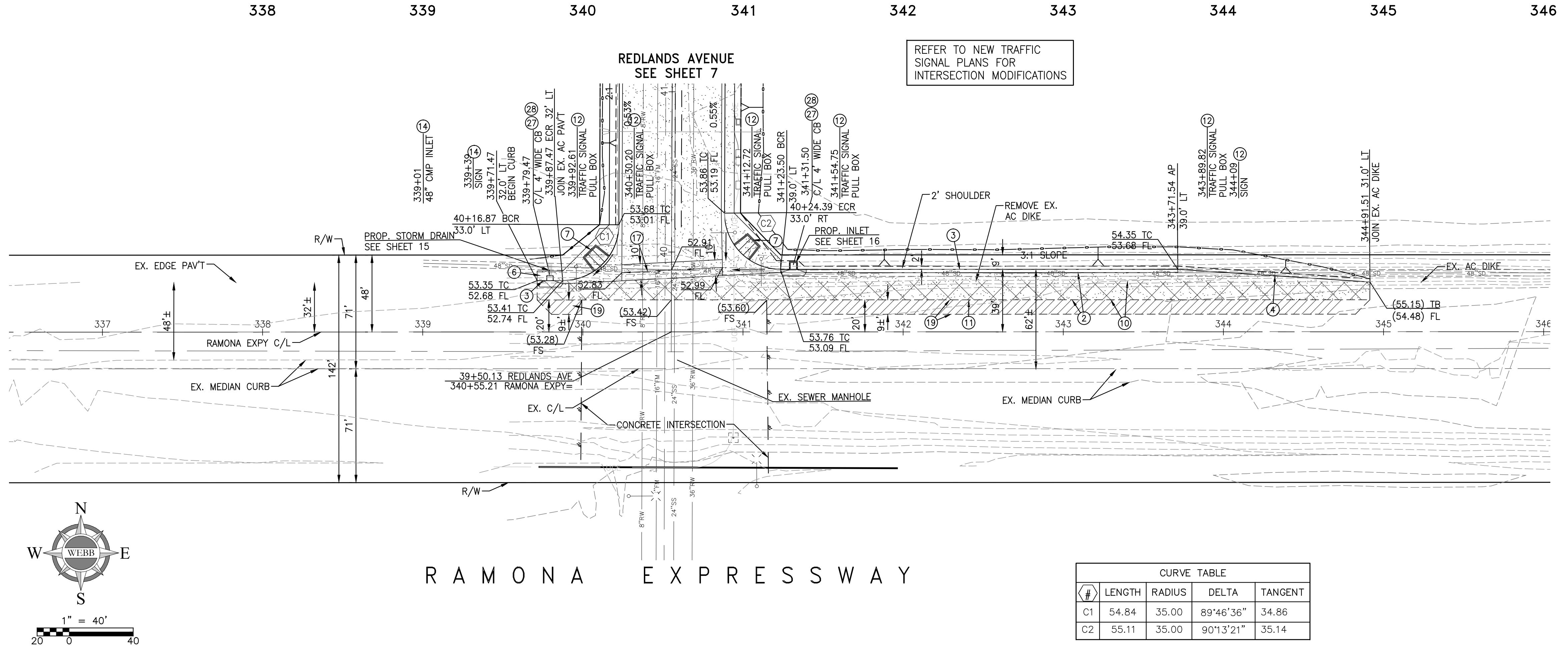
MARK:	CITY OF PERRIS	
SHEET 1	AMENDED DPR NO. 11-12-0004 STRATFORD RANCH-PARCEL MAP 36469 REDLANDS AVENUE STA 87+00.00 TO STA 91+58.00	

SHEET NO. 13
OF 23 SHEETS
P8-1189



SCALES

HORIZ. 1"=40'
VERT. 1"=4'

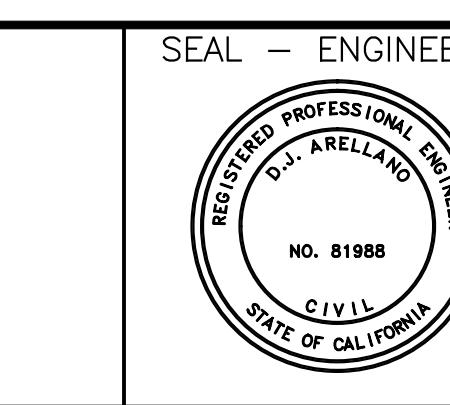


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MARK	BY	DATE	REVISIONS	APPR.	DATE
ENGINEER			CITY		

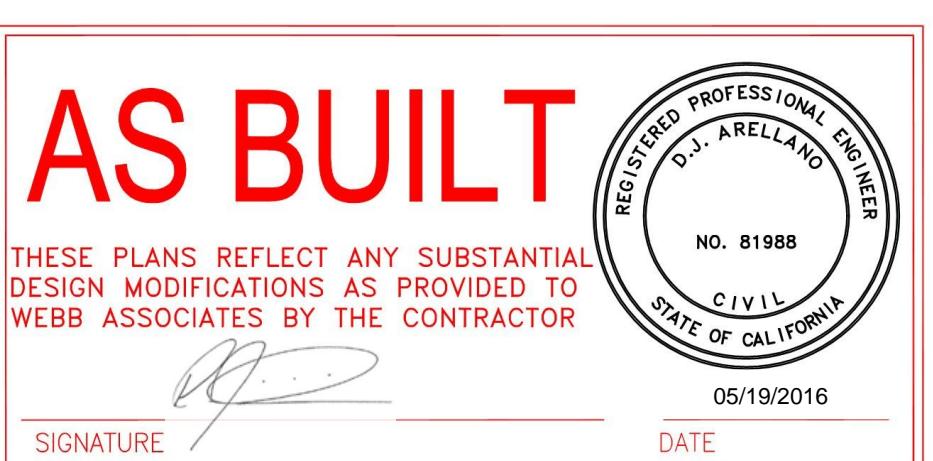
CITY OF PERRIS
APPROVED BY:
CITY ENGINEER
DATE



ALBERT A. WEBB
ASSOCIATES
ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 686-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #C81988
1/12/2015
DATE

BENCHMARK:
SEE SHEET 1
SCALE: H: AS SHOWN V: AS SHOWN
FOR: IDI
W.O. 2013-0239
CITY FILE NO. P8-1189

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
RAMONA EXPRESSWAY
STA 114+00.00 TO STA 119+93.75
SHEET NO. 14 OF 23 SHEETS

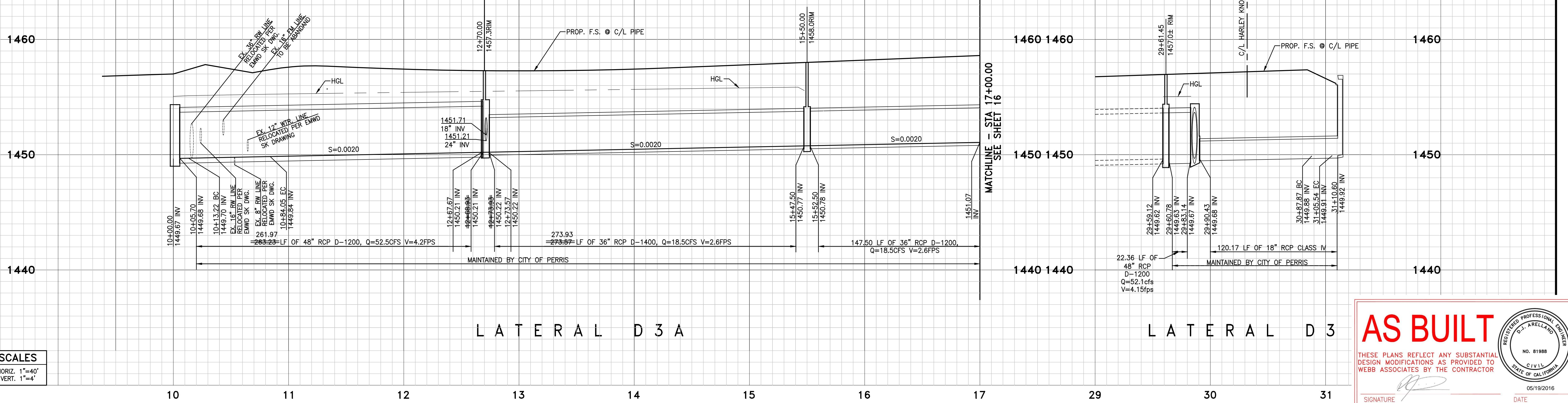


LEGEND:

- CONSTRUCT 8" AC OVER 18" AGGREGATE BASE
- REMOVE EXISTING AC PAVING
- INSTALL 8" PCC CONCRETE OVER 16" AGGREGATE BASE

NOTE TO CONTRACTOR

1. CONTRACTOR TO VERIFY LOCATIONS AND ELEVATIONS OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION



AS BUILT

THESE PLANS REFLECT ANY SUBSTANTIAL DESIGN MODIFICATIONS AS PROVIDED TO WEBB ASSOCIATES BY THE CONTRACTOR



05/19/2016

SIGNATURE

DATE

SCALES

HORIZ. 1"=40'
VERT. 1"=4'

CURVE DATA

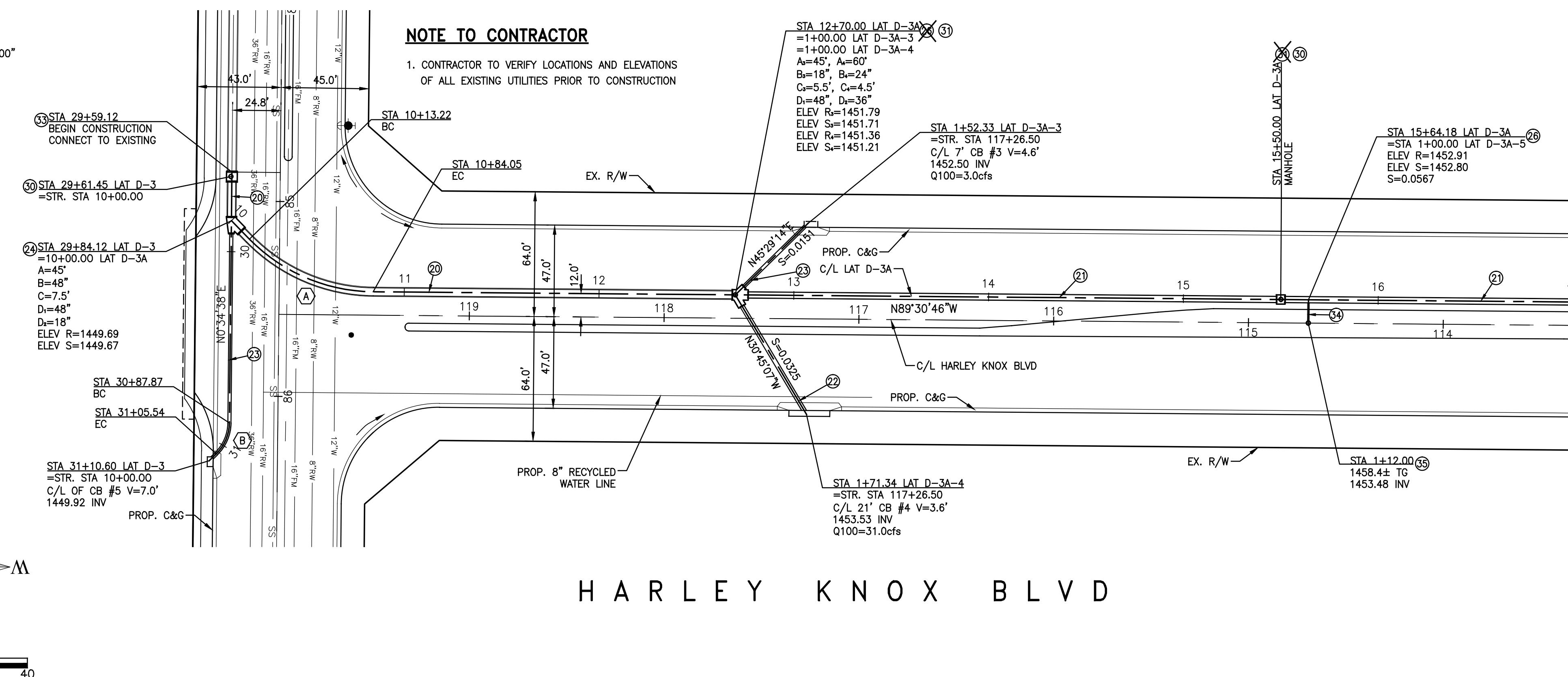
(A) $\Delta=45^{\circ}0'24''$
R=90.0'
L=70.83'
T=37.36'

(B) $\Delta=45^{\circ}0'00''$
R=22.5'
L=17.67'
T=9.32'

REDLANDS AVE

NOTE TO CONTRACTOR

1. CONTRACTOR TO VERIFY LOCATIONS AND ELEVATIONS OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION

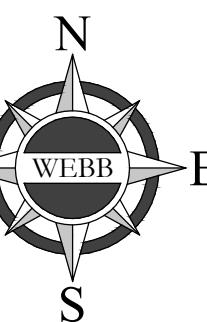
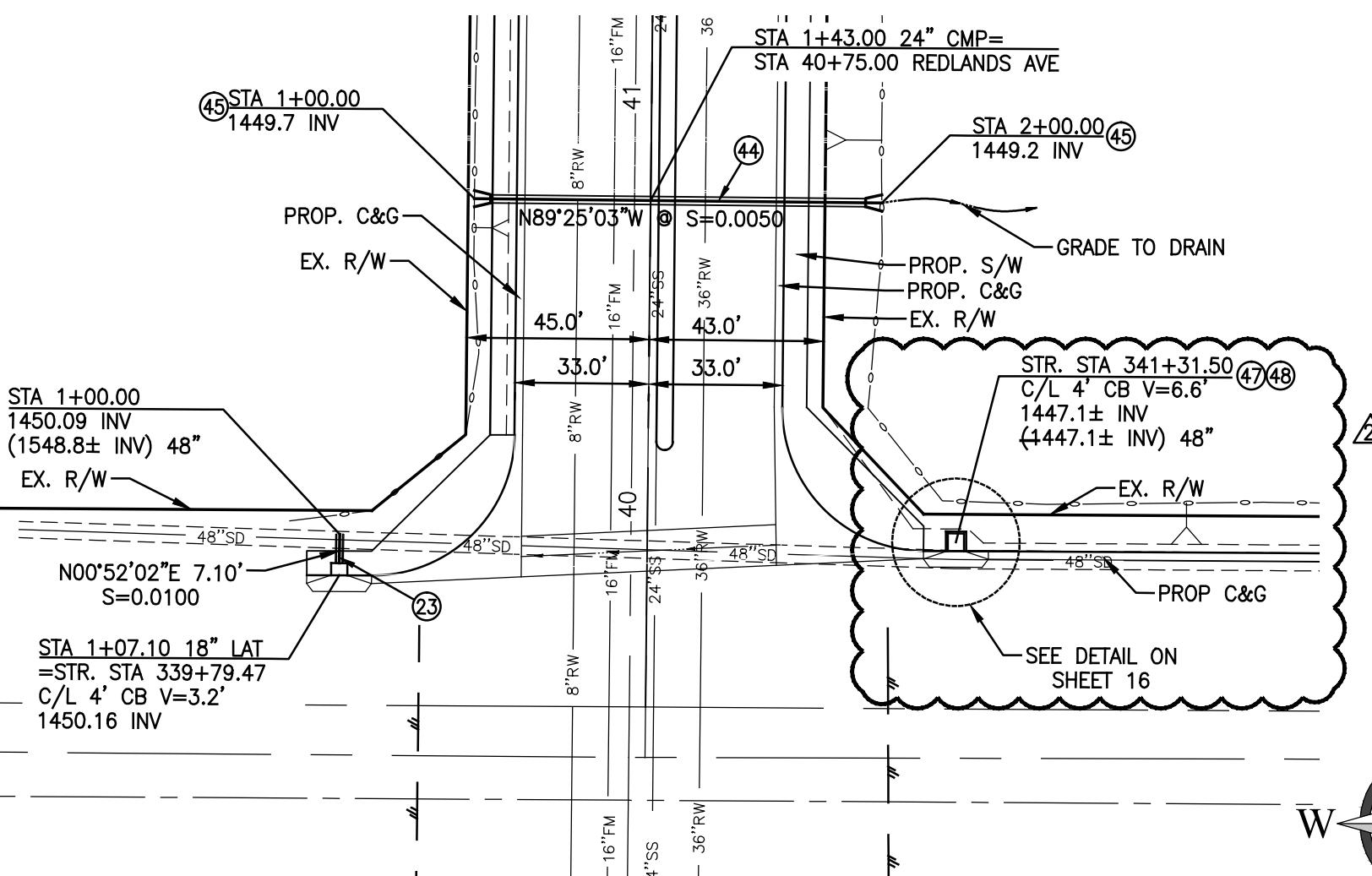


NOTE TO CONTRACTOR

1. CONTRACTOR TO VERIFY LOCATIONS AND ELEVATIONS OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION

MATCHLINE - STA 17+00.00
SEE SHEET 16

REDLANDS AVE



RAMONA EXPRESSWAY

CONSTRUCTION NOTES

- (20) INSTALL 48" RCP (D-LOAD PER PLAN)
- (21) INSTALL 36" RCP (D-LOAD PER PLAN)
- (22) INSTALL 24" RCP (D-LOAD PER PLAN)
- (23) INSTALL 18" RCP (D-LOAD PER PLAN)
- (24) CONSTRUCT JUNCTION STRUCTURE NO 2 PER RCF&WCD STD. JS227
- (25) CONSTRUCT JUNCTION STRUCTURE NO. 4 PER RCF&WCD STD JS229
- (26) CONSTRUCT MANHOLE NO. 2 PER RCF&WCD STD. MH252
- (27) CONSTRUCT MANHOLE NO. 4 PER RCF&WCD STD. MH254
- (28) REMOVE CONCRETE BULKHEAD
- (29) INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL)
- (30) INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE
- (31) INSTALL 24" CMP HEL-COR PIPE ("CONTECH" OR APPROVED EQUAL)
- (32) INSTALL 24" FLARED END SECTION ("CONTECH" OR APPROVED EQUAL)
- (33) CONSTRUCT LOCAL DEPRESSION GRATING CATCH BASIN PER SPPWC STD 303-3 AND DETAIL ON SHEET 16
- (34) CONSTRUCT MODIFIED GRATING CATCH BASIN PER SPPWC STD 313-3 CASE C
- (35) CONSTRUCT MANHOLE NO. 4 PER RCF&WCD STD. MH254
- (36) REMOVE CONCRETE BULKHEAD
- (37) INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL)
- (38) INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE
- (39) INSTALL 24" CMP HEL-COR PIPE ("CONTECH" OR APPROVED EQUAL)
- (40) INSTALL 24" FLARED END SECTION ("CONTECH" OR APPROVED EQUAL)
- (41) CONSTRUCT LOCAL DEPRESSION GRATING CATCH BASIN PER SPPWC STD 303-3 AND DETAIL ON SHEET 16
- (42) CONSTRUCT MODIFIED GRATING CATCH BASIN PER SPPWC STD 313-3 CASE C

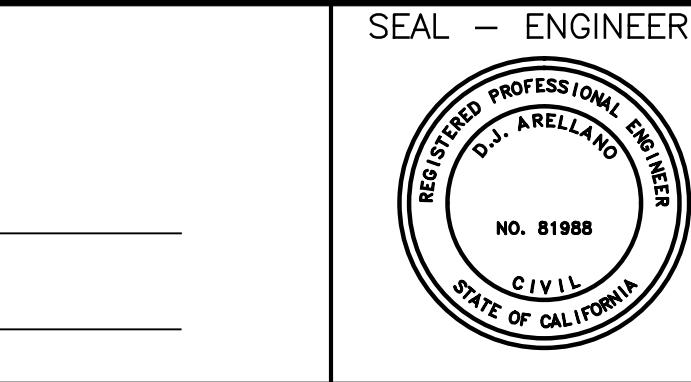


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DJ	5/29/15	CATCH BASIN REVISED PER FIELD CONDITIONS
MARK	BY DATE	REVISIONS
ENGINEER	APPR. DATE	CITY

CITY OF PERRIS
APPROVED BY:



ALBERT A.
WEBB
ASSOCIATES

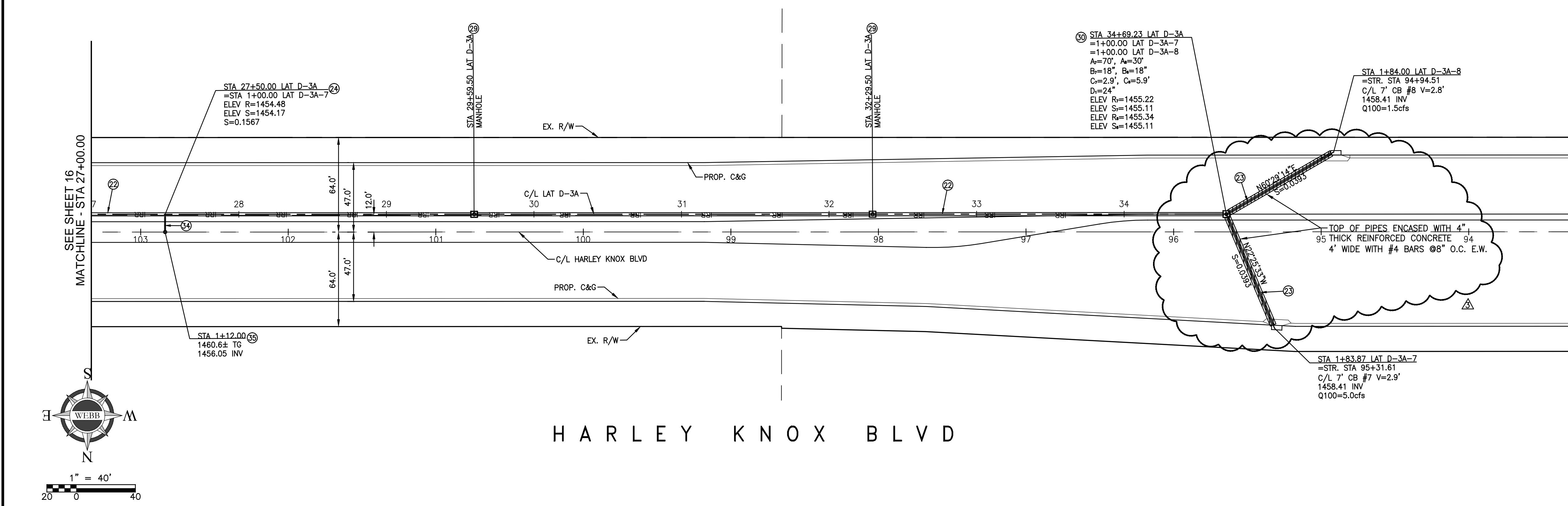
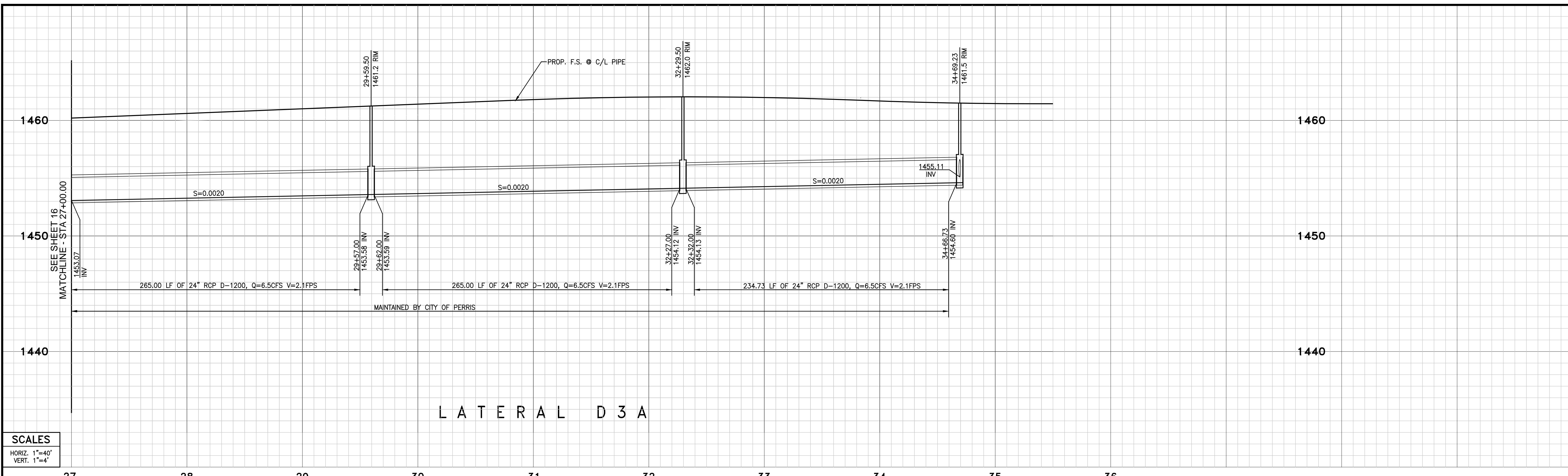
REGISTERED PROFESSIONAL ENGINEER
NO. 81988
CIVIL
STATE OF CALIFORNIA

ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 686-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #081988
1/12/2015
DATE

BENCHMARK:
SEE SHEET 1
SCALE:
H: AS SHOWN V: N/A
FOR:
W.O.:
2013-0239
CITY FILE NO.
P8-1189

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STORM DRAIN IMPROVEMENT PLANS
LATERAL D-3, D-3A
STA 29+84.12-STA 31+10.60/STA 10+00-STA 17+00

SHEET NO.
15
OF 23 SHEETS
G:\2013\1\3-0239\DRAWINGS\DES\1-3-0239-C-SD.DWG 5/17/2016 2:42 PM



CONSTRUCTION NOTES

- (22) INSTALL 24" RCP (D-LOAD PER PLAN)
 - (23) INSTALL 18" RCP (D-LOAD PER PLAN)
 - (24) CONSTRUCT JUNCTION STRUCTURE NO 2 PER RCFC&WCD STD. JS227
 - (29) CONSTRUCT MANHOLE NO. 1 PER RCFC&WCD STD. MH251
 - (31) CONSTRUCT MANHOLE NO. 4 PER RCFC&WCD STD. MH254
 - (34) INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL)
 - (35) INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE

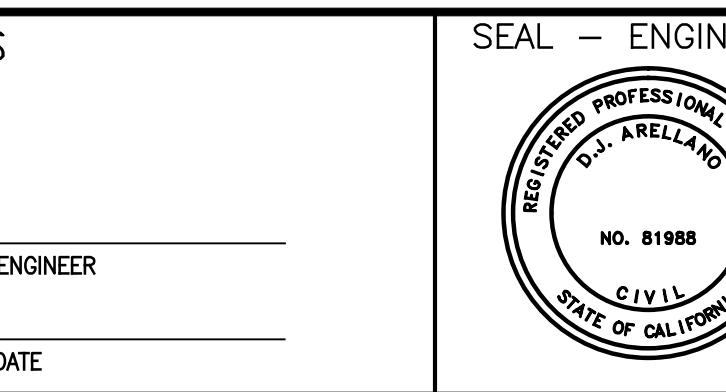
AS BUILT



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CITY OF PERRIS
APPROVED BY



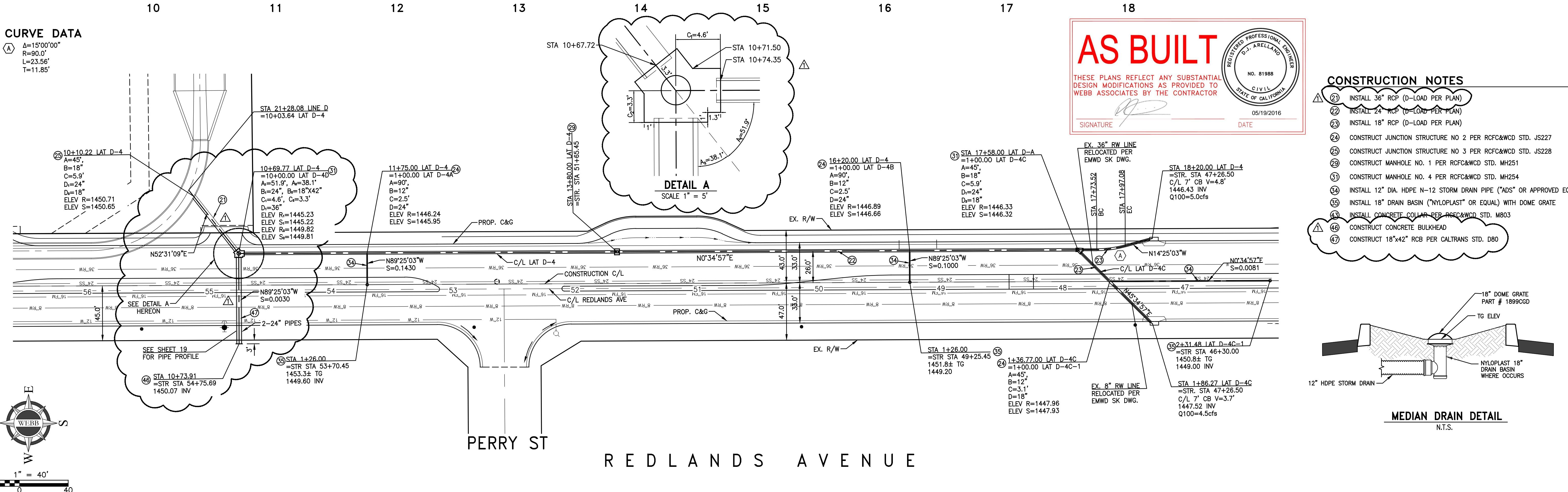
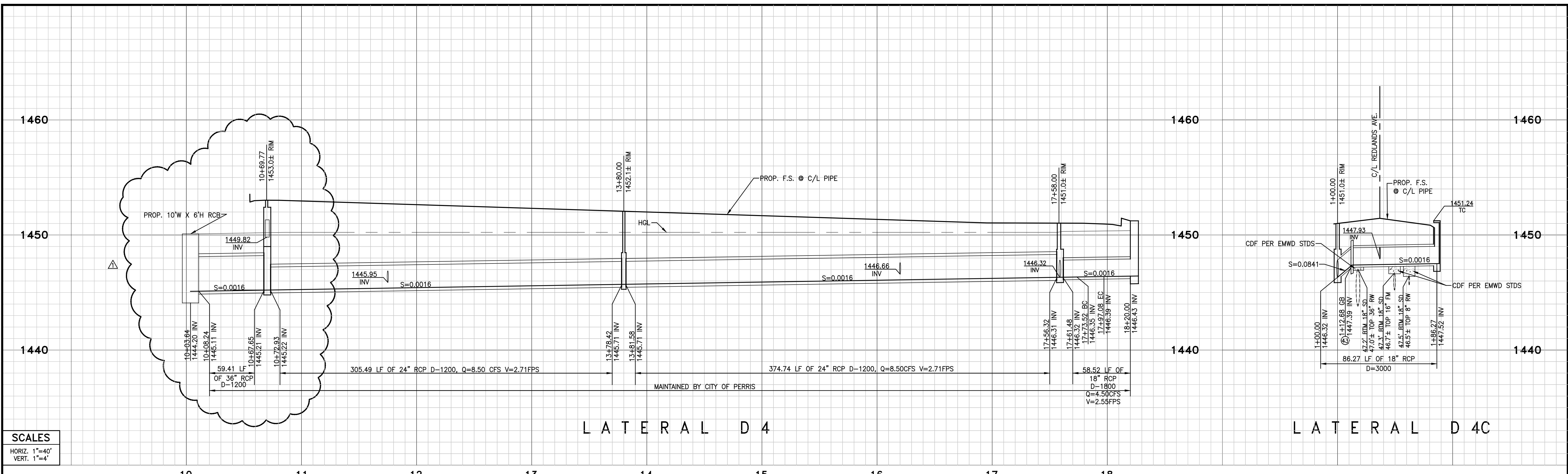
EER | A

BENCHM

MARK:

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STORM DRAIN IMPROVEMENT PLANS
LATERAL D-3A
STA 27+00-STA 34+69 23

SHEET NO.
17
OF 23 SHEETS
P8-1189

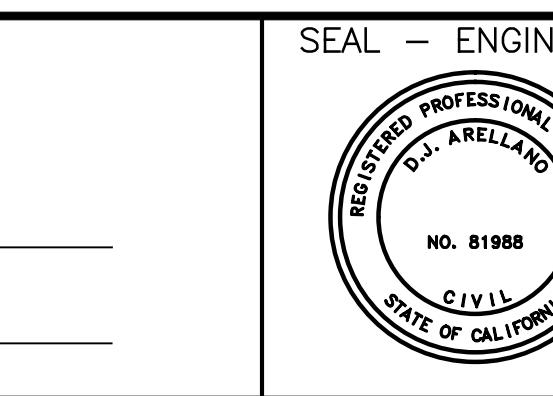


The DIG A LERT logo features the words "DIG A LERT" in large, bold, outlined letters. Below the letters is a decorative wavy line. In the center is a circular graphic with a thick black border. Inside the circle is a white area with a large diagonal black slash from top-left to bottom-right. Overlaid on the circle is a black silhouette of a shovel digging into the ground, with a pipe visible nearby.

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CITY OF PERRIS
APPROVED BY



EER	ALBERT A. WEBB ASSOCIATES	ENGINEERING 3788 McCARTHY RIVERSIDE PH. (951) FAX (951)
UNDER THE SUPERVISION OF: 		
<hr/> D.J. ARELLANO		<hr/> R.C.E. #C81988

G CONSULTANTS
CRAY STREET
CA. 92506
686-1070
788-1256

1/12/2015

DATE

BENCHMARK
SEE SHEET
SCALE:
H: AS SHOWN

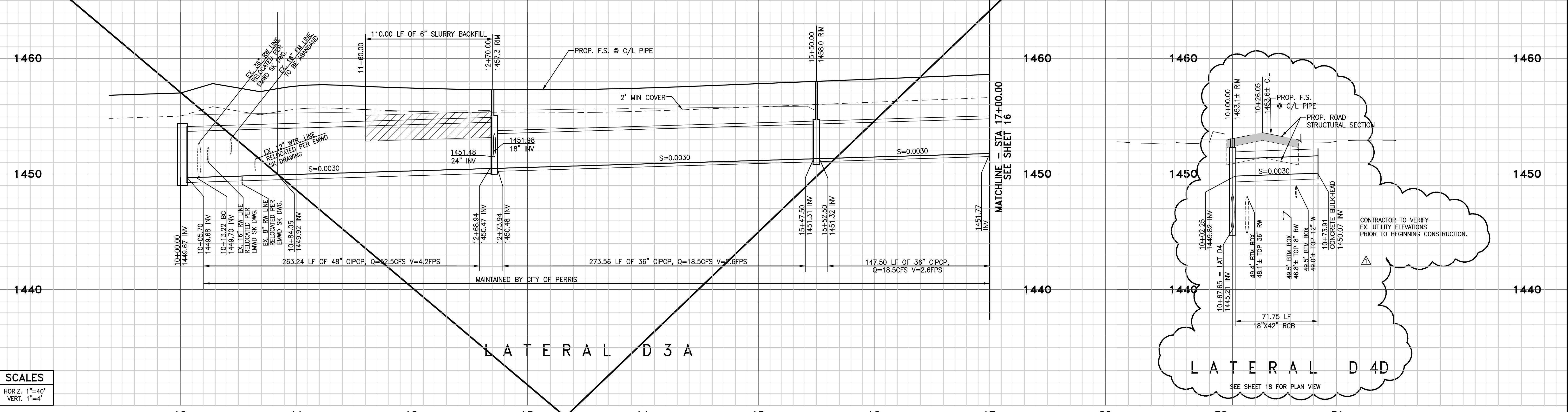
K: ET 1	CITY OF PERRIS AMENDED DPR NO. 11-12-000 STORM DRAIN IMPROVEMENT PLANS LATERAL D-4, D-4A
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SHEET NO.
18
OF 23 SHEETS

P8-1189

NOTE TO CONTRACTOR

1. CONTRACTOR TO VERIFY LOCATIONS AND ELEVATIONS OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION



CURVE DATA

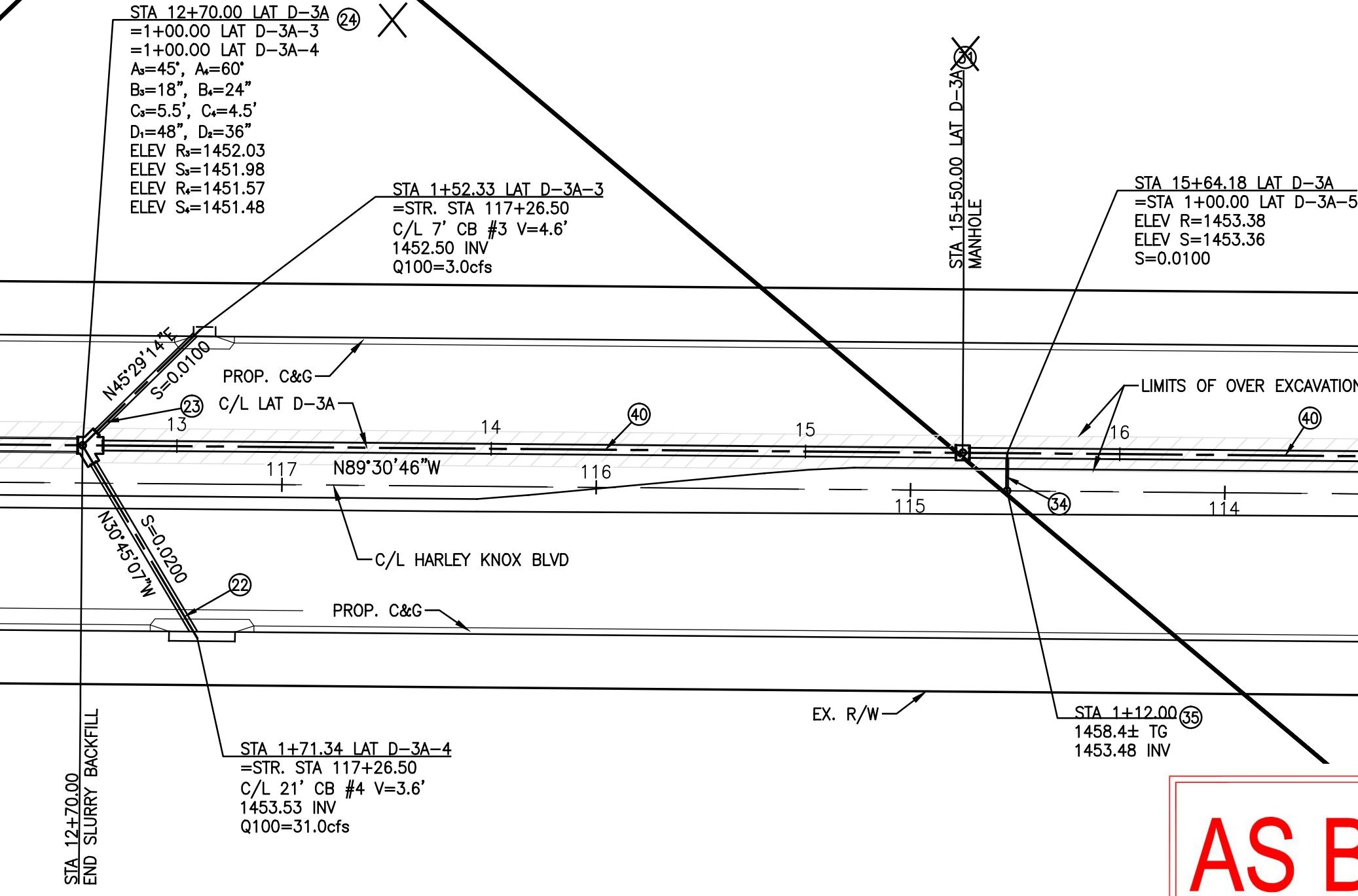
(A) $\Delta=45^{\circ}24'$
R=90.0'
L=70.83'
T=37.36'

(B) $\Delta=45^{\circ}00'00"$
R=22.5'
L=17.67'
T=9.32'

REDLANDS AVE

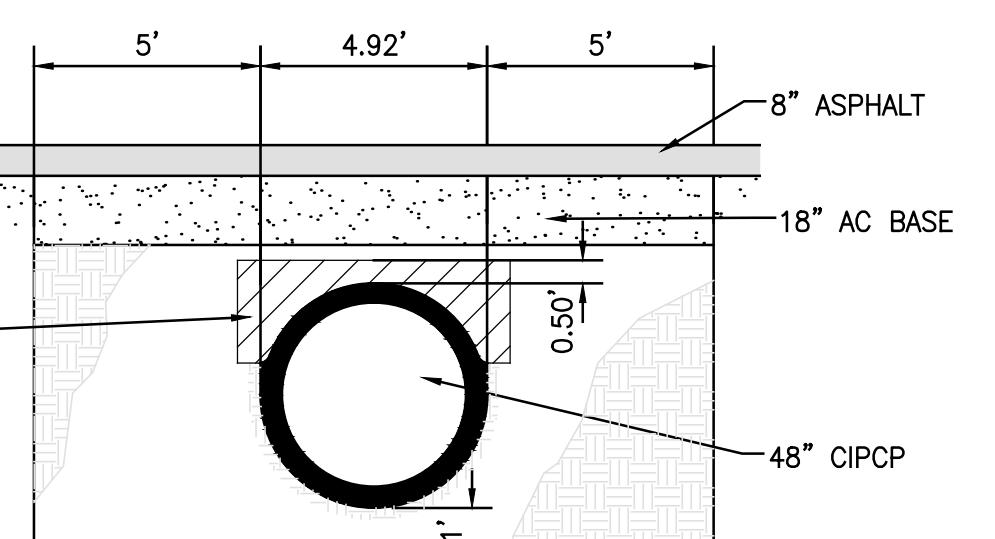
NOTE TO CONTRACTOR

1. CONTRACTOR TO VERIFY LOCATIONS AND ELEVATIONS OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION



CONSTRUCTION NOTES

- (22) INSTALL 24" RCP (D-LOAD PER PLAN)
- (23) INSTALL 18" RCP (D-LOAD PER PLAN)
- (24) CONSTRUCT JUNCTION STRUCTURE NO 2 PER RCF&WCD STD. JS227
- (25) CONSTRUCT JUNCTION STRUCTURE NO. 4 PER RCF&WCD STD JS229
- (30) CONSTRUCT MANHOLE NO. 2 PER RCF&WCD STD. MH252
- (31) CONSTRUCT MANHOLE NO. 4 PER RCF&WCD STD. MH254
- (33) REMOVE CONCRETE BULKHEAD
- (34) INSTALL 12" DIA. HDPE N-12 STORM DRAIN PIPE ("ADS" OR APPROVED EQUAL)
- (35) INSTALL 18" DRAIN BASIN ("NYLOPLAST" OR EQUAL) WITH DOME GRATE
- (39) INSTALL 48" CIPCP PER MANUFACTURES SPECS
- (40) INSTALL 36" CIPCP PER MANUFACTURES SPECS
- (42) INSTALL 6" SLURRY BACKFILL (2 SACK)

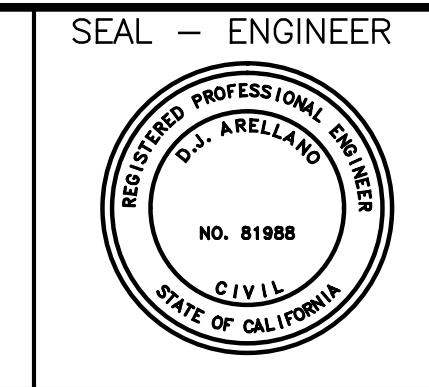


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APPROVED BY:		CITY OF PERRIS		SEAL - ENGINEER	
D.J. ARELLANO	REG. PROFESSIONAL ENGINEER NO. 81988 CIVIL STATE OF CALIFORNIA	CITY ENGINEER			
D.J. ARELLANO	REG. PROFESSIONAL ENGINEER NO. 81988 CIVIL STATE OF CALIFORNIA				
DATE					

CITY OF PERRIS
APPROVED BY:
CITY ENGINEER
DATE



ALBERT A. WEBB & ASSOCIATES
ENGINEERING CONSULTANTS
3788 McCRAY STREET
RIVERSIDE CA. 92506
PH. (951) 686-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #081988
DATE
1/12/2015

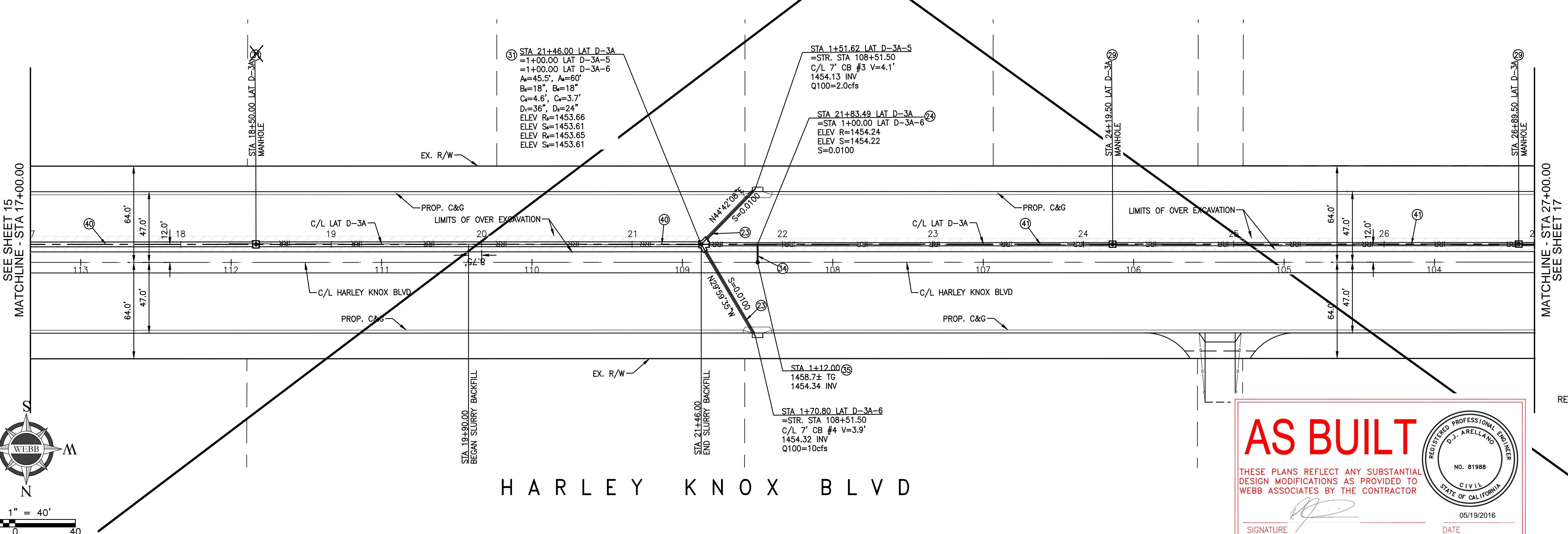
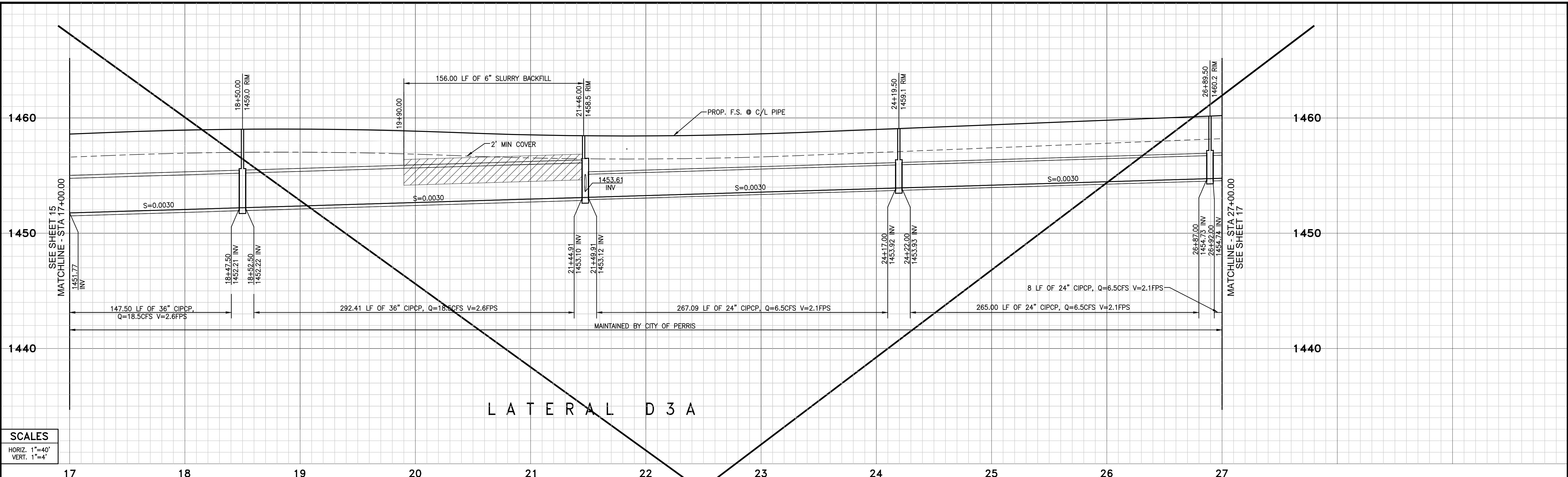
BENCHMARK:
SEE SHEET 1

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STORM DRAIN IMPROVEMENT PLANS
CIPCP - ALTERNATE BID ITEM LATERAL D-3A
STA 10+00-STA 17+00

SHEET NO.	19
OF	23
SHEETS	

FOR: W.O. 2013-0239 CITY FILE NO. P8-1189

SCALE: H: AS SHOWN V: N/A

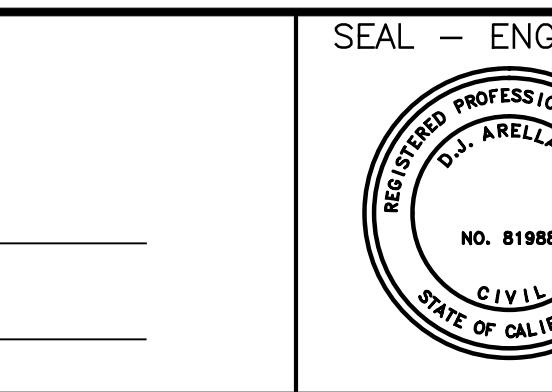


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D.J.M	5/17/16	RCP USED IN LIEU OF CIP SD PIPES
MARK	BY DATE	REVISIONS
ENGINEER	APPR. DATE	CITY

CITY OF PERRIS
APPROVED BY:
CITY ENGINEER
DATE



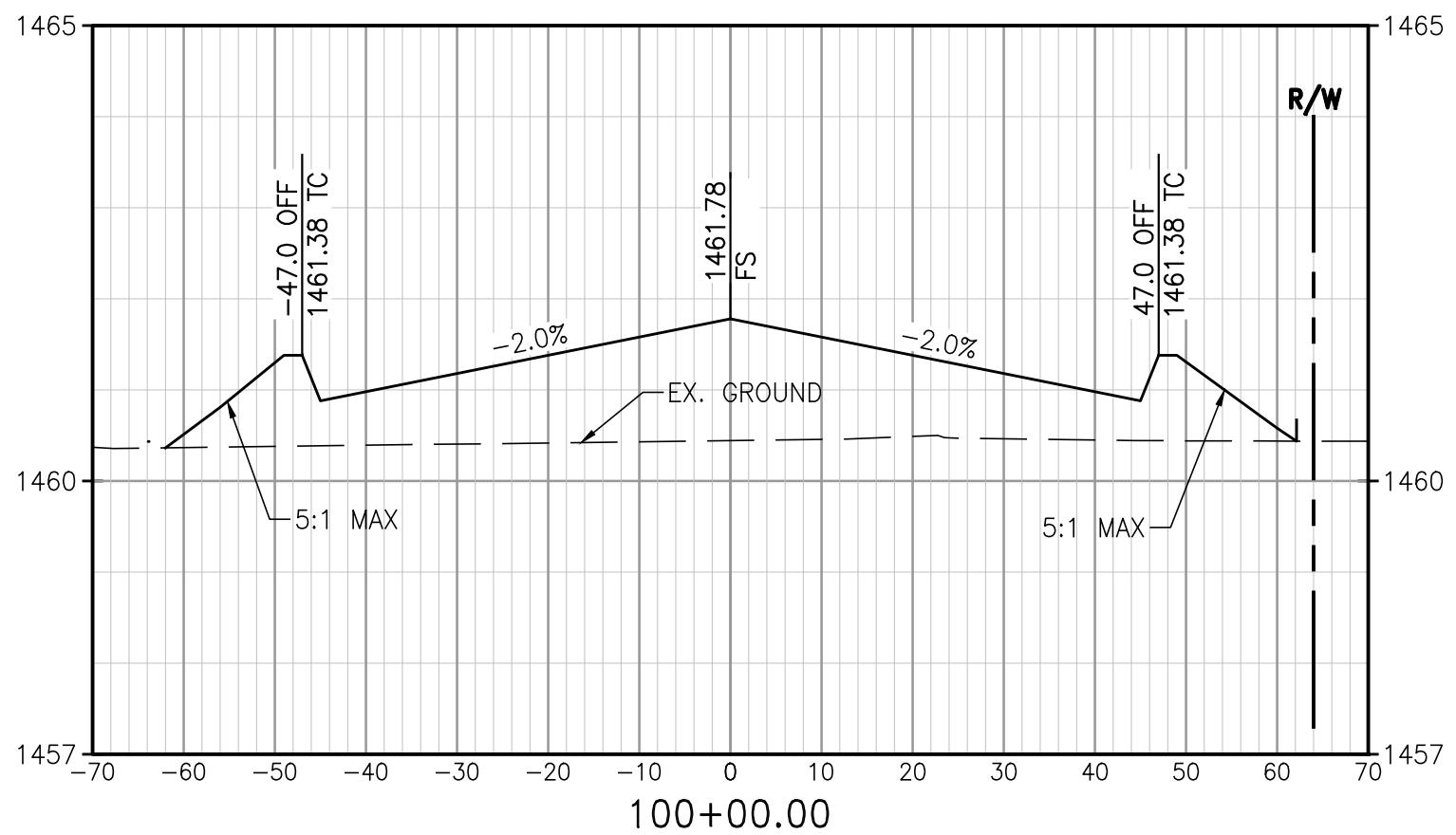
ALBERT A. WEBB
ASSOCIATES
REGISTERED PROFESSIONAL ENGINEERS
NO. 81988
CIVIL
STATE OF CALIFORNIA
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #081988
1/12/2015
DATE

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STORM DRAIN IMPROVEMENT PLANS
CIPCP - ALTERNATE BID ITEM LATERAL D-3A
STA 17+00-STA 27+00

SHEET NO.	20
OF	23
SHEETS	

FOR: W.O. 2013-0239 CITY FILE NO. P8-1189

SCALE: H: AS SHOWN V: N/A



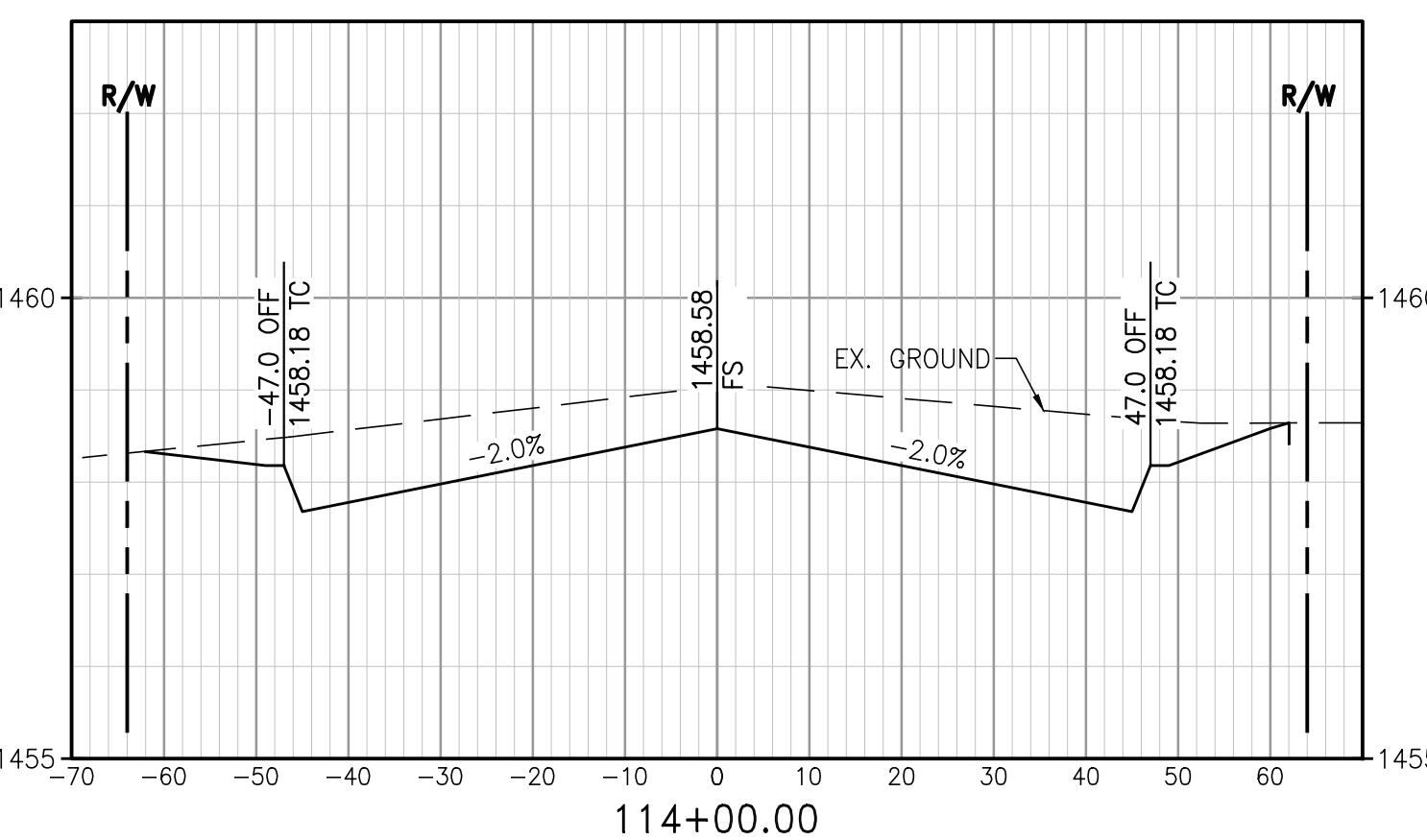
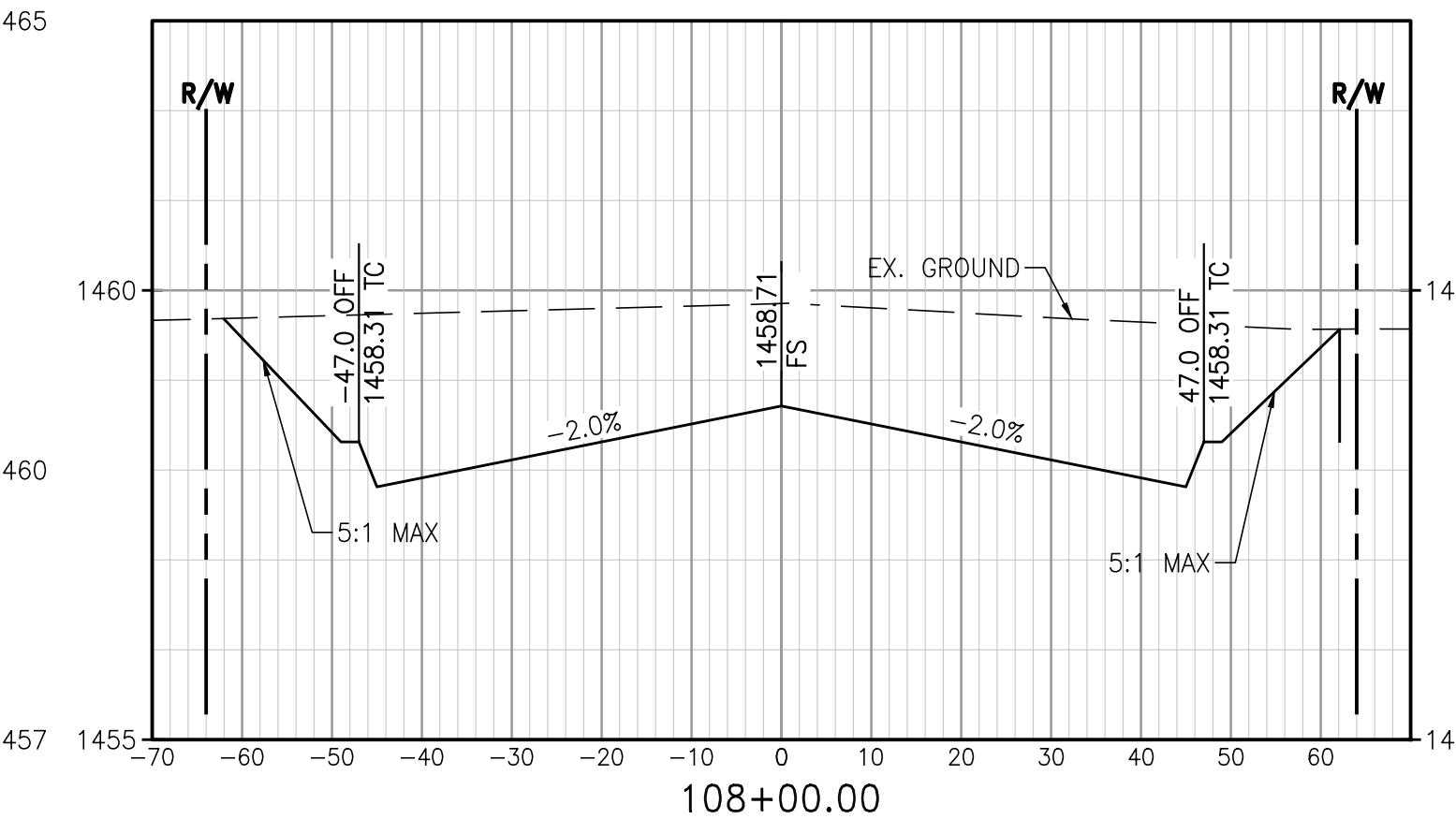
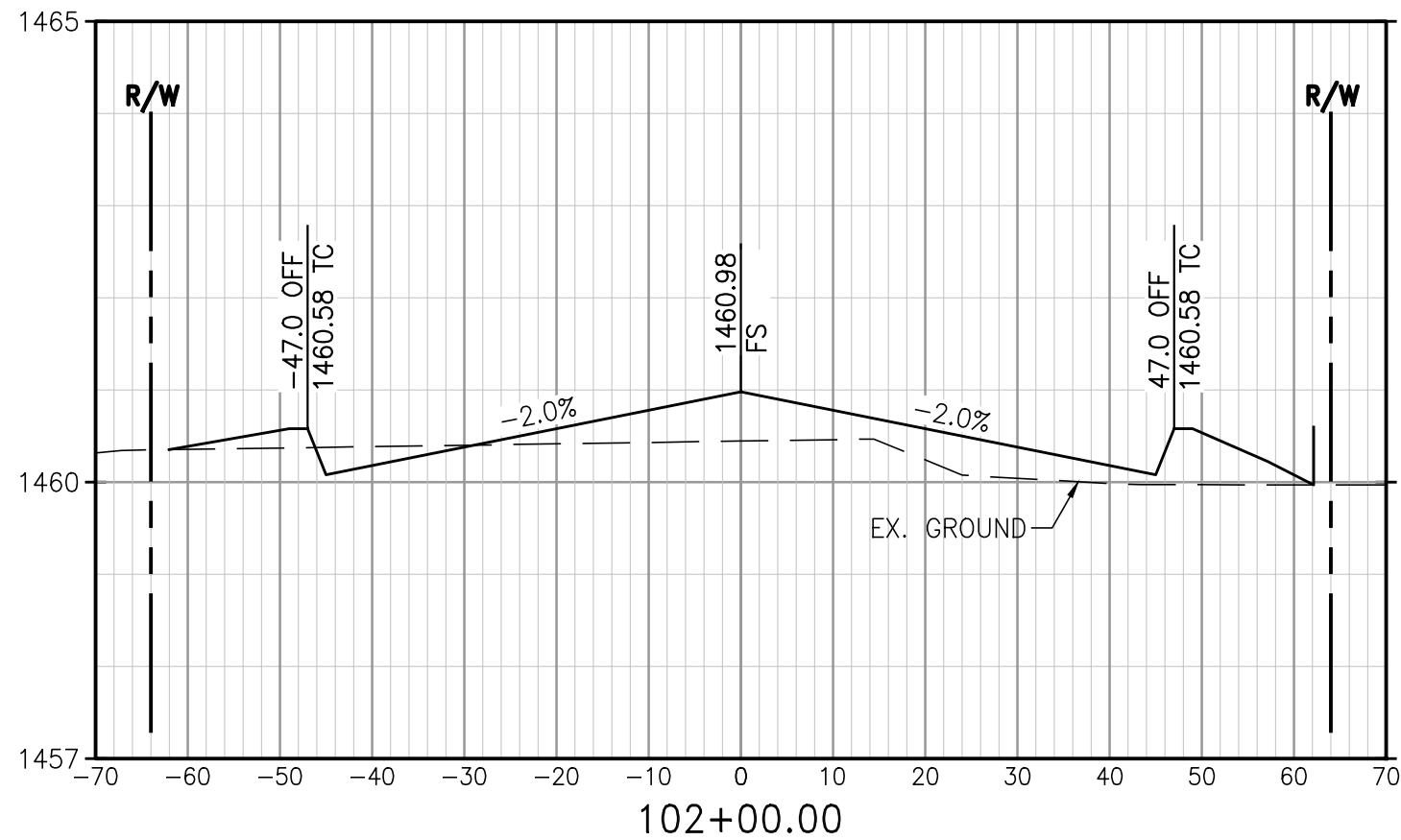
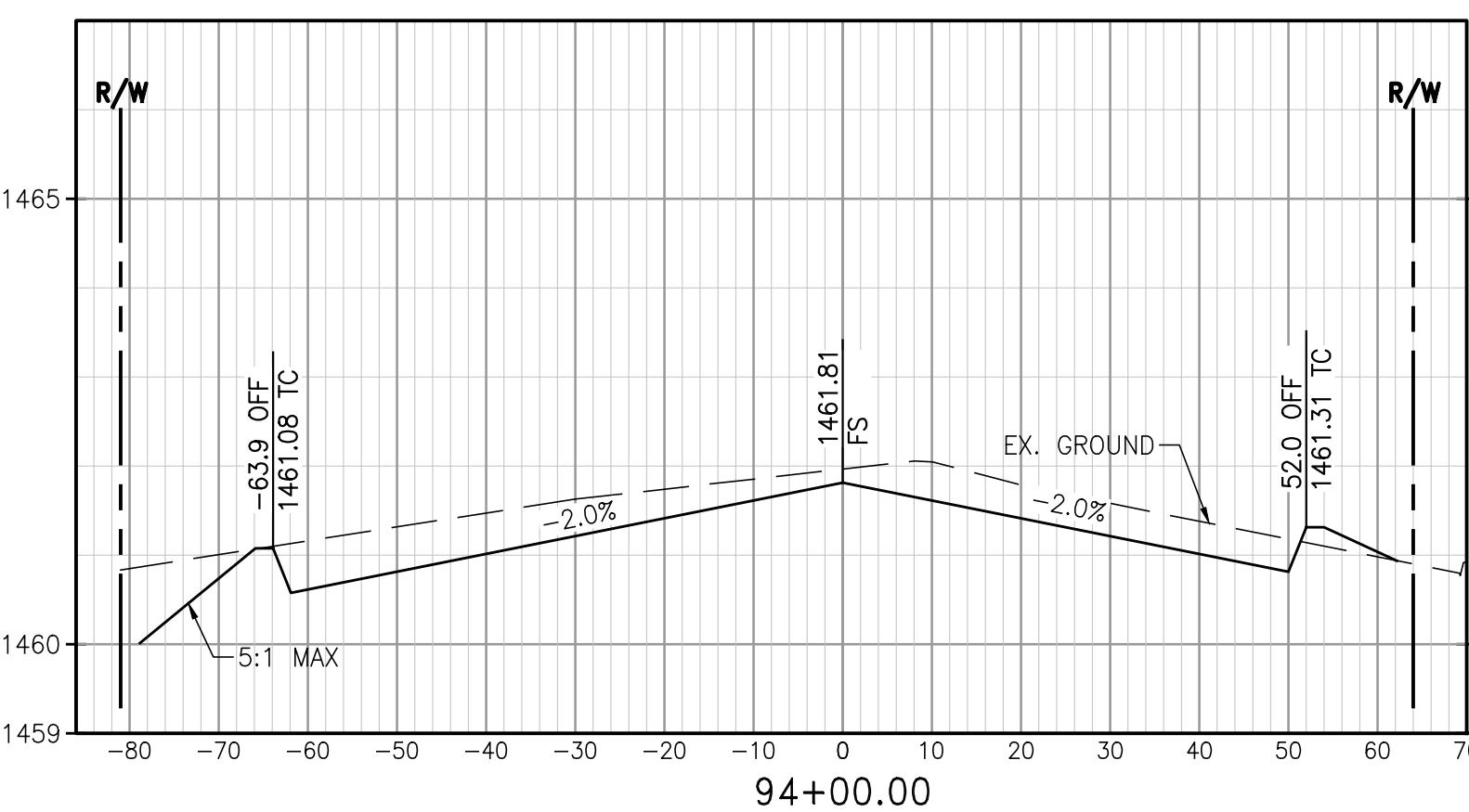
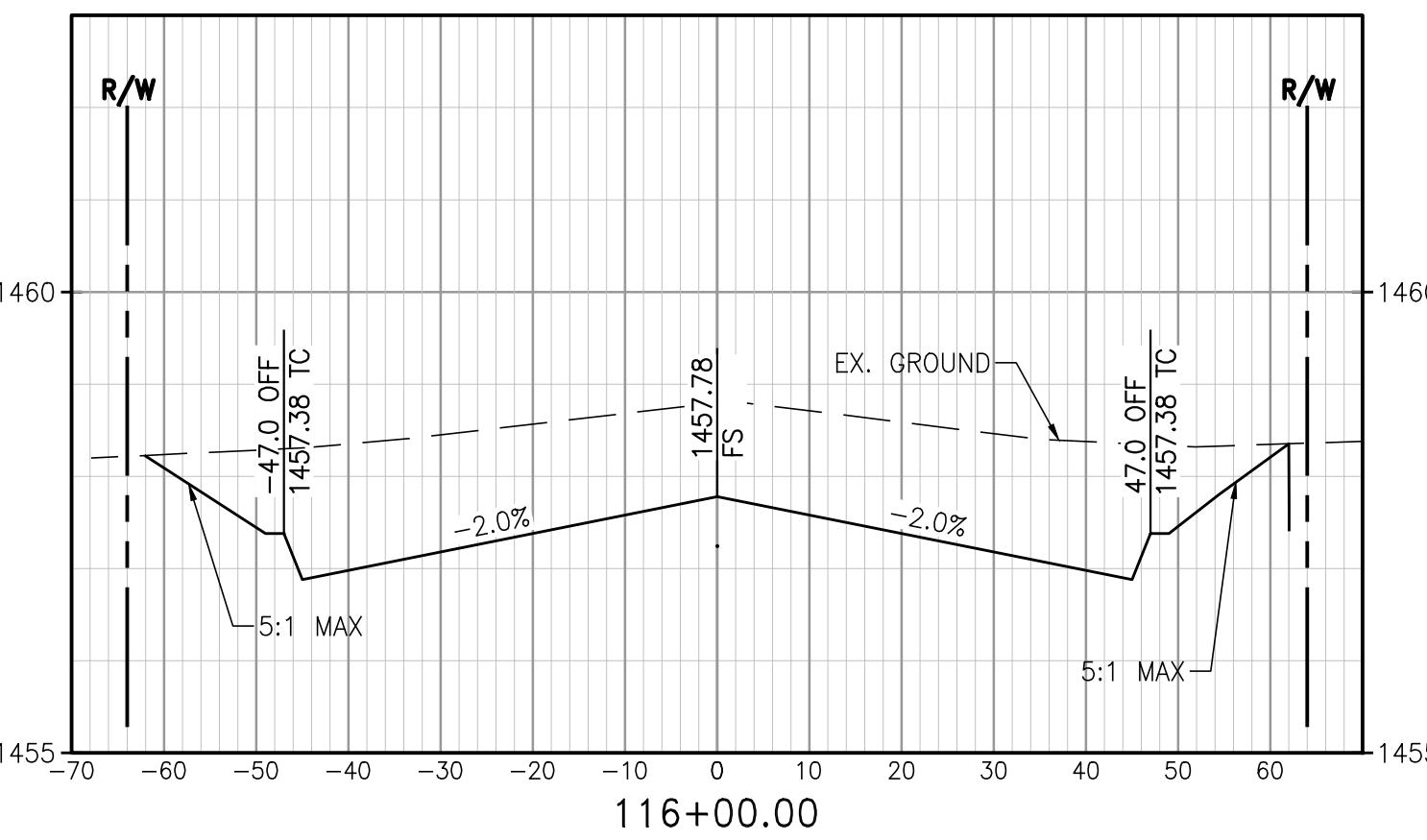
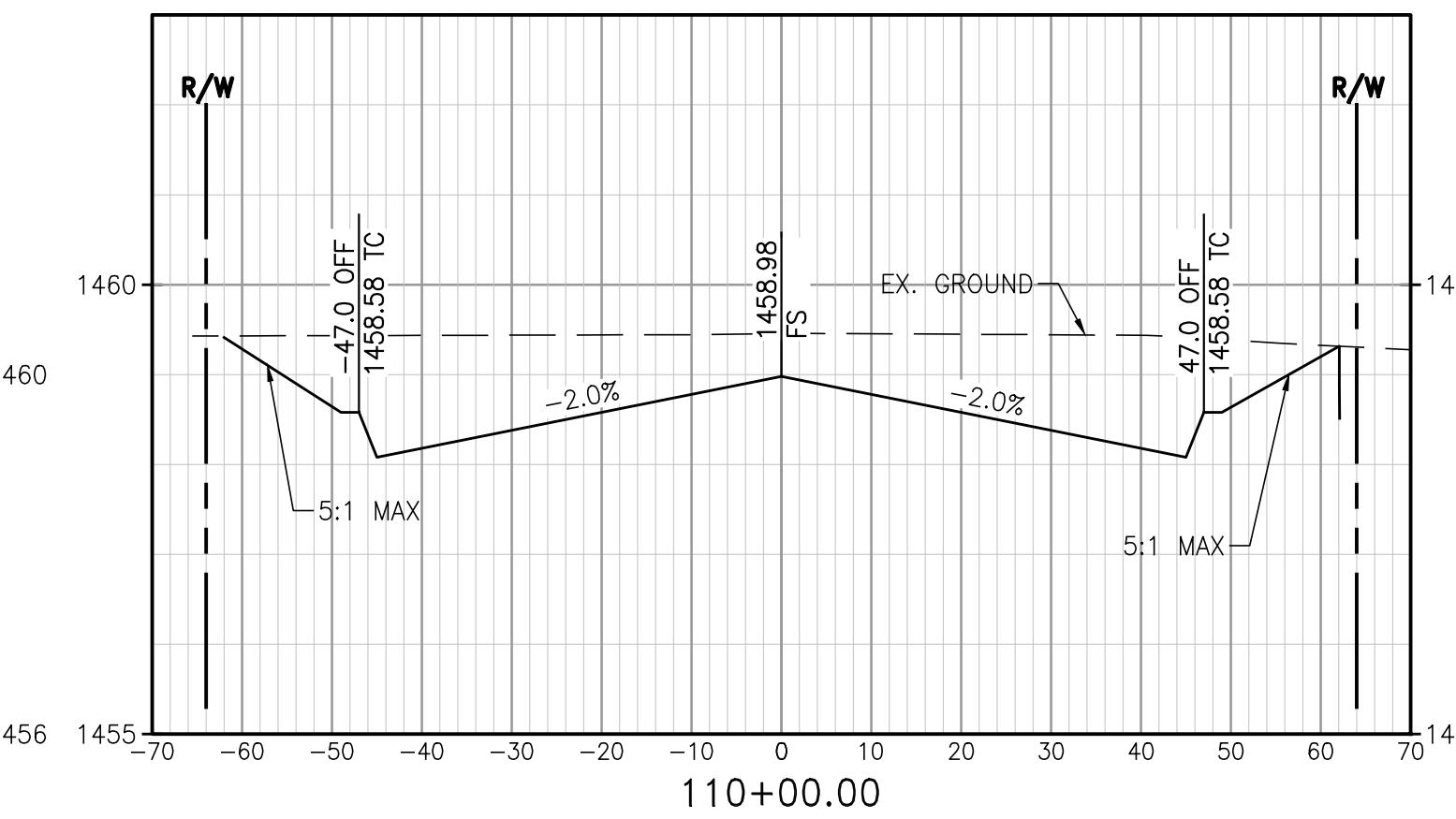
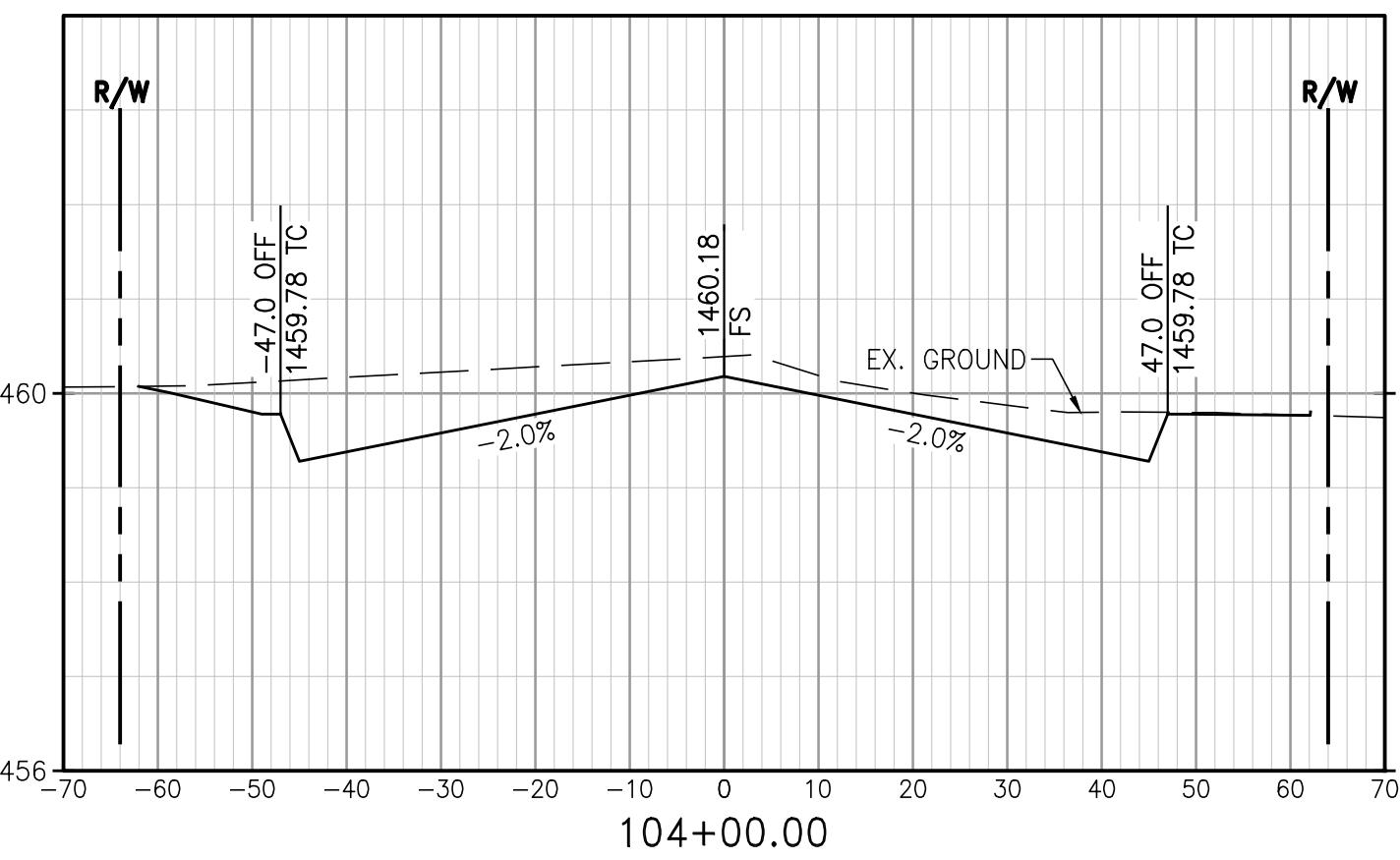
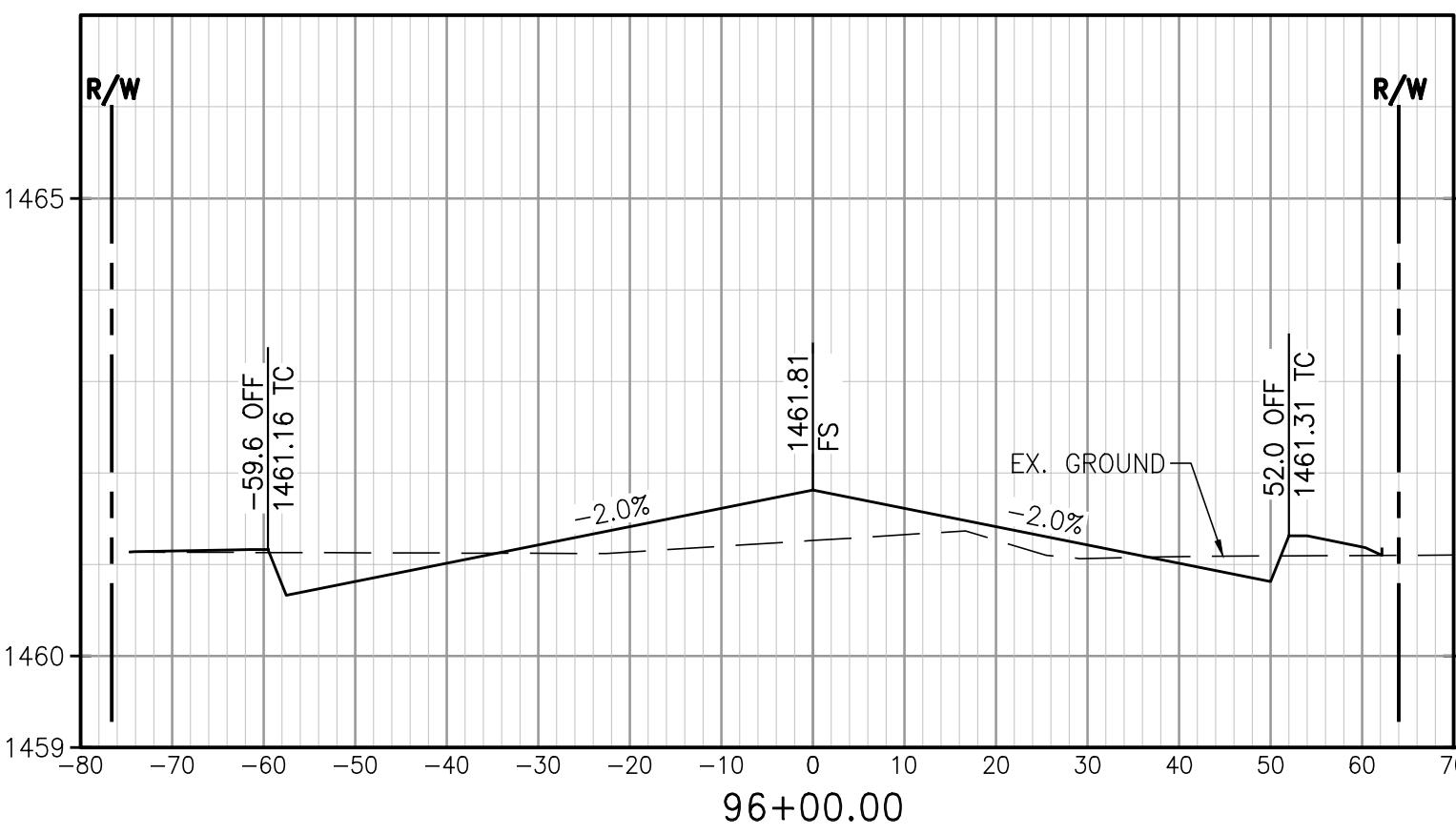
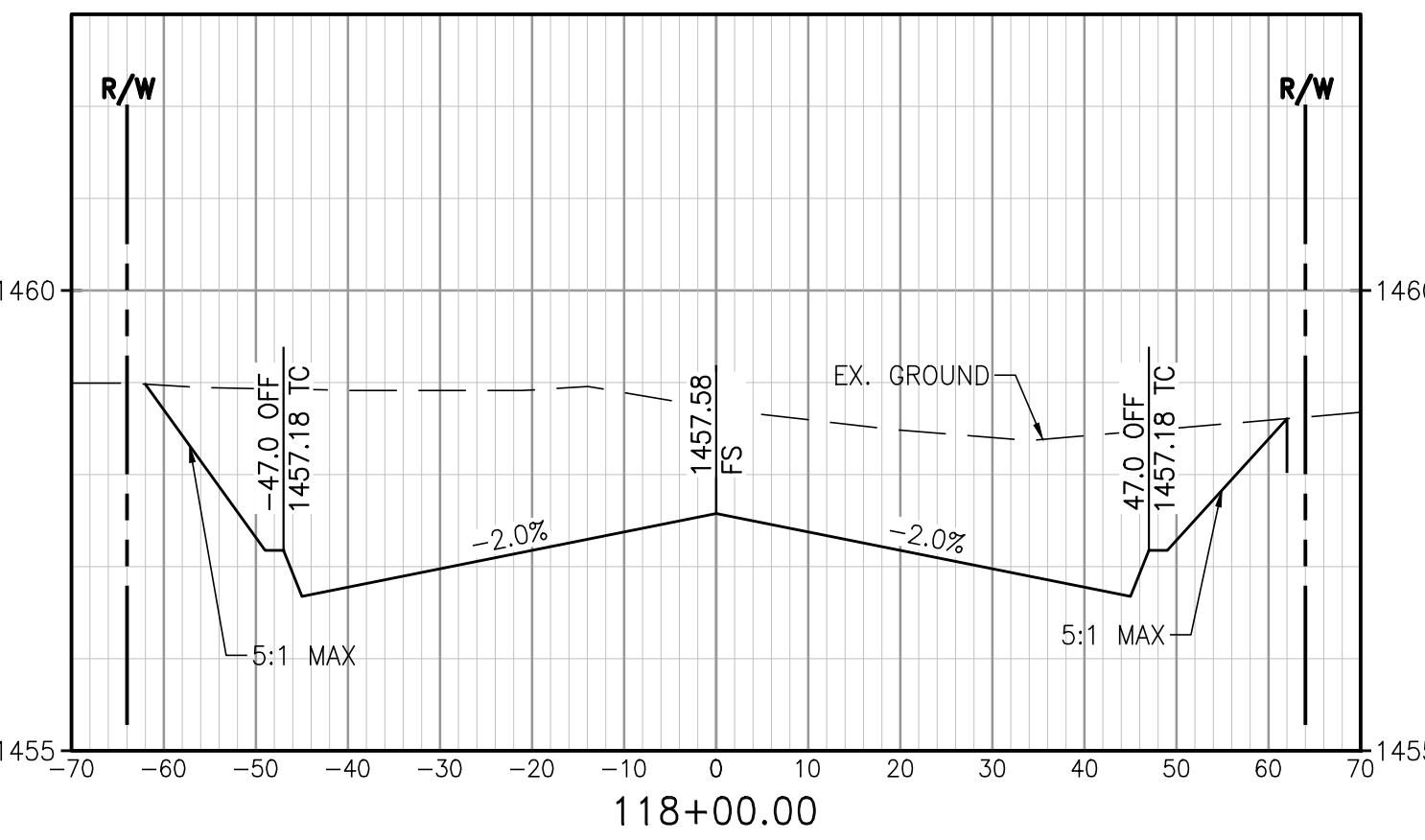
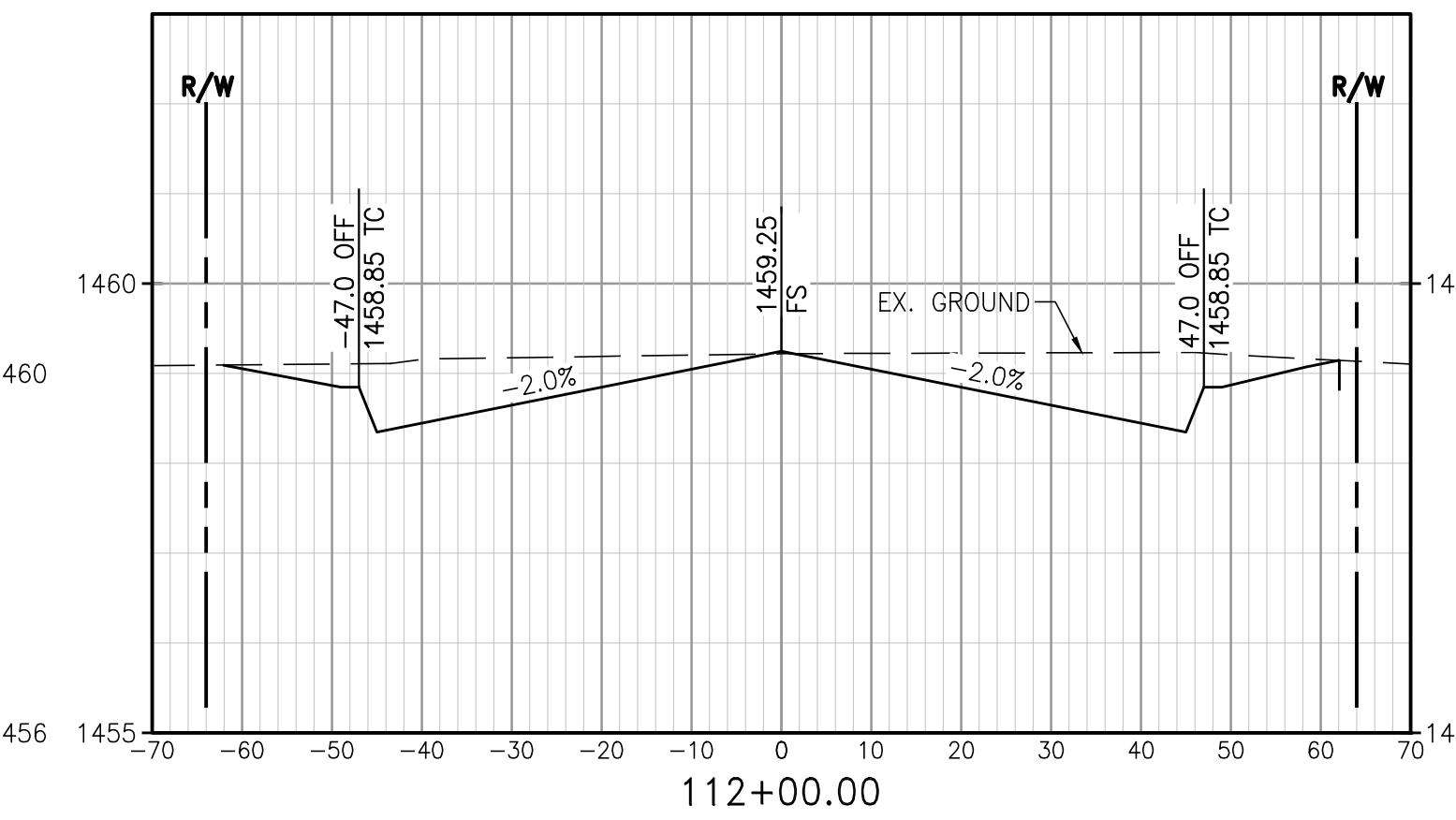
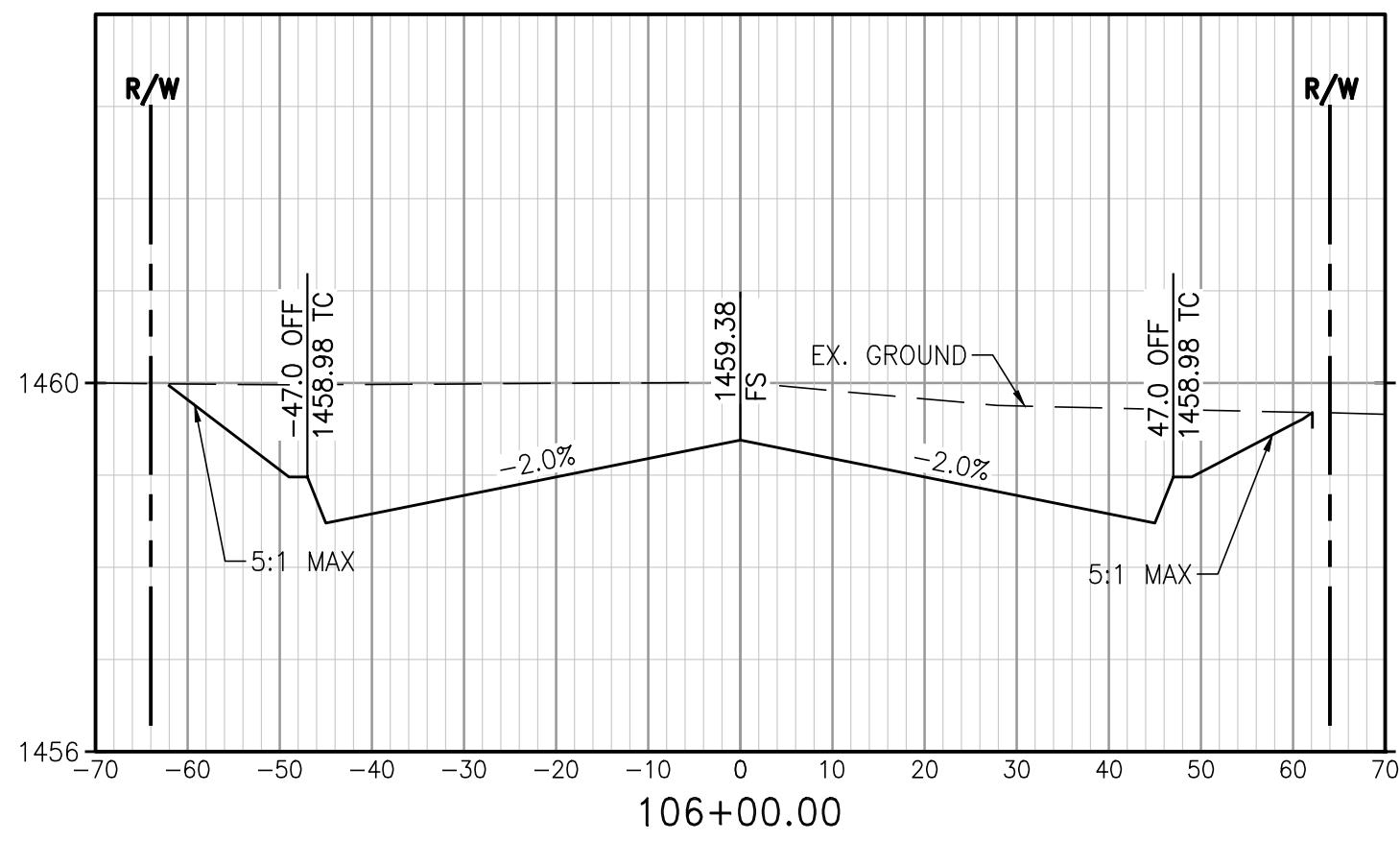
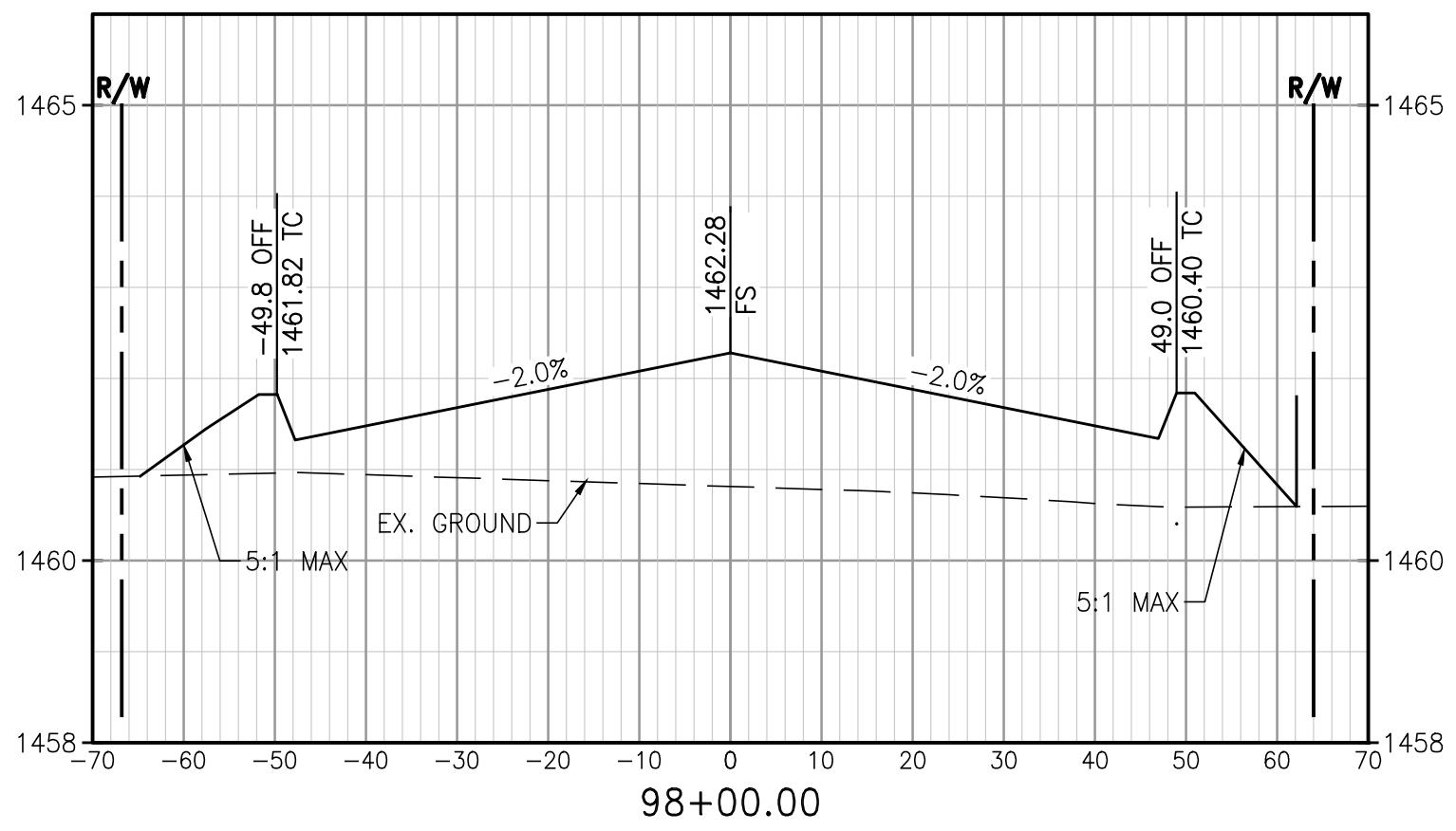
AS BUILT

THESE PLANS REFLECT ANY SUBSTANTIAL DESIGN MODIFICATIONS AS PROVIDED TO WEBB ASSOCIATES BY THE CONTRACTOR

[Signature]

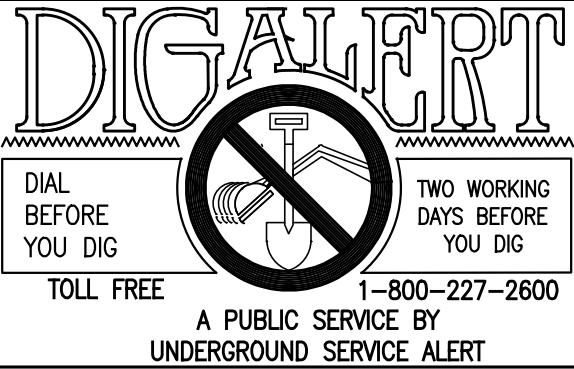
05/19/2016

DATE



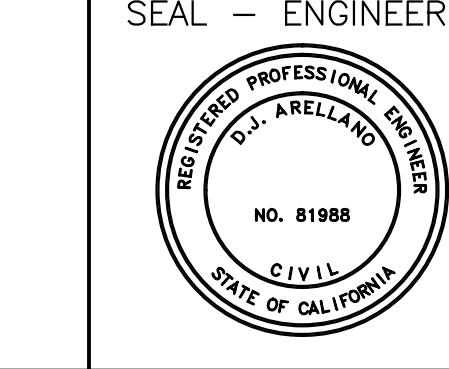
NOTE: MEDIAN OMITTED FROM SECTIONS

FOR REFERENCE ONLY



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MARK	BY DATE	REVISIONS	APPR.	DATE
ENGINEER	CITY			

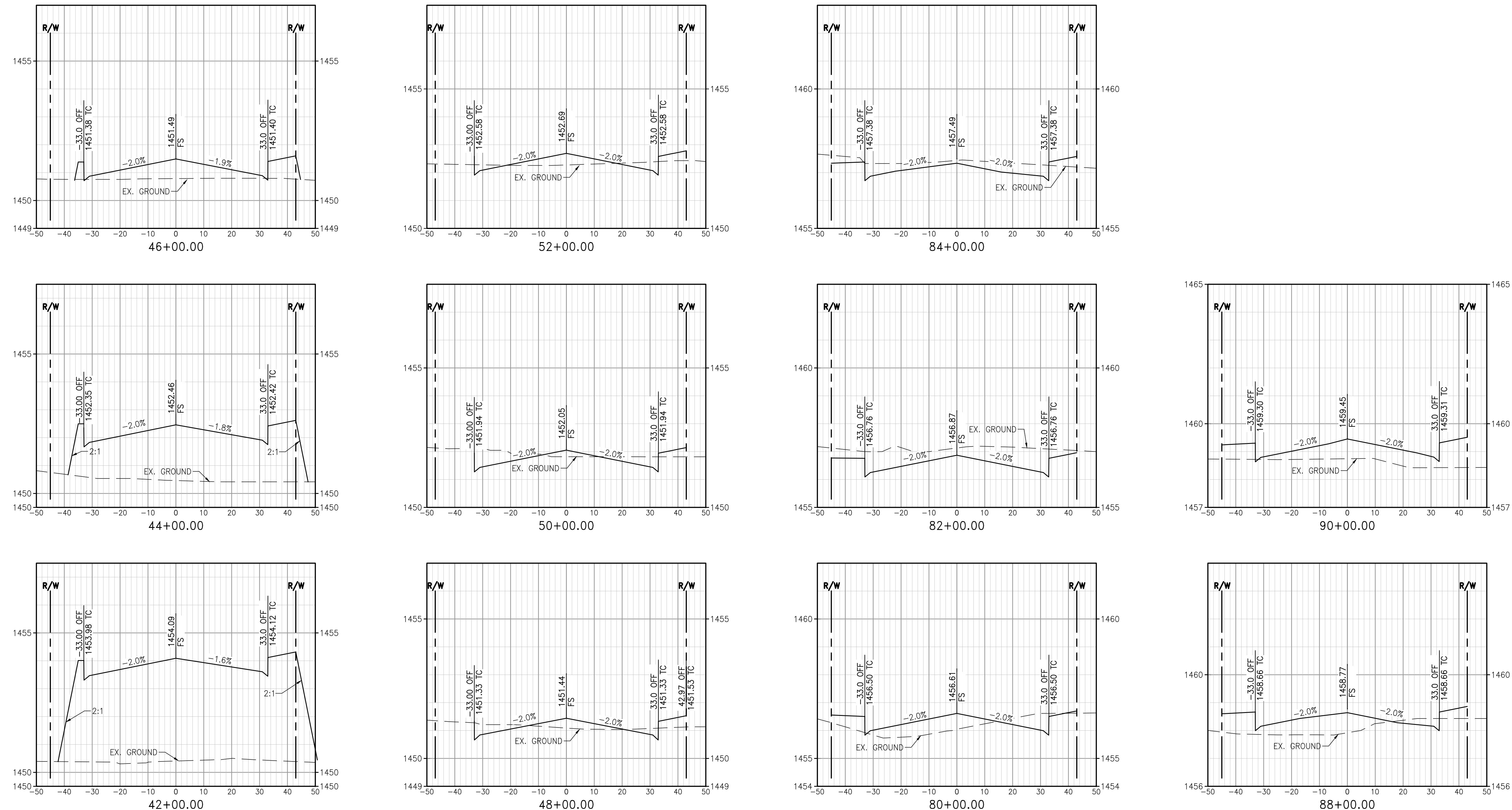


ENGINEERING CONSULTANTS
3788 McCRAY STREET
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PH. (951) 686-1070
FAX (951) 788-1256
UNDER THE SUPERVISION OF:
[Signature]
D.J. ARELLANO R.C.E. #C81988 DATE 1/12/2015

BENCHMARK:
SEE HEREON

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
STREET IMPROVEMENT PLAN
HARLEY KNOX BLVD CROSS SECTIONS

SHEET NO.
22
OF 23 SHEETS
PA-1189
CITY FILE NO.
PA-1189
W.O. 2013-0239
FOR: IDI
H: 1"=20' V: 1"=2'

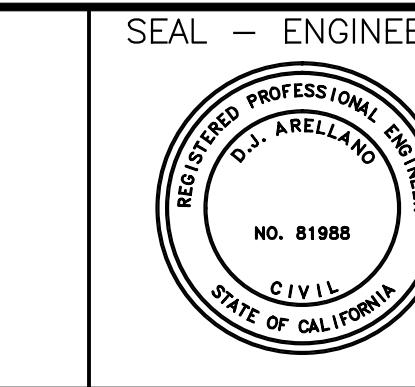


NOTE: MEDIANES OMITTED FROM SECTIONS



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MARK	BY	DATE	APPR.	DATE
REVISIONS			CITY	
ENGINEER				



ALBERT A. ENGINEERING CONSULTANTS
WEBB ASSOCIATES
REGISTERED PROFESSIONAL ENGINEER
D.J. ARELLANO
NO. 81988
CIVIL
STATE OF CALIFORNIA
UNDER THE SUPERVISION OF:
D.J. ARELLANO
R.C.E. #C81988
1/12/2015
DATE

BENCHMARK:
SEE SHEET 1

CITY OF PERRIS
AMENDED DPR NO. 11-12-0004
STRATFORD RANCH-PARCEL MAP 36469
SECTIONS AND DETAILS
REDLANDS AVE CROSS SECTIONS
SHEET NO. 23
OF 23 SHEETS
FOR REFERENCE ONLY

